

APPENDIX A

**SEDIMENT VIBRACORE COLLECTION AND PROCESSING METHODS, STATION
SUMMARIES, AND GRAPH CORE PROFILES**

APPENDIX A-1

SEDIMENT VIBRACORE COLLECTION AND PROCESSING METHODS

A.1 INTRODUCTION

This appendix provides additional details for the work performed under Work Orders (WOs) 4A-080/4A-080A, and summarizes the rationale for project activities performed by Amec Foster Wheeler. This appendix is organized as follows:

- Section A.2 – Standard Operating Procedures Development: presents the rationale for changes to development of standard operating procedures (SOPs) for WO 4A-080 Task 1 and WO 4A-80A.
- Section A.3 – Sediment Core Collection and Transport Methodology: presents the scope and methods used for sediment collection and transport of cores (WO 4A-80 Task 1).
- Section A.4 – Processing, Analytical Methods, and Sampling Schemes: presents the methods used to prepare and process sediment cores for analyses (WO 4A-80 Task 2).
- Section A.5 – Station Summaries: presents station summaries of the cores collected and processed (WO 4A-80 Tasks 1 and 2).
- Section A.6 – References: provides references for documents cited in this appendix.

A.2 STANDARD OPERATING PROCEDURES DEVELOPMENT

In July and August 2017, Amec Foster Wheeler Environment & Infrastructure, Inc. (Amec Foster Wheeler) project management met with Dr. Kevin Yeager and associates of the University of Kentucky regarding the methods used for core collection in the 2009 Phase II scope of work. These efforts resulted in developing SOPs for coring, core handling, core sectioning, subsampling aliquots from sectioned cores, and sample preparations to be followed by Amec Foster Wheeler in work conducted under WOs 4A-080/4A-080A. To this end, Amec Foster Wheeler developed SOP No. S-22, Sediment Core Processing and Interval Sample Collection (September 14, 2017) which is appended to the QAPP (Amec Foster Wheeler, 2016). Quality assurance audits were performed at the Amec Foster Wheeler and University of Kentucky processing laboratories during sample analyses, and the labs were found to be operating in accordance with SOP No. S-22.

A.3 SEDIMENT CORE COLLECTION AND TRANSPORT METHODOLOGY

Methodology used to collect and transport sediment cores associated with WOs 4A-080/4A-080A and modifications to the planned scope of work are described below. Station summary details (including a narrative summary of sediment core collection and processing activities, sediment core field data records (FDRs), Global Positioning System (GPS) deployment accuracy, sediment core logs, and sediment lab bench sheets) are presented in **Appendix A-2**.

A.3.1 OBJECTIVES OF CORING

Sixty-six stations were proposed for the 2017 coring program. At each station, the primary objective was to retrieve cores suitable for thin-interval sectioning and analyses. The number of cores recovered per station varied based on two factors: (1) whether the station represented a location that was a repeat sampling of a 2009 station; and (2) whether the station was being sampled for geochronology and mercury, or only for mercury. For cores that represented repeat locations and were being sampled for geochronology and mercury, sampling occurred in triplicate. For cores that were not repeat locations and were being sampled for geochronology and mercury, sampling occurred in duplicate. For cores that were being sampled only for mercury, sampling entailed recovery of a single core. The principal reason for recovery of either two or three cores for the geochronology program was to allow selection of the least-disturbed core from replicate samples. For the three categories of cores, the sampling goal was recovery of a 90-centimeter (cm) core of consolidated sediment.

At stations located within subtidal and intertidal zones, the secondary objective was to retrieve a supplemental core of soft, unconsolidated sediment. This material is typically discarded in preparation of cores for geochronology analysis. For the unconsolidated sediment, the sampling goal was recovery of 1-foot cores with sampling occurring in duplicate.

A.3.2 CORING STATION NOMENCLATURE

There were three naming conventions for the coring stations, two of which generally followed the reach and management unit convention established and used consistently by Amec Foster Wheeler field teams. The core identification reflected the coring station demarcated numerically (first station, second station, etc.) and the deployment sequence demarcated with an alpha code (i.e., A, B, C, or D). The three naming conventions are as follows:

- For 2017 locations also sampled in 2009, the station names were repeated (i.e., if the 2009 station location was PBR 4, the 2017 station ID was PBR-04).
- For 2017 locations that were not sampled in 2009, cores were labelled by reach – management unit - transect number – station number – core deployment. Thus, UPB-MU11-GC-1-C represents Upper Penobscot Bay, Management Unit 11, geochronology core, first core station, third deployment.
- For 2017 locations that were associated with a transect, cores were labelled by reach – transect number - station number – core deployment. Thus, MM-T1-C1-B represents Mendall Marsh - transect number one - first core station - second deployment.

In some instances, a deployment did not result in an acceptable core. In this case, the deployment was still recorded and the FDR was completed with an alpha code for the deployment. The result of this naming strategy is that the final recovered cores may not be named or numbered sequentially.

A.3.3 WORK PLANS

WO 4A-080 originally proposed the use of vibracore equipment for coring. Following evaluation of proposed methods and analytical objectives, the coring protocol was modified to include manual piston cores, slide hammer, push cores, and box cores.

A.3.4 TARGET RECOVERY: CORING

Multiple coring techniques were tailored to field conditions to achieve consistent target recoveries across the subtidal zone, intertidal zone and marsh platform. Two types of cores were collected:

- 90-cm consolidated core: 90-cm consolidated sediment cores were used for geochronology and total mercury analyses. Coring targeted a 4-foot penetration depth using vibracore, manual piston core, and slide hammer techniques.
- 1.0-foot unconsolidated core: 1.0-foot unconsolidated sediment cores were used for characterization of soft sediments in the intertidal and subtidal zones. Coring targeted a 2.0-foot penetration depth using the manual push core technique and a 1.0-foot hand push core penetration depth when a box core was utilized.

An acceptable core was defined as a core in which 70 percent of the target length was recovered; for locations in which multiple cores were retrieved (see Section A.3.1), comparison of duplicate and triplicate cores allowed for determination of acceptable refusal.

During the field program, it was determined that an additional soft-liner core could be collected at intertidal and subtidal locations, opened aboard the field sampling platform, and used to evaluate sediment stratigraphy prior to use of the vibracore technique. These real-time observations allowed for adjustment to the vibracore program to improve core recovery. Stations for which an additional soft-liner core was collected are detailed in **Appendix A-2**.

A.3.5 INTACT SEDIMENT SURFACE

To best replicate the 2009 coring program outlined in the Phase II Study Report (PRMSP, 2013), Amec Foster Wheeler met with field team personnel from the University of Kentucky. Discussions focused on the details of how cores would be collected and processed, specifically addressed the handling and storage of cores, as well as the strategy used to identify the intact sediment surface.

To be consistent with the 2009 Phase II procedures, the intact sediment surface was determined and secured as follows:

- Following recovery of a core, a ruler was inserted into the top of the core barrel using minimal to no force until resistance was felt.
- The depth of resistance was defined as the consolidated sediment surface.

- Distance from the top of the core barrel to the consolidated sediment surface was recorded, then marked on the outside of the core barrel liner.
- A hole was drilled through the core barrel liner approximately 1 inch above the consolidated sediment surface to allow removal of overlying water and sediments.
- A Dremel tool was used to cut the core barrel liner to the level of the intact surface layer and a cap was secured to the top of the core.

During the field program, it became apparent that there was frequently a surface interval of soft, unconsolidated sediment that was disturbed/re-suspended during coring of subtidal and intertidal sediments. To recover this material for analysis, both push cores and box cores were added to the sampling program to minimize the disturbance and resuspension of the soft sediment. It was also determined that this material could be most effectively preserved for handling by freezing the core soon after recovery. This methodology (i.e., recovering 1-foot cores of undisturbed unconsolidated surface sediment and then freezing it in the field) was added to the sampling program. Material recovered following this field sampling approach was characterized as unconsolidated, although cores of this material often recovered a small plug of the underlying consolidated bed sediment at the base of the core.

A.3.6 SEQUENCE OF OPERATIONS FOR CORE COLLECTION

Three crews were necessary to perform the field work proposed under WO 4A-080/080A. For subtidal and intertidal coring, two field crews on subcontracted vessels were used. The third crew performed marsh platform coring, as well as some of the nearshore intertidal coring. The sequence of operations for each on-water vessel and crew and the marsh platform coring crew are presented below.

A.3.6.1 Research Vessel (R/V) *Edison*

The R/V *Edison* is a 34-foot custom pontoon vessel designed for retrieving deep (8–10-foot) cores from the subtidal zone. The R/V *Edison* was operated by a three-person crew consisting of a US Coast Guard-licensed captain and two coring crew members, and two Amec Foster Wheeler project scientists. The vessel was equipped with a center-vessel moonpool and an approximately 12-foot-tall A-frame for lifting and retrieving sampling equipment. During sampling, a three-point anchor system was used to secure the vessel. Station location data were recorded onboard with a Trimble SPS351 Differential GPS placed within 1 foot of the moonpool. Water depths were recorded from the starboard side of the vessel by a transducer with corrections made by lead line.

Coring equipment on board included a Rossfelder P3 Vibracore with a head weight of 150 pounds and a vibration frequency of 2,850 vibrations per minute at 50 hertz, and a custom-built 1x1x1.5-foot box core sampler weighing 150 pounds with a sampling volume of 1.5 cubic feet. Both the

vibracore and the box core were deployed by gravity through the moonpool of the vessel and retrieved using the onboard winch and A-frame. Other equipment used aboard the R/V *Edison* included a drill, ruler, measuring tape, reciprocating saw, Dremel tool, and core catchers.

Coring with a soft liner employed flexible, 6-mil polyethylene tubing. Coring with a hard liner employed 3-7/8-inch inner diameter rigid polycarbonate tubing.

Coring to recover consolidated bed sediment was performed as follows:

- The R/V *Edison* navigated to each station and was secured on station using a 3-point anchor system.
- Water depth was determined by transducer and verified by lead line.
- The appropriate liner was loaded into the vibracore system barrel, and a 6-foot steel barrel was used for 4-foot penetration.
 - For soft-liner deployments, a soft liner was inserted in the steel barrel. The liner was secured in the steel barrel with rivets joining the liner, steel barrel and core catcher at the bottom of the barrel.
 - For hard-liner deployments, a section of hard liner was placed in the steel barrel and cut to the length with a reciprocating saw. Holes were drilled through the hard liner to match holes located in the steel barrel. Rivets were used to join the hard liner, steel barrel and core catcher.
- Once equipment was rigged for deployment, the GPS position was recorded and the equipment deployed through the vessel moonpool. The vibracore system was lowered to the sediment surface at a controlled rate.
- Once the system reached the sediment surface, vibration was activated and the barrel advanced to the desired penetration. Penetration depth was assessed using a measuring tape attached to the head of the vibracore and by cable markings on the winch.
- After the desired penetration was achieved, the coring equipment was retrieved to the vessel deck.
- Upon retrieval of a soft-liner core, the core was placed horizontally on deck so that material wasn't lost out of the bottom of the vibracore barrel and the liner was cut open. The lithology of the core was documented, and the station location for the associated hard-liner core was adjusted if needed. Material in the soft-liner core was stowed on deck until the station sampling was complete and then was discarded back to the river at the location of collection.
- Upon retrieval of a hard-liner core, cores were maintained in a vertical orientation by securing the core to the bow railing of the vessel. For these cores, visual lithology was documented and the resistance layer defining the consolidated sediment surface was identified. Fluid mud and overlying water were drained, the core was capped, and the

cap was secured with electrical tape. Once the top cap was secured, the core was placed horizontally, the core catcher was removed and a bottom cap was placed and secured with electrical tape. The core liner was labeled with the Station ID, core letter, date and time of collection, an arrow pointing toward the top of the core and the word “TOP” written to indicate core orientation. Both core caps were labeled with the Station ID, core letter and indication of top or bottom. Once labeled, the core was placed in an ice-bath consisting of a large poly drum filled daily with site water and ice for temperature control until arrival landside.

- Equipment was decontaminated between deployments.

For unconsolidated cores, collection aboard the R/V *Edison* was generally performed following the below procedures:

- The box core sampler was rigged for deployment by opening the jaws of the device and placing the release pin.
- Once the equipment was rigged for deployment, a GPS position was recorded and the equipment was deployed through the vessel moonpool.
- The sampler could free fall at winch-lowering speed into the sediment surface and retrieved after 15–30 seconds.
- Once the box core sampler was retrieved to deck and secured, two 1-foot-long hard liners were inserted by hand into the recovered sediment and capped at the top.
- Once cores were recovered from the box core, bottom caps were placed on the liners; the hard liner was maintained in a vertical orientation.
- The core liner was labeled with the Station ID, core letter, date and time of collection, an arrow indicating the direction of the top of the core and the word “TOP” written to indicate core orientation.
- Both core caps were labeled with the Station ID, core letter and indication of top or bottom.
- General lithology of the two cores was documented visually and detailed on the FDR. A single FDR was completed for each individual deployment.
- Liners were placed in an on-vessel freezer (a cooler with dry ice, refreshed as needed) until arrival landside. Cores were maintained vertically in the cooler.

A.3.6.2 *Coring Carolina*

The *Coring Carolina* is a 24-foot customized Carolina Skiff, optimal for obtaining manual-piston cores and manual push cores in shallow, intertidal locations. The *Coring Carolina* was operated by a three-person crew consisting of a US Coast Guard-licensed captain and two coring crew members, and two Amec Foster Wheeler project scientists. The vessel is equipped with stabilizers, a moonpool, and an approximately 10-foot-tall A-frame structure used for hoisting

sampling equipment onboard. The vessel was secured at each coring location with two spud legs. Location data on the *Coring Carolina* was recorded with MX42-DGPS equipment, which was located approximately 2 feet off the starboard side of the moonpool. Water depths were recorded from the starboard side of the vessel using a transducer with lead line corrections.

On the first day of coring aboard the *Coring Carolina*, at station OR-T3-C3, the crew attempted to obtain consolidated cores using a custom hydraulic vibracore equipment designed and built by TG&B Marine Services, Inc. Due to the intensity of the coring vibration during sediment penetration, this method resulted in poor recovery and severely disturbed cores. The coring technique was replaced with manual piston core equipment to better achieve WO objectives for recovery of acceptable consolidated sediment cores. This system was utilized to complete the remainder of work conducted in WO4A-80 aboard the *Coring Carolina* vessel.

The manual piston core system, developed and built by TG&B Marine Services of Monument Beach, Massachusetts, uses a piston placed at the leading edge of a 2-5/8-inch inner diameter polycarbonate liner and secured with a clamp to the sampler head. A sufficient length of stainless steel pipe is used to lower the liner to the bottom. A rope line attached to the piston inside the liner is held taut aboard the vessel to keep the piston stationary approximately 1 inch above the sediment surface while manually pushing the core to advance the liner into the sediment. If pushing the core encountered resistance/refusal, then a slide hammer is attempted to achieve desired depth, then the sampler assembly is retrieved to the vessel deck.

Unconsolidated cores were obtained using a WaterMark Universal Core Sediment Sampler, which is analogous to the manual piston core sampler without the use of the slide hammer. The system uses a 2-5/8-inch inner diameter polycarbonate liner secured with a clamp to the sampler head, which contains a one-way valve that provides suction to retain the core in the liner. A sufficient length of stainless steel pipe is secured to the sampler head and used to lower the liner to the bottom. Manual force is used to push the liner into the sediment to retrieve a sediment core. When the desired depth of penetration is achieved, the sampler assembly is vertically retrieved to the vessel deck.

The following procedure was used aboard the *Coring Carolina* to obtain consolidated cores using the manual piston sampler:

- The *Coring Carolina* was navigated to and spudded onto the coring station.
- The GPS position was recorded and the equipment deployed through the vessel moonpool.
- The water depth measurement was taken via lead line measurement in the vessel moonpool.

- The manual piston sampler was rigged and proper measurements taken to prevent over-penetration of the sampler into the sediment.
- The sampler was deployed through the vessel moonpool to the sediment surface. Once on the bottom, the taut line was cleated off to the vessel A-frame to provide stability and to hold the piston near the top of the sediment surface.
- A GPS position was recorded using a handheld tablet connected to an R1 Integrated GNSS System held directly over the core position in the vessel moonpool.
- The sampler was pushed by manual force to a depth at which it could not be advanced further. Once this depth was achieved, the sampler was advanced with the slide hammer to either the desired penetration depth or refusal (if occurred first).
- The sampler was retrieved to deck using manual force. The bottom cap was placed when the liner rose above the water surface. Any material protruding from the bottom of the liner upon retrieval was captured and labelled as nose material prior to placing the bottom cap.
- Liners were handled in a vertical orientation.
- Fluid mud measurements were obtained, the intact sediment surface was established, and overlying water drained before a cap was placed on top of the liner and secured with electrical tape.
- The core liner was labeled with the Station ID, core letter, date and time of collection, an arrow indicating the direction of the top of the core, and the word “TOP” to indicate core handling orientation.
- Both core caps were labeled with the Station ID, core letter and indication of top or bottom.
- General lithology was documented visually through the core liner and pertinent field information was documented on the FDR for the coring deployment. A single FDR was completed for each individual deployment.
- Once labeled, the core was placed in an ice bath (a large poly drum filled daily with site water and ice) to provide temperature control until arrival landside.
- Equipment was decontaminated between deployments.

The following procedure was used aboard the *Coring Carolina* to obtain unconsolidated cores using the WaterMark Universal Core Sediment Sampler:

- The *Coring Carolina* was navigated to and spudded onto the coring station.
- Once the vessel was spudded onto the coring station, a GPS position was recorded and the equipment deployed through the vessel moonpool.
- The water depth measurement was taken via lead line measurement in the vessel moonpool.

- The WaterMark Universal Core Sediment sampler was rigged and proper measurements taken to prevent over-penetration into the sediment.
- The sampler was deployed through the vessel moonpool to the sediment surface.
- The sampler was pushed by manual force to the desired penetration depth, or refusal, whichever was encountered first.
- The sampler was retrieved to deck using manual force. As soon as the liner broke the water's surface, a cap was placed on the bottom to reduce the possibility of material loss and was secured with electrical tape. Any material protruding from the bottom of the liner upon retrieval was captured and labelled as nose material prior to placing the cap.
- Liner cores were handled in a vertical orientation and a cap was placed on the top of the liner without determining the intact sediment surface or trimming the liner.
- The core liner was labeled with the Station ID, core letter, date and time of collection, an arrow indicating the direction of the top of the core, and the word "TOP" to indicate core handling orientation.
- Both core caps were labeled with the Station ID, core letter, and indication of top or bottom.
- General lithology of the two cores was documented by visual methods through the core liner, and pertinent field information was documented on the FDR for each deployment. A single FDR was completed for each individual deployment.
- Liners were placed in an on-vessel freezer (a cooler with dry ice, refreshed as needed) until arrival landside. Cores were retained in vertical orientation in the cooler.

A.3.6.3 Marsh Platform Coring Sequence of Operations

Coring in the marsh platform zone was performed by Amec Foster Wheeler staff. A typical field crew consisted of three to five individuals. This section describes the methodology employed by the field crew for collecting consolidated and unconsolidated cores.

Cores were obtained with a sampler that utilized a 10-pound slide hammer and 120-cm steel core barrel. A 3-inch outer diameter plastic sleeve was placed inside the 120-cm steel core barrel. Cores were obtained in proximity of one another at the planned GPS coring location, as shown on the figures in **Appendix A-2**. GPS locations were collected using a handheld tablet and an R1 Integrated GNSS System. After core collection, a test pit was excavated using a shooter shovel to obtain field descriptions of the sediment. In situations where a test pit was not possible (i.e., soft/saturated sediment), a push core sampler was used to obtain a sediment core for field description purposes.

The following procedure was used to obtain consolidated cores utilizing the slide hammer technique:

- The field crew walked to the proposed coring location. If the core location was located in Orland River, access was prearranged per the Orland River access agreements (WO4A-080A Task 3).
- A GPS position was recorded using a handheld tablet connected to an R1 Integrated GNSS System held directly over the deployed core.
- Core barrels for each location were driven into the ground with the slide hammer.
- Sediment was excavated around driven core barrels to relieve suction and allow for easy extraction of the core barrels from the ground.
- The test pit was excavated adjacent to the coring location to document general lithology in proximity to the core locations. In situations where soft or saturated sediments were encountered, push cores were used to collect materials for lithology classification.
- The water depth was measured in the core hole after extraction of the core from the ground.
- The core liner was extracted from the steel barrel and labeled with the Station ID, core letter, date and time of collection, an arrow indicating the direction of the top of the core, and the word “TOP” to indicate core handling orientation.
- The top core cap was labeled with the Station ID, core letter, and indication of top. Both caps were secured to the liner with electrical tape.
- Liners were handled in a vertical orientation from the time of extraction to storage in the field station cool storage.
- A single FDR was completed for each coring station. Multiple deployments were recorded on a single FDR.

The procedure detailed above was used for obtaining unconsolidated cores. In some instances, where vegetation was abundant, the slide hammer was utilized to advance the sampler to the target penetration. In other instances, due to the soft/saturated nature of the surface sediment, the sampler was pushed to achieve target penetration.

A.3.7 LANDSIDE STORAGE OF COLLECTED CORES AT FIELD STATION

Consolidated cores were stored in a vertical orientation in landside refrigerated storage at a temperature of 4 degrees Celsius. Unconsolidated cores were stored in vertical orientation in landside freezer storage at a temperature of about -20 degrees Celsius.

A.3.8 TRANSPORTING SEDIMENT CORES FOR PROCESSING

The sediment coring program yielded 65 consolidated cores and 27 unconsolidated cores that were transported to the sediment processing laboratory in Durham, North Carolina, and the University of Kentucky laboratory in Lexington, Kentucky, via ground transportation and packed in custom built containers in general accordance with ASTM International (ASTM) D4220, Standard Practices for Preserving and Transporting Soil Samples. Consolidated cores were transported on ice and packed with foam insulation and vermiculite to limit disturbance during transit. These cores were transported horizontally and vertically. Frozen 1-foot unconsolidated cores were transported in a chest freezer packed with vermiculite and foam insulation. The frozen cores were transported vertically.

An attempt was made early in the field investigation to ship cores by air courier. Cores for this attempt were packaged on ice horizontally and secured with custody seals. At some point, between the FedEx office in Bangor, Maine, and the University of Kentucky laboratory, the custody seals were broken and two cores were removed from the shipping receptacle. Due to the loss of cores during shipment, air courier was abandoned as a potential transportation method.

A.4 PROCESSING, ANALYTICAL METHODS, AND SAMPLING SCHEMES

This section provides information and references for the core preparation and processing conducted by Amec Foster Wheeler and the University of Kentucky, and analytical methods for samples shipped to other laboratories. Additional details on each station and cores are included in **Appendix A-2**.

A.4.1 CORE PREPARATION

Consolidated and unconsolidated cores were prepared and processed using different methodologies to meet project goals and objectives. The consolidated sediment cores were prepared for processing and interval sectioning at both the Amec Foster Wheeler and University of Kentucky sediments laboratories. Unconsolidated sediment cores were processed by Amec Foster Wheeler. Sediment core processing and interval sample collection was conducted in general accordance with SOP-S22, Consolidated Sediments; and SOP-S25, Unconsolidated Sediments (Amec Foster Wheeler, 2016).

The sediment lab was subdivided into separate work areas to minimize cross-contamination. The first sediment lab work area was designated for opening the cores and removing the overlying water from consolidated cores, when necessary. The second sediment lab work area was designated for logging the cores, homogenizing discrete intervals, measurements, and subsampling aliquots for laboratory analyses. Sediment lab work surfaces were cleaned and

appropriately decontaminated between cores, and equipment that encountered sediment was either decontaminated before re-use or was used a single time and then discarded.

Information recorded for consolidated cores included the amount of overlying water drawn off, the reason for selection, lithology, aliquot intervals, and photographs. If the core was selected for chemistry, bulk density plugs were collected. The wet aliquot sheets recorded the weight of material in each container for analysis. This information is included with the station summaries in **Appendix A-2**.

Information recorded for unconsolidated cores included the reason for selection, lithology, aliquot intervals, and photographs. If the core was selected for chemistry, then a wet aliquot sheet also recorded the weight of material placed in each container for analysis. This information is included with the station summaries in **Appendix A-2**.

A.4.2 CORE PROCESSING – CONSOLIDATED CORES

The following procedures were performed on co-located geochronology and mercury cores. Upon arrival at the sediment lab, consolidated cores were stored in an on-site cool storage unit that maintained a temperature of 4 degrees Celsius. In the first sediment lab work area, overlying water was manually suctioned and wicked, and the overlying water depth was recorded. The top of the sediment surface was marked on the liner exterior and the liner was cut with a Dremel tool to insure a snug fit of the cap at the sediment surface interface. Next, the core was placed in a custom guide and a circular saw was used to cut the liner longitudinally. The core was then moved to the second sediment lab work area where the core was opened and logged.

Following logging, intervals were sectioned, homogenized, and aliquoted for laboratory analyses. As proposed in the WO regarding the geochronology stations, multiple consolidated cores were collected to provide for the laboratory selection of the least-disturbed core for analyses. Each of these geochronology cores was opened and logged, and qualified laboratory personnel then selected the appropriate core. This selection process was in accordance with the procedures outlined in SOP-S22. Material was homogenized by hand in a stainless-steel bowl prior to transferring samples to laboratory sample jars. After subsampling aliquots, jars were placed in the on-site cool storage. Material left over after subsampling aliquots for chemical analyses was retained as a record sample and placed in cool storage.

A.4.2.1 Interval Sectioning Methodology

Consolidated cores were sectioned into intervals utilizing the following method, where sufficient mass was available:

- 1-cm increments from 0–20 cm;

- 2-cm increments from 20–40 cm; and
- 5-cm increments from 40–90 cm or the end of the core.

A.4.2.2 Bulk Density Measurements

Select intervals from processed cores were analyzed for bulk density. A one-cubic-cm plug of sample was obtained from the center of each designated interval from the core using a plastic syringe. The sample was placed in a tin and dried in an oven for a period of seven hours. After seven hours, the mass was measured and the sample placed in the oven for another one-hour period. After the second drying period, the mass was weighed again. If the sample mass change was less than 1 percent, the drying was considered complete. If the change was greater than 1 percent, the sample was dried and measured at one-hour intervals until the change was less than 1 percent. The oven used for drying the samples was a Blue M LO-225-E Laboratory Oven, maintained at a temperature of 110 degrees Celsius. Mass measurements were recorded on laboratory bench sheets that are included in individual station summaries in **Appendix A-2**.

A.4.2.3 Chemical Analyses

This section details the chemical analyses performed on interval sections and the laboratories that performed the analyses. For the co-located geochronology and mercury cores, interval sections were subsampled and provided to laboratories for chemical analysis in the following priority sequence:

- Radiochemistry at the University of Kentucky, American Radiation Services, General Engineering Laboratories, Texas A&M University at Galveston, and Flett Research Ltd. laboratories.
- Total mercury by US Environmental Protection Agency (EPA) Method 1631 following the project-specific adaptation 7474-1631 at Eurofins Frontier Global Sciences and Flett Research Ltd.
- Total organic carbon by the Lloyd-Kahn method on select samples and total solids by Standard Method 2540B at Alpha Analytical, Inc.
- Particulate organic carbon at University of Kentucky and Texas A&M University at Galveston laboratories.
- Bulk density performed at Amec Foster Wheeler and University of Kentucky laboratories.
- Grain size performed by laser diffraction at University of Kentucky laboratory.

Cores from mercury-specific stations were prepared and processed at the Amec Foster Wheeler sediment laboratory. The cores were opened and logged prior to sectioning following the same procedures as the co-located geochronology and mercury cores. Cores were sectioned for

analysis as follows, and samples were provided to laboratories for chemical analysis in the following volume driven priority sequence:

- Total mercury by EPA Method 1631 following the project-specific adaptation 7474-1631 at Eurofins Frontier Global Sciences.
- Total organic carbon by Lloyd-Kahn method on select samples and total solids by Standard Method 2540B at Alpha Analytical, Inc.
- Bulk density performed at Amec Foster Wheeler sediment laboratory.
- Organic content by ASTM D2974C at 550 degrees Celsius performed by Amec Foster Wheeler.
- Grain size performed by laser diffraction at University of Kentucky laboratory.

Excess amount of the homogenized sample, when available, was retained as a record sample and placed into temperature controlled storage.

A.4.3 CORE PROCESSING – UNCONSOLIDATED CORES

Unconsolidated cores were stored in an on-site chest freezer maintained at a temperature of approximately -20 degrees Celsius. At most locations where unconsolidated cores were retrieved, a replicate core was collected. One frozen core was designated for chemical analyses and one for lithology. Selection of the core for chemical analysis was based on the definition of the ice/sediment interface and recovered core length. If only one unconsolidated core was obtained from a station, the single core was processed for chemical analysis, and lithology was not recorded.

A.4.3.1 Interval Sectioning Methodology

For the frozen unconsolidated core designated for chemical analyses, the liner and frozen sediment were cut into “interval pucks” using a chop saw. These cut intervals were placed in a stainless-steel bowl and allowed to thaw over a 3-hour period in the second sediment lab work area. Once thawed, the intervals were homogenized using stainless-steel mixing rods and transferred to laboratory sample jars. The additional samples of excess mass were placed in refrigerated storage.

A.4.3.2 Chemical Analysis

Intervals were subsampled from unconsolidated cores in the following volume-driven priority order: total mercury by EPA Method 1631 following the project-specific adaptation 7474-1631 at Eurofins Frontier Global Sciences; total organic carbon by Lloyd-Kahn method on select samples and total solids by Standard Method 2540B at Alpha Analytical, Inc.; and organic content by ASTM D2974C at 550 degrees Celsius by Amec Foster Wheeler. An amount of the homogenized

sample, when available, was retained as a record sample and placed into temperature controlled storage.

Proposed sampling and analysis priority order for the 1-foot unconsolidated cores (depending on the analytical lab minimum sample mass) was as follows:

- 0.0–0.1 foot,
- 0.1–0.3 foot,
- 0.3–0.5 foot,
- 0.5–0.7 foot, and
- 0.7–1 foot.

The plastic core liner of the frozen core designated for lithology was cut lengthwise down the core using a custom-made guide. Following cutting, cores were moved to the second sediment lab work area where the frozen core was thawed, the lithology was logged, and the core was photographed.

Data recorded in the lab included photographs, lithology, selection or rejection reasoning, and aliquot weights. This information is included with the station summaries in **Appendix A-2**.

A.5 STATION SUMMARIES

Core station summaries for the 66 locations where coring was performed are included in **Appendix A-2**. Each core station summary includes:

- Narrative summary of sediment core collection and processing activities;
- The FDR for the core;
- GPS deployment accuracy;
- Core logs;
- Sediment lab bench sheets; and
- Sediment lab photo logs.

A.6 REFERENCES

Amec Foster Wheeler Environment & Infrastructure, Inc. (Amec Foster Wheeler). 2016. Draft Quality Assurance Project Plan (QAPP), Penobscot River Phase III Engineering Study, Penobscot River, Maine. July 26.

Penobscot River Mercury Study Panel (PRMSP). 2013. Final Report: Mercury Contamination of the Penobscot River Estuary: Current Situation, Remediation Targets, and Possible Remediation Procedures. Penobscot River Mercury Study. April.

APPENDIX A-2
SEDIMENT VIBRACORE STATION SUMMARIES
(PROVIDED ELECTRONICALLY)

APPENDIX B

LABORATORY ANALYTICAL AND DATA VALIDATION REPORTS

APPENDIX B-1
ANALYTICAL LABORATORY REPORTS
(PROVIDED ELECTRONICALLY)

APPENDIX B-2
ANALYTICAL DATA VALIDATION REPORTS

EQUIPMENT AND ROOM BLANK RESULTS

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	E1631 Mercury NG/L Total	
					Result	Qualifier
1707702	QC	7/25/2017	EQ_072517_PONAR_QC	EB	0.74	
1707704	QC	7/25/2017	EQ_072517_CSHOE_QC	EB	0.15	J
1707704	QC	7/25/2017	EQ_072517_CORE_QC	EB	0.50	U
1710686	QC	10/11/2017	AFWRDUSEDSLAB_101117_FB_R1_QC	FB	0.25	J
1710686	QC	10/11/2017	AFWRDUSEDSLAB_101117_FB_R2_QC	FB	0.42	J
1710686	QC	10/11/2017	AFWRDUDIH2O_101117_EB_QC	EB	0.50	U
1710686	QC	10/11/2017	AFWRDUSINK_101117_EB_QC	EB	0.40	J
1710725	QC	10/16/2017	UKYSEDSLAB_101617_FB_R1_QC	FB	0.22	J
1710725	QC	10/16/2017	UKYSEDSLAB_101617_FB_R2_QC	FB	0.18	J
1710725	QC	10/16/2017	UKYSEDSLAB_101617_FB_R3_QC	FB	0.14	J
1710725	QC	10/16/2017	UKYSEDSLAB_101617_FB_R4_QC	FB	0.16	J

Notes

EB = Equipment Blank
 FB = Field Blank
 J = Estimated value
 U = Result is non-detect
 NG/L = Nanograms per liter
 QC = Quality Control

INTER LABORATORY COMPARISON RESULTS - GAMMA SPECTROSCOPY

Sample ID	Lab Fraction Method Parameter Unit	ARS N EPA 901.1M Cesium-137 PCI/G			Flett T Gamma Spec Cesium-137 PCI/G			GEL N HSL300 Cesium-137 PCI/G			TAMUG T Gamma Spec Cesium-137 PCI/G			UKY T Gamma Spec Cesium-137 PCI/G			%RSD (3 reps for all labs)	
		Result	Qual	%RSD	Result	Qual	%RSD	Result	Qual	%RSD	Result	Qual	%RSD	Result	Qual	%RSD	%RSD	
PBR-20-F-17_SED_002-015CM_R1		0.097			0.157			0.183			0.246			0.188			31.0	
PBR-20-F-17_SED_002-015CM_R2		0.091		55.6	0.155		18.3	0.129		18.0	0.187		16.3	0.150		12.9	25.0	30.4
PBR-20-F-17_SED_002-015CM_R3		0.227			0.111		J	0.147			0.258			0.155			33.7	
PBR-20-F-17_SED_015-028CM_R1		-0.072	U		-0.033	U			U		0.008				U		NA	
PBR-20-F-17_SED_015-028CM_R2		0.003	U	NA	-0.010	U	NA		U	NA		U	NA		U	NA	NA	NA
PBR-20-F-17_SED_015-028CM_R3		-0.053	U		-0.048	U			U		0.043				U		NA	
PBR-20-F-17_SED_038-048CM_R1		0.001	U		-0.017	U			U		0.014				U		NA	
PBR-20-F-17_SED_038-048CM_R2		-0.066	U	NA	0.015	U	NA		U	NA	0.068		NA		U	NA	NA	NA
PBR-20-F-17_SED_038-048CM_R3		0.013	U		0.011	U			U			U			U		NA	

Notes

- N = Normal
- T = Total
- NA = Not Applicable
- PCI/G = picocuries per gram
- Qual = qualifier
- %RSD = percent relative standard deviation

INTER LABORATORY COMPARISON RESULTS - ALPHA SPECTROSCOPY

Lab Fraction Method Parameter Unit	ARS N HASL-300 Po-01-RC Polonium-210 PCI/G			Flett T Alpha Spec Lead-210 PCI/G			GEL N HSL300 Mod Polonium-210 PCI/G			TAMUG T Alpha Spec Lead-210 PCI/G			UKY T Alpha Spec Lead-210 PCI/G				
	Sample ID	Result	Qual	%RSD	Result	Qual	%RSD	Result	Qual	%RSD	Result	Qual	%RSD	Result	Qual	%RSD	%RSD (3 reps for all labs)
PBR-20-F-17_SED_002-015CM_R1	0.504			0.414			0.586			0.255			0.682			33.5	
PBR-20-F-17_SED_002-015CM_R2	0.484		7.1	0.488		8.4	0.547		5.8	0.322		17.5	0.768		14.3	30.8	27.0
PBR-20-F-17_SED_002-015CM_R3	0.438			0.470			0.614			0.365			0.576			20.7	
PBR-20-F-17_SED_015-028CM_R1	0.29			0.278			0.287			0.197			0.5324			39.9	
PBR-20-F-17_SED_015-028CM_R2	0.292		3.0	0.302		4.3	0.289		8.4	0.174		17.1	0.4752		5.7	35.2	36.2
PBR-20-F-17_SED_015-028CM_R3	0.276			0.297			0.332			0.140			0.4982			41.7	
PBR-20-F-17_SED_038-048CM_R1	0.307			0.294			0.387			0.171			0.5651			42.2	
PBR-20-F-17_SED_038-048CM_R2	0.312		0.8	0.332		6.1	0.346		12.8	0.279		27.5	0.4617		14.9	20.0	29.7
PBR-20-F-17_SED_038-048CM_R3	0.309			0.319			0.299			0.1874			0.4258			27.5	

Notes

N = Normal

T = Total

PCI/G = picocuries per gram

Qual = qualifier

%RSD = percent relative standard deviation

**Data Validation Summary
 2017 Geochronology Interval Cores
 Penobscot River Estuary Phase III – Engineering Evaluation
 Penobscot River, Maine**

1.0 INTRODUCTION

Sediment samples were collected in September, October and November 2017 from the Penobscot River located in Maine. Samples were analyzed by Eurofins Frontier Global Sciences, Inc. (Eurofins) located in Bothell, Washington and included in sample delivery groups (SDGs) 1709433, 1709434, 1709835, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, and 1711304. Samples were also analyzed by Alpha Analytical located in Mansfield, Massachusetts and are reported in SDGs L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290, and L1741134. Samples were analyzed by one or more of the following: Clean Water Act (CWA, 2012) or Standard Methods for the Examination of Water and Wastewater (SM, 2014):

Laboratory	Parameter	Analytical Method	Validation Level
Eurofins	Mercury, total	CWA 1631B (Hot aqua regia digestion)	10% Stage III/ 90% Stage IIB
Alpha	TOC	Lloyd Kahn	10% Stage III/ 90% Stage IIB
Eurofins/Alpha	% Solids	SM2540	10% Stage III/ 90% Stage IIB

A Stage IIB data validation was completed on all SDGs. A Stage III data validation was performed on ten percent of samples. Data validation was completed using National Functional Guidelines for Inorganic Superfund Data Review (USEPA, 2014) and EPA New England Environmental Data Review Supplement for Regional Data Review Elements and Superfund Specific Guidance/Procedures (USEPA, 2013) where applicable. Data quality evaluations were completed using quality control (QC) limits specified in the draft Penobscot River Estuary Phase III Engineering Evaluation Quality Assurance Project Plan (QAPP) [Amec Foster Wheeler, 2016]. The project laboratory reported results using a combination of two detection limits including the reporting limit (RL) and the method detection limit (MDL). Results for compounds that are not detected in samples are reported as U qualified results at the RL. Positive detections between the MDL and RL are qualified as estimated (J) by the laboratory.

Data validation review and qualification actions are discussed in the following subsections. It should be noted that only instances that result in an impact to data quality are presented in this report. There may be QC elements outside of QAPP and/or method control limits not presented in this report since there is no impact to data quality. Samples included in this data evaluation are presented in Table 1.

Data qualifications were completed if necessary in accordance with the guidelines or the professional judgment of the project chemist. The following qualifiers as applied during data validation or reported by the laboratory are included in the final data set:

J = The reported concentration is considered an estimated value

Validation reason codes were applied to results associated with QC measurements outside project QC goals. The validation qualification actions and associated validation reason codes applied to sample

results are summarized on Table 2. The following data validation reason codes were applied to one or more sample results:

- HT = Holding time exceeded
- LD = Lab Duplicate limit exceeded
- MS-H = MS and/or MSD recovery high
- MS-RPD = MS/MSD RPD limit exceeded

A complete summary of final sample results is provided in Table 3.

Data were evaluated based on the following parameters:

- * Data Completeness and Chain of Custody
Holding Times and Preservation
- * Blanks
- * Initial Calibration
- * Continuing Calibration
- * Laboratory Control Sample (LCS)
Matrix Spike/Matrix Spike Duplicates (MS/MSD)
Laboratory Duplicates
- * Field Duplicates
- * Detection Limits
- * Sample Result Verification/Electronic Evaluation Verification (EDD)
- * Ongoing Precision Recovery

- * = indicates that criteria were met and/or no impact to data quality for this parameter

With the exception of the following items discussed below, results were determined to be usable as reported by the laboratory.

2.0 Mercury – 1631

Results were determined to be usable as reported by the laboratory.

3.0 TOC- Lloyd Kahn

Laboratory Duplicate/ Replicate

SDG L1736459 – Sample burn replicate RPDs for samples VE-MU4-GC-1-E-17_SED_011-012CM (32%), VE-MU4-GC-1-E-17_SED_040-045CM (92%), and VE-MU4-GC-1-E-17_SED_055-060CM (50%) exceeded the QC limit of 30%. All TOC results for samples VE-MU4-GC-1-E-17_SED_011-012CM, VE-MU4-GC-1-E-17_SED_040-045CM and VE-MU4-GC-1-E-17_SED_055-060CM were qualified as estimated (J) due to imprecision.

SDG L1736460 – Sample burn replicate RPDs for samples VN-MU3-GC-1-D-17_SED_032-034CM (38%) and VN-MU3-GC-1-D-17_SED_045-050CM (51%) exceeded the QC limit of 30%. All TOC results for samples VN-MU3-GC-1-D-17_SED_032-034CM and VN-MU3-GC-1-D-17_SED_045-050CM were qualified as estimated (J) due to imprecision.

SDG L1739126 – Sample burn replicate RPD for sample FF-MU7-GC-1-B-17_SED_024-026CM (39%) exceeded the QC limit of 30%. All TOC results for sample FF-MU7-GC-1-B-17_SED_024-026CM were qualified as estimated (J) due to imprecision.

Matrix Spike

SDG L1732773 – Sample OR-T3-C2-C-17_SED_140-145CM was used for MS analysis. The MS recoveries for TOC Rep 1 (133%) and TOC Rep 2 (151%) were above the upper QC limit of 125%. Based on professional judgment, all TOC results for sample OR-T3-C2-C17_SED_140-145CM were qualified estimated (J) and are potentially high biased.

SDG L1735008 – Sample ES-01-C3-17_SED_000-001CM was used for MS analysis. The MS recoveries for TOC Rep 1 (356%) and TOC Rep 2 (189%) were above the upper QC limit of 125%. Based on professional judgment, all TOC results for sample ES-01-C3-17_SED_000-001CM were qualified estimated (J) and are potentially high biased.

SDG L1735008 – Sample ES-01-C3-17_SED_040-045CM was used for MS analysis. The MS recovery for TOC Rep 2 (143%) was above the upper QC limit of 125%. Based on professional judgment, the TOC Rep 2 and average TOC results for sample ES-01-C3-17_SED_040-045CM were qualified estimated (J) and are potentially high biased.

SDG L1735009 – Sample ES-18-B-17_SED_001-002CM was used for MS analysis. The MS recovery for TOC Rep 1 (143%) was above the upper QC limit of 125%. Based on professional judgment, the TOC Rep 1 and average TOC results for sample ES-18-B-17_SED_001-002CM were qualified estimated (J) and are potentially high biased.

SDG L1735009 – Sample ES-18-B-17_SED_026-028CM was used for MS analysis. The MS recovery for TOC Rep 1 (141%) and Rep 2 (145%) were above the upper QC limit of 125%. Based on professional judgment, all TOC results for sample ES-18-B-17_SED_026-028CM were qualified estimated (J) and are potentially high biased.

SDG L1735010 – Sample PBR-18-E17_SED_028-030CM was used for MS analysis. The MS recovery for TOC Rep 2 (133%) was above the upper QC limit of 125%. The MS recovery does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample PBR-18-E17_SED_028-030CM do not need to be qualified.

SDG L1736452 – Sample MM-T2-C1-B17_SED_030-032CM was used for MS analysis. The MS recovery for TOC Rep 1 (42%) was below the lower QC limit of 75% and Rep 2 (185%) was above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations are > 4X the spike amount added. Based on professional judgement the TOC results for sample MM-T2-C1-B17_SED_030-032CM do not need to be qualified.

SDG L1736457 – Sample UPB-MU11-GC-1-C2-17_SED_002-003CM was used for MS analysis. The MS recovery for TOC Rep 1 (139%) and Rep 2 (129%) were above the upper QC limit of 125%. The MS recovery for Rep 1 does not apply because the sample concentration is > 4X the spike amount added. Based on professional judgment, Rep 2 and average TOC results for sample UPB-MU11-GC-1-C2-17_SED_002-003CM were qualified estimated (J) and are potentially high biased.

SDG L1736459 – Sample VE-MU4-GC-1-E-17_SED_024-026CM was used for MS analysis. The MS recovery for sample VE-MU4-GC-1-E-17_SED_024-026CM TOC Rep 1 (163%) was above the upper QC limit of 125%. The Rep 1 and average TOC results for sample VE-MU4-GC-1-E-17_SED_024-026CM were qualified estimated (J) and are potentially high biased.

Sample VE-MU4-GC-1-E-17_SED_030-032CM was used for MS analysis. The MS recovery for sample VE-MU4-GC-1-E-17_SED_030-032CM TOC Rep 2 (134%) was above the upper QC limit of 125%. The Rep 2 and average TOC results for sample VE-MU4-GC-1-E-17_SED_030-032CM were qualified estimated (J) and are potentially high biased.

SDG L1736460 – Sample VN-MU3-GC-1-D-17_SED_020-022CM was used for MS analysis. The MS recoveries for sample VN-MU3-GC-1-D-17_SED_020-022CM TOC Rep 1 (127%) and Rep 2 (156%) were above the upper QC limit of 125%. The MS recovery for Rep 1 does not apply because the sample concentration is > 4X the spike amount added. Based on professional judgment, Rep 2 and average TOC results for sample VN-MU3-GC-1-D-17_SED_020-022CM were qualified estimated (J) and are potentially high biased.

Sample VN-MU3-GC-1-D-17_SED_070-075CM was used for MS analysis. The MS recovery for sample VN-MU3-GC-1-D-17_SED_070-075CM TOC Rep 1 (136%) was above the upper QC limit of 125%. Based on professional judgment, Rep 1 and average TOC results for sample VN-MU3-GC-1-D-17_SED_070-075CM were qualified estimated (J) and are potentially high biased.

SDG L1739126 – Samples FF-MU7-GC-1-B-17_SED_005-006CM and FF-MU7-GC-1-B-17_SED_032-034CM were used for MS/MSD analysis.

-) The MSD recovery for sample FF-MU7-GC-1-B-17_SED_005-006CM TOC Rep 1 (167%) was above the upper QC limit of 125%. The MS/MSD RPDs were elevated for Rep 1 (29%) and Rep 2 (34%). Based on professional judgment, Rep 1 and average TOC results for sample FF-MU7-GC-1-B-17_SED_005-006CM were qualified estimated (J) and are potentially high biased. All TOC results for sample FF-MU7-GC-1-B-17_SED_005-006CM were qualified estimated (J) due to the imprecision.
-) The MS and/or MSD recoveries for sample FF-MU7-GC-1-B-17_SED_032-034CM TOC Rep 1 (MSD 135%) and Rep 2 (MS 129%) were above the upper QC limit of 125%. Based on professional judgment, all TOC results for sample FF-MU7-GC-1-B-17_SED_032-034CM were qualified estimated (J) and are potentially high biased.

SDG L1740286 – Sample MM-T4-C2-D-17_SED_075-080CM was used for MS analysis. The MS recovery for TOC Rep 1 (235%) and Rep 2 (148%) were above the upper QC limit of 125%. The MS recovery for Rep 1 does not apply because the sample concentration is > 4X the spike amount added. Based on professional judgment, Rep 2 and average TOC results for sample MM-T4-C2-D-17_SED_075-080CM were qualified estimated (J) and are potentially high biased.

SDG L1740290 – Sample OR-T3-C5-D-17_SED_020-022CM was used for MS analysis. The MS recovery for TOC Rep 1 (146%) was above the upper QC limit of 125%. The MS recovery for Rep 1 does not apply because the sample concentration is > 4X the spike amount added. No qualifications were necessary.

SDG L1741134 – Sample UPB-MU11-GC1-D-17_SED_024-026CM was used for MS analysis. The MS recovery for TOC Rep 2 (137%) was above the upper QC limit of 125%. The MS recovery for Rep 2 does

not apply because the sample concentration is > 4X the spike amount added. No qualifications were necessary.

4.0 Percent Solids – 2540G

Holding Times and Preservation

SDG 1709433 – Percent total solids for each sample in SDG 1709433 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1709434 – Percent total solids for each sample in SDG 1709434 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1709835 – Percent total solids for each sample in SDG 1709835 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1709837 – Percent total solids for each sample in SDG 1709837 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1709838 – Percent total solids for each sample in SDG 1709838 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1709839 – Percent total solids for each sample in SDG 1709839 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1709840 – Percent total solids for each sample in SDG 1709840 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1709841 – Percent total solids for each sample in SDG 1709841 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1709842 – Percent total solids for each sample in SDG 1709842 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1709843 – Percent total solids for each sample in SDG 1709843 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1709844 – Percent total solids for each sample in SDG 1709844 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1709845 – Percent total solids for each sample in SDG 1709845 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1710292 – Percent total solids for each sample in SDG 1710292 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1710318 – Percent total solids for each sample in SDG 1710318 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1710322 – Percent total solids for each sample in SDG 1710322 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1710323 – Percent total solids for each sample in SDG 1710323 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1710903 – Percent total solids for each sample in SDG 1710903 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1711168 – Percent total solids for each sample in SDG 1711168 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1711170 – Percent total solids for each sample in SDG 1711170 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1711172 – Percent total solids for each sample in SDG 1711172 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

SDG 1711304 – Percent total solids for each sample in SDG 1711304 was analyzed beyond technical hold time. The results for total solids were qualified as estimated (J).

Laboratory Duplicate

SDG L1735008 – Sample ES-01-C3-17_SED_000-001CM was selected by the laboratory for duplicate analysis. The RPD (25%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample ES-01-C3-17_SED_000-001CM was qualified estimated (J) due to the imprecision.

SDG L1735010 – Samples PBR-18-E-17_SED_001-002CM and PBR-18-E-17_SED_055-060CM were selected by the laboratory for duplicate analysis. The RPDs of sample PBR-18-E-17_SED_001-002CM (11%) and PBR-18-E-17_SED_055-060CM (15%) exceed the QC limit of 10%. Based on professional judgment, the percent solids result for sample PBR-18-E-17_SED_001-002CM and PBR-18-E-17_SED_055-060CM were qualified estimated (J) due to the imprecision.

References:

Amec Foster Wheeler, 2016. “Draft Penobscot River Estuary Phase III – Engineering Study Quality Assurance Project Plan”, Penobscot River, Maine, July 2016.

Eurofins, 2017. “AMEC Sediment Lab Homogenization and Subsampling Procedure.” Work Instruction EFSR-P-SP-WI15953; August 8, 2017.

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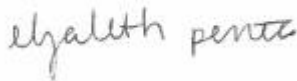
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U.S. Environmental Protection Agency (USEPA), 2013. "EPA New England Environmental Data Review Supplement for Regional Data Review Elements and Superfund Specific Guidance/Procedures"; Quality Assurance Unit Staff; Office of Environmental Measurement and Evaluation; April 22, 2013.

Data Validator: Elizabeth Penta

December 19, 2017



Senior Reviewer: Denise King

December 27, 2017

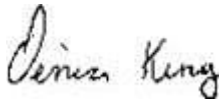


TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_000-001CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_001-002CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_002-003CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_003-004CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_004-005CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_005-006CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_006-007CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_007-008CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_008-009CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_009-010CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_010-011CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_011-012CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_012-013CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_013-014CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_014-015CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_015-016CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_016-017CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_017-018CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_018-019CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_019-020CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_020-022CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_022-024CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_024-026CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_026-028CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_028-030CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_030-032CM	9/12/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_032-034CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_034-036CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_036-038CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_038-040CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_040-045CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_045-050CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_050-055CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_055-060CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_060-065CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_065-070CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_070-075CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_075-080CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_080-085CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_085-090CM	9/12/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_090-095CM	9/13/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_095-100CM	9/13/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_100-105CM	9/13/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_105-110CM	9/13/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_110-115CM	9/13/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_115-120CM	9/13/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_120-125CM	9/13/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_125-130CM	9/13/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_130-135CM	9/13/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_135-140CM	9/13/2017	FS	1	1	
1709433	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_140-145CM	9/13/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_000-001CM	9/11/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury	TOC
					Analysis Method	% Solids	EPA 1631	Lloyd-Kahn
					QC Code			
1709434	SED	PBR-26-A	PBR-26-A-17_SED_001-002CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_002-003CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_003-004CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_004-005CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_005-006CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_006-007CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_007-008CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_008-009CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_009-010CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_010-011CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_011-012CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_012-013CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_013-014CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_014-015CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_015-016CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_016-017CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_017-018CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_018-019CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_019-020CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_020-022CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_022-024CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_024-026CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_026-028CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_028-030CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_030-032CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_032-034CM	9/11/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709434	SED	PBR-26-A	PBR-26-A-17_SED_034-036CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_036-038CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_038-040CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_040-045CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_045-050CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_050-055CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_055-060CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_060-065CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_065-070CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_070-075CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_075-080CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_080-085CM	9/11/2017	FS	1	1	
1709434	SED	PBR-26-A	PBR-26-A-17_SED_085-090CM	9/11/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_000-001CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_001-002CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_002-003CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_003-004CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_004-005CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_005-006CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_006-007CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_007-008CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_008-009CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_009-010CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_010-011CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_011-012CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_012-013CM	9/25/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	QC Code	Method Class	Mercury	TOC
						Analysis Method	% Solids	EPA 1631
1709835	SED	ES-01-C3	ES-01-C3-17_SED_013-014CM	9/25/2017	FS	1	1	
1709835	SED	ES-01-C3	ES-01-C3-17_SED_014-015CM	9/25/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_015-016CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_016-017CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_017-018CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_018-019CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_019-020CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_020-022CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_022-024CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_024-026CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_026-028CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_028-030CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_030-032CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_032-034CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_034-036CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_036-038CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_038-040CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_040-045CM	9/26/2017	FS	1	1	
1709837	SED	PBR-20-E	PBR-20-E-17_SED_045-050CM	9/26/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_015-016CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_016-017CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_017-018CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_018-019CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_019-020CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_020-022CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_022-024CM	9/25/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709838	SED	ES-01-C3	ES-01-C3-17_SED_024-026CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_026-028CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_028-030CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_030-032CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_032-034CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_034-036CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_036-038CM	9/25/2017	FS	1	1	
1709838	SED	ES-01-C3	ES-01-C3-17_SED_038-040CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_040-045CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_045-050CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_050-055CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_055-060CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_060-065CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_065-070CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_070-075CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_075-080CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_080-085CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_085-090CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_090-095CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_095-100CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_100-105CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_105-110CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_110-115CM	9/25/2017	FS	1	1	
1709839	SED	ES-01-C3	ES-01-C3-17_SED_115-120CM	9/25/2017	FS	1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_000-001CM	9/26/2017	FS	1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_001-002CM	9/26/2017	FS	1	1	

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TABLE 1
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	QC Code	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
						Analysis Method	% Solids		
1709840	SED	PBR-20-E	PBR-20-E-17_SED_002-003CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_003-004CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_004-005CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_005-006CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_006-007CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_007-008CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_008-009CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_009-010CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_010-011CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_011-012CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_012-013CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_013-014CM	9/26/2017	FS		1	1	
1709840	SED	PBR-20-E	PBR-20-E-17_SED_014-015CM	9/26/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_000-001CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_001-002CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_002-003CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_003-004CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_004-005CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_005-006CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_006-007CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_007-008CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_008-009CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_009-010CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_010-011CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_011-012CM	9/25/2017	FS		1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_012-013CM	9/25/2017	FS		1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709841	SED	ES-18-B	ES-18-B-17_SED_013-014CM	9/25/2017	FS	1	1	
1709841	SED	ES-18-B	ES-18-B-17_SED_014-015CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_015-016CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_016-017CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_017-018CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_018-019CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_019-020CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_020-022CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_022-024CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_024-026CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_026-028CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_028-030CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_030-032CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_032-034CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_034-036CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_036-038CM	9/25/2017	FS	1	1	
1709842	SED	ES-18-B	ES-18-B-17_SED_038-040CM	9/25/2017	FS	1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_000-001CM	9/26/2017	FS	1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_001-002CM	9/26/2017	FS	1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_002-003CM	9/26/2017	FS	1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_003-004CM	9/26/2017	FS	1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_004-005CM	9/26/2017	FS	1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_005-006CM	9/26/2017	FS	1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_006-007CM	9/26/2017	FS	1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_007-008CM	9/26/2017	FS	1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_008-009CM	9/26/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	QC Code	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
						Analysis Method	% Solids		
1709843	SED	PBR-18-E	PBR-18-E-17_SED_009-010CM	9/26/2017	FS		1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_010-011CM	9/26/2017	FS		1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_011-012CM	9/26/2017	FS		1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_012-013CM	9/26/2017	FS		1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_013-014CM	9/26/2017	FS		1	1	
1709843	SED	PBR-18-E	PBR-18-E-17_SED_014-015CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_015-016CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_016-017CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_017-018CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_018-019CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_019-020CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_020-022CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_022-024CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_024-026CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_026-028CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_028-030CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_030-032CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_032-034CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_034-036CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_036-038CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_038-040CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_040-045CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_045-050CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_050-055CM	9/26/2017	FS		1	1	
1709844	SED	PBR-18-E	PBR-18-E-17_SED_055-060CM	9/26/2017	FS		1	1	
1709845	SED	ES-18-B	ES-18-B-17_SED_040-045CM	9/25/2017	FS		1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709845	SED	ES-18-B	ES-18-B-17_SED_045-050CM	9/25/2017	FS	1	1	
1709845	SED	ES-18-B	ES-18-B-17_SED_050-055CM	9/25/2017	FS	1	1	
1709845	SED	ES-18-B	ES-18-B-17_SED_055-060CM	9/25/2017	FS	1	1	
1709845	SED	ES-18-B	ES-18-B-17_SED_060-065CM	9/25/2017	FS	1	1	
1709845	SED	ES-18-B	ES-18-B-17_SED_065-070CM	9/25/2017	FS	1	1	
1709845	SED	ES-18-B	ES-18-B-17_SED_070-075CM	9/25/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_000-001CM	9/29/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_001-002CM	9/29/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_002-003CM	9/29/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_003-004CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_004-005CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_005-006CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_006-007CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_007-008CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_008-009CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_009-010CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_010-011CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_011-012CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_012-013CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_013-014CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_014-015CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_015-016CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_016-017CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_017-018CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_018-019CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_019-020CM	10/2/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_020-022CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_022-024CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_024-026CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_026-028CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_028-030CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_030-032CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_032-034CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_034-036CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_036-038CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_038-040CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_040-045CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_045-050CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_050-055CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_055-060CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_060-065CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_065-070CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_070-075CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_075-080CM	10/2/2017	FS	1	1	
1710292	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_080-085CM	10/2/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_000-001CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_001-002CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_002-003CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_003-004CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_004-005CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_005-006CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_006-007CM	9/27/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury	TOC
					Analysis Method	% Solids	EPA 1631	Lloyd-Kahn
					QC Code			
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_007-008CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_008-009CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_009-010CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_010-011CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_011-012CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_012-013CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_013-014CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_014-015CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_015-016CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_016-017CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_017-018CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_018-019CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_019-020CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_020-022CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_022-024CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_024-026CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_026-028CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_028-030CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_030-032CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_032-034CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_034-036CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_036-038CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_038-040CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_040-045CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_045-050CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_050-055CM	9/27/2017	FS	1	1	

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_055-060CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_060-065CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_065-070CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_070-075CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_075-080CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_080-085CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_085-090CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_090-095CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_095-100CM	9/27/2017	FS	1	1	
1710318	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_100-105CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_000-001CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_001-002CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_002-003CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_003-004CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_004-005CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_005-006CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_006-007CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_007-008CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_008-009CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_009-010CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_010-011CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_011-012CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_012-013CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_013-014CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_014-015CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_015-016CM	9/27/2017	FS	1	1	

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury	TOC
					Analysis Method	% Solids	EPA 1631	Lloyd-Kahn
					QC Code			
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_016-017CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_017-018CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_018-019CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_019-020CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_020-022CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_022-024CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_024-026CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_026-028CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_028-030CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_030-032CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_032-034CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_034-036CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_036-038CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_038-040CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_040-045CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_045-050CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_050-055CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_055-060CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_060-065CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_065-070CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_070-075CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_075-080CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_080-085CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_085-090CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_090-095CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_095-100CM	9/27/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_100-105CM	9/27/2017	FS	1	1	
1710322	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_105-110CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_000-001CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_001-002CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_002-003CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_003-004CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_004-005CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_005-006CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_006-007CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_007-008CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_008-009CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_009-010CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_010-011CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_011-012CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_012-013CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_013-014CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_014-015CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_015-016CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_016-017CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_017-018CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_018-019CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_019-020CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_020-022CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_022-024CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_024-026CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_026-028CM	9/27/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_028-030CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_030-032CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_032-034CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_034-036CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_036-038CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_038-040CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_040-045CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_045-050CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_050-055CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_055-060CM	9/27/2017	FS	1	1	
1710323	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_060-065CM	9/27/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_000-001CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_001-002CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_002-003CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_003-004CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_004-005CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_005-006CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_006-007CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_007-008CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_008-009CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_009-010CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_010-011CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_011-012CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_012-013CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_013-014CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_014-015CM	10/18/2017	FS	1	1	

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury	TOC
					Analysis Method	% Solids	EPA 1631	Lloyd-Kahn
					QC Code			
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_015-016CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_016-017CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_017-018CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_018-019CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_019-020CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_020-022CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_022-024CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_024-026CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_026-028CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_028-030CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_030-032CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_032-034CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_034-036CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_036-038CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_038-040CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_040-045CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_045-050CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_050-055CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_055-060CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_060-065CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_065-070CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_070-075CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_075-080CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_080-085CM	10/18/2017	FS	1	1	
1710903	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_085-090CM	10/18/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_000-001CM	10/26/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_001-002CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_002-003CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_003-004CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_004-005CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_005-006CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_006-007CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_007-008CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_008-009CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_009-010CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_010-011CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_011-012CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_012-013CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_013-014CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_014-015CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_015-016CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_016-017CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_017-018CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_018-019CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_019-020CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_020-022CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_022-024CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_024-026CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_026-028CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_028-030CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_030-032CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_032-034CM	10/26/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury	TOC
					Analysis Method	% Solids	EPA 1631	Lloyd-Kahn
					QC Code			
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_034-036CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_036-038CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_038-040CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_040-045CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_045-050CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_050-055CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_055-060CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_060-065CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_065-070CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_070-075CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_075-080CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_080-085CM	10/26/2017	FS	1	1	
1711168	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_085-090CM	10/26/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_000-001CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_001-002CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_002-003CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_003-004CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_004-005CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_005-006CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_006-007CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_007-008CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_008-009CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_009-010CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_010-011CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_011-012CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_012-013CM	10/31/2017	FS	1	1	

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury	TOC
					Analysis Method	% Solids	EPA 1631	Lloyd-Kahn
					QC Code			
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_013-014CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_014-015CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_015-016CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_016-017CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_017-018CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_018-019CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_019-020CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_020-022CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_022-024CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_024-026CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_026-028CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_028-030CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_030-032CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_032-034CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_034-036CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_036-038CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_038-040CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_040-045CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_045-050CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_050-055CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_055-060CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_060-065CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_065-070CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_070-075CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_075-080CM	10/31/2017	FS	1	1	
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_080-085CM	10/31/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1711170	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_085-090CM	10/31/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_000-001CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_001-002CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_002-003CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_003-004CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_004-005CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_005-006CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_006-007CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_007-008CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_008-009CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_009-010CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_010-011CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_011-012CM	10/24/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_012-013CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_013-014CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_014-015CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_015-016CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_016-017CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_017-018CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_018-019CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_019-020CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_020-022CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_022-024CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_024-026CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_026-028CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_028-030CM	10/25/2017	FS	1	1	

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_030-032CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_032-034CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_034-036CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_036-038CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_038-040CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_040-045CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_045-050CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_050-055CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_055-060CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_060-065CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_065-070CM	10/25/2017	FS	1	1	
1711172	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_070-075CM	10/25/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_000-001CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_001-002CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_004-005CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_011-012CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_014-015CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_015-016CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_016-017CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_017-018CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_019-020CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_020-022CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_022-024CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_024-026CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_026-028CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_028-030CM	11/1/2017	FS	1	1	

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_030-032CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_032-034CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_034-036CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_036-038CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_038-040CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_040-045CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_045-050CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_050-055CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_055-060CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_060-065CM	11/1/2017	FS	1	1	
1711304	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_065-070CM	11/1/2017	FS	1	1	
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_000-001CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_001-002CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_003-004CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_005-006CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_006-007CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_007-008CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_014-015CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_017-018CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_020-022CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_022-024CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_024-026CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_026-028CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_028-030CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_030-032CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_032-034CM	9/11/2017	FS			1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_034-036CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_036-038CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_038-040CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_040-045CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_045-050CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_050-055CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_055-060CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_060-065CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_065-070CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_070-075CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_075-080CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_080-085CM	9/11/2017	FS			1
L1732772	SED	PBR-26-A	PBR-26-A-17_SED_085-090CM	9/11/2017	FS			1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_000-001CM	9/12/2017	FS			1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_001-002CM	9/12/2017	FS			1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_003-004CM	9/12/2017	FS			1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_004-005CM	9/12/2017	FS			1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_005-006CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_006-007CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_007-008CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_008-009CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_009-010CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_010-011CM	9/12/2017	FS			1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_011-012CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_012-013CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_014-015CM	9/12/2017	FS	1		1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
				QC Code				
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_015-016CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_016-017CM	9/12/2017	FS			1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_017-018CM	9/12/2017	FS			1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_018-019CM	9/12/2017	FS			1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_019-020CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_020-022CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_022-024CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_024-026CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_026-028CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_028-030CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_030-032CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_032-034CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_034-036CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_036-038CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_038-040CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_040-045CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_045-050CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_050-055CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_055-060CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_060-065CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_065-070CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_070-075CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_075-080CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_080-085CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_085-090CM	9/12/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_090-095CM	9/13/2017	FS	1		1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_095-100CM	9/13/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_100-105CM	9/13/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_105-110CM	9/13/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_110-115CM	9/13/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_115-120CM	9/13/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_120-125CM	9/13/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_125-130CM	9/13/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_130-135CM	9/13/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_135-140CM	9/13/2017	FS	1		1
L1732773	SED	OR-T3-C2-C	OR-T3-C2-C-17_SED_140-145CM	9/13/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_000-001CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_001-002CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_002-003CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_003-004CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_004-005CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_015-016CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_017-018CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_020-022CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_022-024CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_024-026CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_026-028CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_028-030CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_030-032CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_032-034CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_034-036CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_036-038CM	9/25/2017	FS	1		1

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_038-040CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_040-045CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_045-050CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_050-055CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_055-060CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_060-065CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_065-070CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_070-075CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_075-080CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_080-085CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_085-090CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_090-095CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_095-100CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_100-105CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_105-110CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_110-115CM	9/25/2017	FS	1		1
L1735008	SED	ES-01-C3	ES-01-C3-17_SED_115-120CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_001-002CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_002-003CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_003-004CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_004-005CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_005-006CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_007-008CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_008-009CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_010-011CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_011-012CM	9/25/2017	FS	1		1

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1735009	SED	ES-18-B	ES-18-B-17_SED_012-013CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_013-014CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_014-015CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_015-016CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_016-017CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_017-018CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_018-019CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_019-020CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_020-022CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_022-024CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_024-026CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_026-028CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_028-030CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_030-032CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_032-034CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_034-036CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_036-038CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_038-040CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_040-045CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_045-050CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_050-055CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_055-060CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_060-065CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_065-070CM	9/25/2017	FS	1		1
L1735009	SED	ES-18-B	ES-18-B-17_SED_070-075CM	9/25/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_001-002CM	9/26/2017	FS	1		1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_002-003CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_008-009CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_010-011CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_014-015CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_018-019CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_019-020CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_020-022CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_022-024CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_024-026CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_026-028CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_028-030CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_030-032CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_032-034CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_034-036CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_036-038CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_038-040CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_040-045CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_045-050CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_050-055CM	9/26/2017	FS	1		1
L1735010	SED	PBR-18-E	PBR-18-E-17_SED_055-060CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_000-001CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_001-002CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_002-003CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_003-004CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_004-005CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_006-007CM	9/26/2017	FS	1		1

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_008-009CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_009-010CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_011-012CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_012-013CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_013-014CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_016-017CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_017-018CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_018-019CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_020-022CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_022-024CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_024-026CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_026-028CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_028-030CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_030-032CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_032-034CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_034-036CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_036-038CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_038-040CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_040-045CM	9/26/2017	FS	1		1
L1735011	SED	PBR-20-E	PBR-20-E-17_SED_045-050CM	9/26/2017	FS	1		1
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_030-032CM	10/2/2017	FS			1
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_036-038CM	10/2/2017	FS			1
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_038-040CM	10/2/2017	FS			1
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_040-045CM	10/2/2017	FS	1		1
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_045-050CM	10/2/2017	FS	1		1
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_050-055CM	10/2/2017	FS	1		1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_055-060CM	10/2/2017	FS	1		1
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_060-065CM	10/2/2017	FS	1		1
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_065-070CM	10/2/2017	FS	1		1
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_070-075CM	10/2/2017	FS	1		1
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_075-080CM	10/2/2017	FS	1		1
L1736452	SED	MM-T2-C1-B	MM-T2-C1-B-17_SED_080-085CM	10/2/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_002-003CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_011-012CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_014-015CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_015-016CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_019-020CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_020-022CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_022-024CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_024-026CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_026-028CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_028-030CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_030-032CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_032-034CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_034-036CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_036-038CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_038-040CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_040-045CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_045-050CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_050-055CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_055-060CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_060-065CM	9/27/2017	FS	1		1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_065-070CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_070-075CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_075-080CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_080-085CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_085-090CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_090-095CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_095-100CM	9/27/2017	FS	1		1
L1736457	SED	UPB-MU11-GC-1-C2	UPB-MU11-GC-1-C2-17_SED_100-105CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_000-001CM	9/27/2017	FS			1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_001-002CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_002-003CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_003-004CM	9/27/2017	FS			1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_004-005CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_005-006CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_006-007CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_007-008CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_008-009CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_009-010CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_010-011CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_011-012CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_012-013CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_013-014CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_014-015CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_015-016CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_016-017CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_017-018CM	9/27/2017	FS	1		1

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_018-019CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_019-020CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_020-022CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_022-024CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_024-026CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_026-028CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_028-030CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_030-032CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_032-034CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_034-036CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_036-038CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_038-040CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_040-045CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_045-050CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_050-055CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_055-060CM	9/27/2017	FS	1		1
L1736459	SED	VE-MU4-GC-1-E	VE-MU4-GC-1-E-17_SED_060-065CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_020-022CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_022-024CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_024-026CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_026-028CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_028-030CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_030-032CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_032-034CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_034-036CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_036-038CM	9/27/2017	FS	1		1

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_038-040CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_040-045CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_045-050CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_050-055CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_055-060CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_060-065CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_065-070CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_070-075CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_075-080CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_080-085CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_085-090CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_090-095CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_095-100CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_100-105CM	9/27/2017	FS	1		1
L1736460	SED	VN-MU3-GC-1-D	VN-MU3-GC-1-D-17_SED_105-110CM	9/27/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_000-001CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_003-004CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_004-005CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_005-006CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_006-007CM	10/18/2017	FS			1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_007-008CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_008-009CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_009-010CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_010-011CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_011-012CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_012-013CM	10/18/2017	FS	1		1

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_013-014CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_014-015CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_015-016CM	10/18/2017	FS			1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_016-017CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_017-018CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_018-019CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_019-020CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_020-022CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_022-024CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_024-026CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_026-028CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_028-030CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_030-032CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_032-034CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_034-036CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_036-038CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_038-040CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_040-045CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_045-050CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_050-055CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_055-060CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_060-065CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_065-070CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_070-075CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_075-080CM	10/18/2017	FS	1		1
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_080-085CM	10/18/2017	FS	1		1

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739126	SED	FF-MU7-GC-1-B	FF-MU7-GC-1-B-17_SED_085-090CM	10/18/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_020-022CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_022-024CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_024-026CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_026-028CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_028-030CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_030-032CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_032-034CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_034-036CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_036-038CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_038-040CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_040-045CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_045-050CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_050-055CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_055-060CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_060-065CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_065-070CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_070-075CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_075-080CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_080-085CM	10/26/2017	FS	1		1
L1740286	SED	MM-T4-C2-D	MM-T4-C2-D-17_SED_085-090CM	10/26/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_020-022CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_022-024CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_024-026CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_026-028CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_028-030CM	10/31/2017	FS	1		1

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DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_030-032CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_032-034CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_034-036CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_036-038CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_038-040CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_040-045CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_045-050CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_050-055CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_055-060CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_060-065CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_065-070CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_070-075CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_075-080CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_080-085CM	10/31/2017	FS	1		1
L1740288	SED	OR-T2-C5-B	OR-T2-C5-B-17_SED_085-090CM	10/31/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_020-022CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_022-024CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_024-026CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_026-028CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_028-030CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_032-034CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_034-036CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_036-038CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_038-040CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_040-045CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_045-050CM	10/25/2017	FS	1		1

Created by: BCG 12/20/2017

Checked by: EP 12/20/2017

TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_050-055CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_055-060CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_060-065CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_065-070CM	10/25/2017	FS	1		1
L1740290	SED	OR-T3-C5-D	OR-T3-C5-D-17_SED_070-075CM	10/25/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_000-001CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_004-005CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_016-017CM	11/1/2017	FS			1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_020-022CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_022-024CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_024-026CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_026-028CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_028-030CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_030-032CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_032-034CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_034-036CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_036-038CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_038-040CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_040-045CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_045-050CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_050-055CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_055-060CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_060-065CM	11/1/2017	FS	1		1
L1741134	SED	UPB-MU11-GC-1-D	UPB-MU11-GC-1-D-17_SED_065-070CM	11/1/2017	FS	1		1

Notes: Count = # of analytes

FS = Field Sample

SDG = Sample Delivery Group

SED = Sediment

Created by: BCG 12/20/2017

Checked by: EP 12/20/2017

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
L1732773	LLOYD_KAHN	L1732773-49	OR-T3-C2-C-17_SED_140-145CM	T	Total Organic Carbon	2.37		2.37	J	MS-H	PERCENT
L1735008	2540G	L1735008-01	ES-01-C3-17_SED_000-001CM	T	Percent Solids	11.3		11.3	J	LD	PERCENT
L1735008	LLOYD_KAHN	L1735008-01	ES-01-C3-17_SED_000-001CM	T	Total Organic Carbon	3.845		3.845	J	MS-H	PERCENT
L1735008	LLOYD_KAHN	L1735008-18	ES-01-C3-17_SED_040-045CM	T	Total Organic Carbon	1.7		1.7	J	MS-H	PERCENT
L1735009	LLOYD_KAHN	L1735009-01	ES-18-B-17_SED_001-002CM	T	Total Organic Carbon	2.53		2.53	J	MS-H	PERCENT
L1735009	LLOYD_KAHN	L1735009-21	ES-18-B-17_SED_026-028CM	T	Total Organic Carbon	1.24		1.24	J	MS-H	PERCENT
L1735010	2540G	L1735010-01	PBR-18-E-17_SED_001-002CM	T	Percent Solids	29		29	J	LD	PERCENT
L1735010	2540G	L1735010-12	PBR-18-E-17_SED_028-030CM	T	Percent Solids	36.7		36.7	J	LD	PERCENT
L1736457	LLOYD_KAHN	L1736457-01	UPB-MU11-GC-1-C2-17_SED_002-003CM	T	Total Organic Carbon	4.32		4.32	J	MS-H	PERCENT
L1736459	LLOYD_KAHN	L1736459-12	VE-MU4-GC-1-E-17_SED_011-012CM	T	Total Organic Carbon	0.9665		0.9665	J	LD	PERCENT
L1736459	LLOYD_KAHN	L1736459-23	VE-MU4-GC-1-E-17_SED_024-026CM	T	Total Organic Carbon	1.64		1.64	J	MS-H	PERCENT
L1736459	LLOYD_KAHN	L1736459-26	VE-MU4-GC-1-E-17_SED_030-032CM	T	Total Organic Carbon	1.73		1.73	J	MS-H	PERCENT
L1736459	LLOYD_KAHN	L1736459-31	VE-MU4-GC-1-E-17_SED_040-045CM	T	Total Organic Carbon	2.065		2.065	J	LD	PERCENT
L1736459	LLOYD_KAHN	L1736459-34	VE-MU4-GC-1-E-17_SED_055-060CM	T	Total Organic Carbon	1.177		1.177	J	LD	PERCENT
L1736460	LLOYD_KAHN	L1736460-01	VN-MU3-GC-1-D-17_SED_020-022CM	T	Total Organic Carbon	4.715		4.715	J	MS-H	PERCENT
L1736460	LLOYD_KAHN	L1736460-07	VN-MU3-GC-1-D-17_SED_032-034CM	T	Total Organic Carbon	3.155		3.155	J	LD	PERCENT
L1736460	LLOYD_KAHN	L1736460-12	VN-MU3-GC-1-D-17_SED_045-050CM	T	Total Organic Carbon	2.505		2.505	J	LD	PERCENT
L1736460	LLOYD_KAHN	L1736460-17	VN-MU3-GC-1-D-17_SED_070-075CM	T	Total Organic Carbon	1.61		1.61	J	MS-H	PERCENT
L1740286	LLOYD_KAHN	L1740286-18	MM-T4-C2-D-17_SED_075-080CM	T	Total Organic Carbon	4.325		4.325	J	MS-H	PERCENT
1709433	% Solids	1709433-01	OR-T3-C2-C-17_SED_000-001CM	T	Percent Solids	36	O-04	36	J	HT	% BY WT.
1709433	% Solids	1709433-02	OR-T3-C2-C-17_SED_001-002CM	T	Percent Solids	35	O-04	35	J	HT	% BY WT.
1709433	% Solids	1709433-03	OR-T3-C2-C-17_SED_002-003CM	T	Percent Solids	36.5	O-04	36.5	J	HT	% BY WT.
1709433	% Solids	1709433-04	OR-T3-C2-C-17_SED_003-004CM	T	Percent Solids	37	O-04	37	J	HT	% BY WT.
1709433	% Solids	1709433-05	OR-T3-C2-C-17_SED_004-005CM	T	Percent Solids	38	O-04	38	J	HT	% BY WT.
1709433	% Solids	1709433-06	OR-T3-C2-C-17_SED_005-006CM	T	Percent Solids	37.3	O-04	37.3	J	HT	% BY WT.
1709433	% Solids	1709433-07	OR-T3-C2-C-17_SED_006-007CM	T	Percent Solids	37.5	O-04	37.5	J	HT	% BY WT.
1709433	% Solids	1709433-08	OR-T3-C2-C-17_SED_007-008CM	T	Percent Solids	37.4	O-04	37.4	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709433	% Solids	1709433-09	OR-T3-C2-C-17_SED_008-009CM	T	Percent Solids	40.7	O-04	40.7	J	HT	% BY WT.
1709433	% Solids	1709433-10	OR-T3-C2-C-17_SED_009-010CM	T	Percent Solids	37.3	O-04	37.3	J	HT	% BY WT.
1709433	% Solids	1709433-11	OR-T3-C2-C-17_SED_010-011CM	T	Percent Solids	38.8	O-04	38.8	J	HT	% BY WT.
1709433	% Solids	1709433-12	OR-T3-C2-C-17_SED_011-012CM	T	Percent Solids	37.1	O-04	37.1	J	HT	% BY WT.
1709433	% Solids	1709433-13	OR-T3-C2-C-17_SED_012-013CM	T	Percent Solids	33.2	O-04	33.2	J	HT	% BY WT.
1709433	% Solids	1709433-14	OR-T3-C2-C-17_SED_013-014CM	T	Percent Solids	32.2	O-04	32.2	J	HT	% BY WT.
1709433	% Solids	1709433-15	OR-T3-C2-C-17_SED_014-015CM	T	Percent Solids	37.6	O-04	37.6	J	HT	% BY WT.
1709433	% Solids	1709433-16	OR-T3-C2-C-17_SED_015-016CM	T	Percent Solids	35.9	O-04	35.9	J	HT	% BY WT.
1709433	% Solids	1709433-17	OR-T3-C2-C-17_SED_016-017CM	T	Percent Solids	35.9	O-04	35.9	J	HT	% BY WT.
1709433	% Solids	1709433-18	OR-T3-C2-C-17_SED_017-018CM	T	Percent Solids	31.5	O-04	31.5	J	HT	% BY WT.
1709433	% Solids	1709433-19	OR-T3-C2-C-17_SED_018-019CM	T	Percent Solids	30.4	O-04	30.4	J	HT	% BY WT.
1709433	% Solids	1709433-20	OR-T3-C2-C-17_SED_019-020CM	T	Percent Solids	36	O-04	36	J	HT	% BY WT.
1709433	% Solids	1709433-21	OR-T3-C2-C-17_SED_020-022CM	T	Percent Solids	48	O-04	48	J	HT	% BY WT.
1709433	% Solids	1709433-22	OR-T3-C2-C-17_SED_022-024CM	T	Percent Solids	36.8	O-04	36.8	J	HT	% BY WT.
1709433	% Solids	1709433-23	OR-T3-C2-C-17_SED_024-026CM	T	Percent Solids	37.8	O-04	37.8	J	HT	% BY WT.
1709433	% Solids	1709433-24	OR-T3-C2-C-17_SED_026-028CM	T	Percent Solids	36.6	O-04	36.6	J	HT	% BY WT.
1709433	% Solids	1709433-25	OR-T3-C2-C-17_SED_028-030CM	T	Percent Solids	39.6	O-04	39.6	J	HT	% BY WT.
1709433	% Solids	1709433-26	OR-T3-C2-C-17_SED_030-032CM	T	Percent Solids	30.4	O-04	30.4	J	HT	% BY WT.
1709433	% Solids	1709433-27	OR-T3-C2-C-17_SED_032-034CM	T	Percent Solids	36.7	O-04	36.7	J	HT	% BY WT.
1709433	% Solids	1709433-28	OR-T3-C2-C-17_SED_034-036CM	T	Percent Solids	37.5	O-04	37.5	J	HT	% BY WT.
1709433	% Solids	1709433-29	OR-T3-C2-C-17_SED_036-038CM	T	Percent Solids	38.7	O-04	38.7	J	HT	% BY WT.
1709433	% Solids	1709433-30	OR-T3-C2-C-17_SED_038-040CM	T	Percent Solids	40.5	O-04	40.5	J	HT	% BY WT.
1709433	% Solids	1709433-31	OR-T3-C2-C-17_SED_040-045CM	T	Percent Solids	39.1	O-04	39.1	J	HT	% BY WT.
1709433	% Solids	1709433-32	OR-T3-C2-C-17_SED_045-050CM	T	Percent Solids	35.7	O-04	35.7	J	HT	% BY WT.
1709433	% Solids	1709433-33	OR-T3-C2-C-17_SED_050-055CM	T	Percent Solids	37.8	O-04	37.8	J	HT	% BY WT.
1709433	% Solids	1709433-34	OR-T3-C2-C-17_SED_055-060CM	T	Percent Solids	37	O-04	37	J	HT	% BY WT.
1709433	% Solids	1709433-35	OR-T3-C2-C-17_SED_060-065CM	T	Percent Solids	38.5	O-04	38.5	J	HT	% BY WT.

TABLE 2
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709433	% Solids	1709433-36	OR-T3-C2-C-17_SED_065-070CM	T	Percent Solids	36.2	O-04	36.2	J	HT	% BY WT.
1709433	% Solids	1709433-37	OR-T3-C2-C-17_SED_070-075CM	T	Percent Solids	37.8	O-04	37.8	J	HT	% BY WT.
1709433	% Solids	1709433-38	OR-T3-C2-C-17_SED_075-080CM	T	Percent Solids	41.9	O-04	41.9	J	HT	% BY WT.
1709433	% Solids	1709433-39	OR-T3-C2-C-17_SED_080-085CM	T	Percent Solids	40	O-04	40	J	HT	% BY WT.
1709433	% Solids	1709433-40	OR-T3-C2-C-17_SED_085-090CM	T	Percent Solids	39.6	O-04	39.6	J	HT	% BY WT.
1709433	% Solids	1709433-41	OR-T3-C2-C-17_SED_090-095CM	T	Percent Solids	45.4	O-04	45.4	J	HT	% BY WT.
1709433	% Solids	1709433-42	OR-T3-C2-C-17_SED_095-100CM	T	Percent Solids	48.7	O-04	48.7	J	HT	% BY WT.
1709433	% Solids	1709433-43	OR-T3-C2-C-17_SED_100-105CM	T	Percent Solids	53.4	O-04	53.4	J	HT	% BY WT.
1709433	% Solids	1709433-44	OR-T3-C2-C-17_SED_105-110CM	T	Percent Solids	56.3	O-04	56.3	J	HT	% BY WT.
1709433	% Solids	1709433-45	OR-T3-C2-C-17_SED_110-115CM	T	Percent Solids	56.7	O-04	56.7	J	HT	% BY WT.
1709433	% Solids	1709433-46	OR-T3-C2-C-17_SED_115-120CM	T	Percent Solids	60.2	O-04	60.2	J	HT	% BY WT.
1709433	% Solids	1709433-47	OR-T3-C2-C-17_SED_120-125CM	T	Percent Solids	61.7	O-04	61.7	J	HT	% BY WT.
1709433	% Solids	1709433-48	OR-T3-C2-C-17_SED_125-130CM	T	Percent Solids	63	O-04	63	J	HT	% BY WT.
1709433	% Solids	1709433-49	OR-T3-C2-C-17_SED_130-135CM	T	Percent Solids	61.7	O-04	61.7	J	HT	% BY WT.
1709433	% Solids	1709433-50	OR-T3-C2-C-17_SED_135-140CM	T	Percent Solids	64.2	O-04	64.2	J	HT	% BY WT.
1709433	% Solids	1709433-51	OR-T3-C2-C-17_SED_140-145CM	T	Percent Solids	61.5	O-04	61.5	J	HT	% BY WT.
1709434	% Solids	1709434-01	PBR-26-A-17_SED_000-001CM	T	Percent Solids	46.9	O-04	46.9	J	HT	% BY WT.
1709434	% Solids	1709434-02	PBR-26-A-17_SED_001-002CM	T	Percent Solids	46.7	O-04	46.7	J	HT	% BY WT.
1709434	% Solids	1709434-03	PBR-26-A-17_SED_002-003CM	T	Percent Solids	55.9	O-04	55.9	J	HT	% BY WT.
1709434	% Solids	1709434-04	PBR-26-A-17_SED_003-004CM	T	Percent Solids	61.6	O-04	61.6	J	HT	% BY WT.
1709434	% Solids	1709434-05	PBR-26-A-17_SED_004-005CM	T	Percent Solids	63.4	O-04	63.4	J	HT	% BY WT.
1709434	% Solids	1709434-06	PBR-26-A-17_SED_005-006CM	T	Percent Solids	58.5	O-04	58.5	J	HT	% BY WT.
1709434	% Solids	1709434-07	PBR-26-A-17_SED_006-007CM	T	Percent Solids	62.7	O-04	62.7	J	HT	% BY WT.
1709434	% Solids	1709434-08	PBR-26-A-17_SED_007-008CM	T	Percent Solids	68.1	O-04	68.1	J	HT	% BY WT.
1709434	% Solids	1709434-09	PBR-26-A-17_SED_008-009CM	T	Percent Solids	63.2	O-04	63.2	J	HT	% BY WT.
1709434	% Solids	1709434-10	PBR-26-A-17_SED_009-010CM	T	Percent Solids	68.9	O-04	68.9	J	HT	% BY WT.
1709434	% Solids	1709434-11	PBR-26-A-17_SED_010-011CM	T	Percent Solids	72.6	O-04	72.6	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709434	% Solids	1709434-12	PBR-26-A-17_SED_011-012CM	T	Percent Solids	74	O-04	74	J	HT	% BY WT.
1709434	% Solids	1709434-13	PBR-26-A-17_SED_012-013CM	T	Percent Solids	74	O-04	74	J	HT	% BY WT.
1709434	% Solids	1709434-14	PBR-26-A-17_SED_013-014CM	T	Percent Solids	75.5	O-04	75.5	J	HT	% BY WT.
1709434	% Solids	1709434-15	PBR-26-A-17_SED_014-015CM	T	Percent Solids	75.6	O-04	75.6	J	HT	% BY WT.
1709434	% Solids	1709434-16	PBR-26-A-17_SED_015-016CM	T	Percent Solids	82	O-04	82	J	HT	% BY WT.
1709434	% Solids	1709434-17	PBR-26-A-17_SED_016-017CM	T	Percent Solids	73.3	O-04	73.3	J	HT	% BY WT.
1709434	% Solids	1709434-18	PBR-26-A-17_SED_017-018CM	T	Percent Solids	70.7	O-04	70.7	J	HT	% BY WT.
1709434	% Solids	1709434-19	PBR-26-A-17_SED_018-019CM	T	Percent Solids	70.2	O-04	70.2	J	HT	% BY WT.
1709434	% Solids	1709434-20	PBR-26-A-17_SED_019-020CM	T	Percent Solids	74.8	O-04	74.8	J	HT	% BY WT.
1709434	% Solids	1709434-21	PBR-26-A-17_SED_020-022CM	T	Percent Solids	70.4	O-04	70.4	J	HT	% BY WT.
1709434	% Solids	1709434-22	PBR-26-A-17_SED_022-024CM	T	Percent Solids	67.7	O-04	67.7	J	HT	% BY WT.
1709434	% Solids	1709434-23	PBR-26-A-17_SED_024-026CM	T	Percent Solids	62.8	O-04	62.8	J	HT	% BY WT.
1709434	% Solids	1709434-24	PBR-26-A-17_SED_026-028CM	T	Percent Solids	78.3	O-04	78.3	J	HT	% BY WT.
1709434	% Solids	1709434-25	PBR-26-A-17_SED_028-030CM	T	Percent Solids	62.5	O-04	62.5	J	HT	% BY WT.
1709434	% Solids	1709434-26	PBR-26-A-17_SED_030-032CM	T	Percent Solids	61.5	O-04	61.5	J	HT	% BY WT.
1709434	% Solids	1709434-27	PBR-26-A-17_SED_032-034CM	T	Percent Solids	63.6	O-04	63.6	J	HT	% BY WT.
1709434	% Solids	1709434-28	PBR-26-A-17_SED_034-036CM	T	Percent Solids	66.4	O-04	66.4	J	HT	% BY WT.
1709434	% Solids	1709434-29	PBR-26-A-17_SED_036-038CM	T	Percent Solids	66.8	O-04	66.8	J	HT	% BY WT.
1709434	% Solids	1709434-30	PBR-26-A-17_SED_038-040CM	T	Percent Solids	68.1	O-04	68.1	J	HT	% BY WT.
1709434	% Solids	1709434-31	PBR-26-A-17_SED_040-045CM	T	Percent Solids	67.7	O-04	67.7	J	HT	% BY WT.
1709434	% Solids	1709434-32	PBR-26-A-17_SED_045-050CM	T	Percent Solids	70.7	O-04	70.7	J	HT	% BY WT.
1709434	% Solids	1709434-33	PBR-26-A-17_SED_050-055CM	T	Percent Solids	68.6	O-04	68.6	J	HT	% BY WT.
1709434	% Solids	1709434-34	PBR-26-A-17_SED_055-060CM	T	Percent Solids	67.1	O-04	67.1	J	HT	% BY WT.
1709434	% Solids	1709434-35	PBR-26-A-17_SED_060-065CM	T	Percent Solids	70.2	O-04	70.2	J	HT	% BY WT.
1709434	% Solids	1709434-36	PBR-26-A-17_SED_065-070CM	T	Percent Solids	68.4	O-04	68.4	J	HT	% BY WT.
1709434	% Solids	1709434-37	PBR-26-A-17_SED_070-075CM	T	Percent Solids	65.7	O-04	65.7	J	HT	% BY WT.
1709434	% Solids	1709434-38	PBR-26-A-17_SED_075-080CM	T	Percent Solids	71.3	O-04	71.3	J	HT	% BY WT.

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709434	% Solids	1709434-39	PBR-26-A-17_SED_080-085CM	T	Percent Solids	63	O-04	63	J	HT	% BY WT.
1709434	% Solids	1709434-40	PBR-26-A-17_SED_085-090CM	T	Percent Solids	65	O-04	65	J	HT	% BY WT.
1709835	% Solids	1709835-01	ES-01-C3-17_SED_000-001CM	T	Percent Solids	33.4	O-04	33.4	J	HT	% BY WT.
1709835	% Solids	1709835-02	ES-01-C3-17_SED_001-002CM	T	Percent Solids	33.4	O-04	33.4	J	HT	% BY WT.
1709835	% Solids	1709835-03	ES-01-C3-17_SED_002-003CM	T	Percent Solids	36.9	O-04	36.9	J	HT	% BY WT.
1709835	% Solids	1709835-04	ES-01-C3-17_SED_003-004CM	T	Percent Solids	33.2	O-04	33.2	J	HT	% BY WT.
1709835	% Solids	1709835-05	ES-01-C3-17_SED_004-005CM	T	Percent Solids	38.6	O-04	38.6	J	HT	% BY WT.
1709835	% Solids	1709835-06	ES-01-C3-17_SED_005-006CM	T	Percent Solids	35	O-04	35	J	HT	% BY WT.
1709835	% Solids	1709835-07	ES-01-C3-17_SED_006-007CM	T	Percent Solids	37.4	O-04	37.4	J	HT	% BY WT.
1709835	% Solids	1709835-08	ES-01-C3-17_SED_007-008CM	T	Percent Solids	36.8	O-04	36.8	J	HT	% BY WT.
1709835	% Solids	1709835-09	ES-01-C3-17_SED_008-009CM	T	Percent Solids	36.4	O-04	36.4	J	HT	% BY WT.
1709835	% Solids	1709835-10	ES-01-C3-17_SED_009-010CM	T	Percent Solids	37.6	O-04	37.6	J	HT	% BY WT.
1709835	% Solids	1709835-11	ES-01-C3-17_SED_010-011CM	T	Percent Solids	36.5	O-04	36.5	J	HT	% BY WT.
1709835	% Solids	1709835-12	ES-01-C3-17_SED_011-012CM	T	Percent Solids	37.4	O-04	37.4	J	HT	% BY WT.
1709835	% Solids	1709835-13	ES-01-C3-17_SED_012-013CM	T	Percent Solids	48	O-04	48	J	HT	% BY WT.
1709835	% Solids	1709835-14	ES-01-C3-17_SED_013-014CM	T	Percent Solids	40.4	O-04	40.4	J	HT	% BY WT.
1709835	% Solids	1709835-15	ES-01-C3-17_SED_014-015CM	T	Percent Solids	38.4	O-04	38.4	J	HT	% BY WT.
1709837	% Solids	1709837-01	PBR-20-E-17_SED_015-016CM	T	Percent Solids	50.1	O-04	50.1	J	HT	% BY WT.
1709837	% Solids	1709837-02	PBR-20-E-17_SED_016-017CM	T	Percent Solids	50.8	O-04	50.8	J	HT	% BY WT.
1709837	% Solids	1709837-03	PBR-20-E-17_SED_017-018CM	T	Percent Solids	56	O-04	56	J	HT	% BY WT.
1709837	% Solids	1709837-04	PBR-20-E-17_SED_018-019CM	T	Percent Solids	59.8	O-04	59.8	J	HT	% BY WT.
1709837	% Solids	1709837-05	PBR-20-E-17_SED_019-020CM	T	Percent Solids	60	O-04	60	J	HT	% BY WT.
1709837	% Solids	1709837-06	PBR-20-E-17_SED_020-022CM	T	Percent Solids	62	O-04	62	J	HT	% BY WT.
1709837	% Solids	1709837-07	PBR-20-E-17_SED_022-024CM	T	Percent Solids	63.8	O-04	63.8	J	HT	% BY WT.
1709837	% Solids	1709837-08	PBR-20-E-17_SED_024-026CM	T	Percent Solids	57	O-04	57	J	HT	% BY WT.
1709837	% Solids	1709837-09	PBR-20-E-17_SED_026-028CM	T	Percent Solids	61.6	O-04	61.6	J	HT	% BY WT.
1709837	% Solids	1709837-10	PBR-20-E-17_SED_028-030CM	T	Percent Solids	60.5	O-04	60.5	J	HT	% BY WT.

TABLE 2
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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709837	% Solids	1709837-11	PBR-20-E-17_SED_030-032CM	T	Percent Solids	65.1	O-04	65.1	J	HT	% BY WT.
1709837	% Solids	1709837-12	PBR-20-E-17_SED_032-034CM	T	Percent Solids	65.7	O-04	65.7	J	HT	% BY WT.
1709837	% Solids	1709837-13	PBR-20-E-17_SED_034-036CM	T	Percent Solids	65.9	O-04	65.9	J	HT	% BY WT.
1709837	% Solids	1709837-14	PBR-20-E-17_SED_036-038CM	T	Percent Solids	62.3	O-04	62.3	J	HT	% BY WT.
1709837	% Solids	1709837-15	PBR-20-E-17_SED_038-040CM	T	Percent Solids	57.2	O-04	57.2	J	HT	% BY WT.
1709837	% Solids	1709837-16	PBR-20-E-17_SED_040-045CM	T	Percent Solids	59.9	O-04	59.9	J	HT	% BY WT.
1709837	% Solids	1709837-17	PBR-20-E-17_SED_045-050CM	T	Percent Solids	62.5	O-04	62.5	J	HT	% BY WT.
1709838	% Solids	1709838-01	ES-01-C3-17_SED_015-016CM	T	Percent Solids	41.6	O-04	41.6	J	HT	% BY WT.
1709838	% Solids	1709838-02	ES-01-C3-17_SED_016-017CM	T	Percent Solids	39.7	O-04	39.7	J	HT	% BY WT.
1709838	% Solids	1709838-03	ES-01-C3-17_SED_017-018CM	T	Percent Solids	42.1	O-04	42.1	J	HT	% BY WT.
1709838	% Solids	1709838-04	ES-01-C3-17_SED_018-019CM	T	Percent Solids	41.1	O-04	41.1	J	HT	% BY WT.
1709838	% Solids	1709838-05	ES-01-C3-17_SED_019-020CM	T	Percent Solids	42.3	O-04	42.3	J	HT	% BY WT.
1709838	% Solids	1709838-06	ES-01-C3-17_SED_020-022CM	T	Percent Solids	42.5	O-04	42.5	J	HT	% BY WT.
1709838	% Solids	1709838-07	ES-01-C3-17_SED_022-024CM	T	Percent Solids	43.9	O-04	43.9	J	HT	% BY WT.
1709838	% Solids	1709838-08	ES-01-C3-17_SED_024-026CM	T	Percent Solids	44.6	[1]	44.6	J	HT	% BY WT.
1709838	% Solids	1709838-09	ES-01-C3-17_SED_026-028CM	T	Percent Solids	45.2	[2]	45.2	J	HT	% BY WT.
1709838	% Solids	1709838-10	ES-01-C3-17_SED_028-030CM	T	Percent Solids	43.7	[3]	43.7	J	HT	% BY WT.
1709838	% Solids	1709838-11	ES-01-C3-17_SED_030-032CM	T	Percent Solids	42.9	[4]	42.9	J	HT	% BY WT.
1709838	% Solids	1709838-12	ES-01-C3-17_SED_032-034CM	T	Percent Solids	46.2	[5]	46.2	J	HT	% BY WT.
1709838	% Solids	1709838-13	ES-01-C3-17_SED_034-036CM	T	Percent Solids	45.6	[6]	45.6	J	HT	% BY WT.
1709838	% Solids	1709838-14	ES-01-C3-17_SED_036-038CM	T	Percent Solids	57.1	[7]	57.1	J	HT	% BY WT.
1709838	% Solids	1709838-15	ES-01-C3-17_SED_038-040CM	T	Percent Solids	48.2	[8]	48.2	J	HT	% BY WT.
1709839	% Solids	1709839-01	ES-01-C3-17_SED_040-045CM	T	Percent Solids	47.1	[9]	47.1	J	HT	% BY WT.
1709839	% Solids	1709839-02	ES-01-C3-17_SED_045-050CM	T	Percent Solids	46.2	[10]	46.2	J	HT	% BY WT.
1709839	% Solids	1709839-03	ES-01-C3-17_SED_050-055CM	T	Percent Solids	46.6	[11]	46.6	J	HT	% BY WT.
1709839	% Solids	1709839-04	ES-01-C3-17_SED_055-060CM	T	Percent Solids	47.8	[12]	47.8	J	HT	% BY WT.
1709839	% Solids	1709839-05	ES-01-C3-17_SED_060-065CM	T	Percent Solids	50.9	[13]	50.9	J	HT	% BY WT.

TABLE 2
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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709839	% Solids	1709839-06	ES-01-C3-17_SED_065-070CM	T	Percent Solids	50	[14]	50	J	HT	% BY WT.
1709839	% Solids	1709839-07	ES-01-C3-17_SED_070-075CM	T	Percent Solids	55.6	[15]	55.6	J	HT	% BY WT.
1709839	% Solids	1709839-08	ES-01-C3-17_SED_075-080CM	T	Percent Solids	53.9	[16]	53.9	J	HT	% BY WT.
1709839	% Solids	1709839-09	ES-01-C3-17_SED_080-085CM	T	Percent Solids	53.2	[17]	53.2	J	HT	% BY WT.
1709839	% Solids	1709839-10	ES-01-C3-17_SED_085-090CM	T	Percent Solids	60	[18]	60	J	HT	% BY WT.
1709839	% Solids	1709839-11	ES-01-C3-17_SED_090-095CM	T	Percent Solids	59.7	[19]	59.7	J	HT	% BY WT.
1709839	% Solids	1709839-12	ES-01-C3-17_SED_095-100CM	T	Percent Solids	56	[20]	56	J	HT	% BY WT.
1709839	% Solids	1709839-13	ES-01-C3-17_SED_100-105CM	T	Percent Solids	58.6	[21]	58.6	J	HT	% BY WT.
1709839	% Solids	1709839-14	ES-01-C3-17_SED_105-110CM	T	Percent Solids	65.4	[22]	65.4	J	HT	% BY WT.
1709839	% Solids	1709839-15	ES-01-C3-17_SED_110-115CM	T	Percent Solids	60.5	[23]	60.5	J	HT	% BY WT.
1709839	% Solids	1709839-16	ES-01-C3-17_SED_115-120CM	T	Percent Solids	65.1	[24]	65.1	J	HT	% BY WT.
1709840	% Solids	1709840-01	PBR-20-E-17_SED_000-001CM	T	Percent Solids	53.7	[1]	53.7	J	HT	% BY WT.
1709840	% Solids	1709840-02	PBR-20-E-17_SED_001-002CM	T	Percent Solids	50.2	[2]	50.2	J	HT	% BY WT.
1709840	% Solids	1709840-03	PBR-20-E-17_SED_002-003CM	T	Percent Solids	53.6	[3]	53.6	J	HT	% BY WT.
1709840	% Solids	1709840-04	PBR-20-E-17_SED_003-004CM	T	Percent Solids	56.6	[4]	56.6	J	HT	% BY WT.
1709840	% Solids	1709840-05	PBR-20-E-17_SED_004-005CM	T	Percent Solids	58	[5]	58	J	HT	% BY WT.
1709840	% Solids	1709840-06	PBR-20-E-17_SED_005-006CM	T	Percent Solids	53.5	[6]	53.5	J	HT	% BY WT.
1709840	% Solids	1709840-07	PBR-20-E-17_SED_006-007CM	T	Percent Solids	65.6	[7]	65.6	J	HT	% BY WT.
1709840	% Solids	1709840-08	PBR-20-E-17_SED_007-008CM	T	Percent Solids	60.2	[8]	60.2	J	HT	% BY WT.
1709840	% Solids	1709840-09	PBR-20-E-17_SED_008-009CM	T	Percent Solids	60.6	[9]	60.6	J	HT	% BY WT.
1709840	% Solids	1709840-10	PBR-20-E-17_SED_009-010CM	T	Percent Solids	61.2	[10]	61.2	J	HT	% BY WT.
1709840	% Solids	1709840-11	PBR-20-E-17_SED_010-011CM	T	Percent Solids	60.8	[11]	60.8	J	HT	% BY WT.
1709840	% Solids	1709840-12	PBR-20-E-17_SED_011-012CM	T	Percent Solids	60.4	[12]	60.4	J	HT	% BY WT.
1709840	% Solids	1709840-13	PBR-20-E-17_SED_012-013CM	T	Percent Solids	60.6	[13]	60.6	J	HT	% BY WT.
1709840	% Solids	1709840-14	PBR-20-E-17_SED_013-014CM	T	Percent Solids	57.3	[14]	57.3	J	HT	% BY WT.
1709840	% Solids	1709840-15	PBR-20-E-17_SED_014-015CM	T	Percent Solids	51.6	[15]	51.6	J	HT	% BY WT.
1709841	% Solids	1709841-01	ES-18-B-17_SED_000-001CM	T	Percent Solids	49.1	[1]	49.1	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709841	% Solids	1709841-02	ES-18-B-17_SED_001-002CM	T	Percent Solids	53	[2]	53	J	HT	% BY WT.
1709841	% Solids	1709841-03	ES-18-B-17_SED_002-003CM	T	Percent Solids	50.9	[3]	50.9	J	HT	% BY WT.
1709841	% Solids	1709841-04	ES-18-B-17_SED_003-004CM	T	Percent Solids	51.5	[4]	51.5	J	HT	% BY WT.
1709841	% Solids	1709841-05	ES-18-B-17_SED_004-005CM	T	Percent Solids	50.7	[5]	50.7	J	HT	% BY WT.
1709841	% Solids	1709841-06	ES-18-B-17_SED_005-006CM	T	Percent Solids	49.8	[6]	49.8	J	HT	% BY WT.
1709841	% Solids	1709841-07	ES-18-B-17_SED_006-007CM	T	Percent Solids	52	[7]	52	J	HT	% BY WT.
1709841	% Solids	1709841-08	ES-18-B-17_SED_007-008CM	T	Percent Solids	53.5	[8]	53.5	J	HT	% BY WT.
1709841	% Solids	1709841-09	ES-18-B-17_SED_008-009CM	T	Percent Solids	54.4	[9]	54.4	J	HT	% BY WT.
1709841	% Solids	1709841-10	ES-18-B-17_SED_009-010CM	T	Percent Solids	55.4	[10]	55.4	J	HT	% BY WT.
1709841	% Solids	1709841-11	ES-18-B-17_SED_010-011CM	T	Percent Solids	54.5	[11]	54.5	J	HT	% BY WT.
1709841	% Solids	1709841-12	ES-18-B-17_SED_011-012CM	T	Percent Solids	56.5	[12]	56.5	J	HT	% BY WT.
1709841	% Solids	1709841-13	ES-18-B-17_SED_012-013CM	T	Percent Solids	61.8	[13]	61.8	J	HT	% BY WT.
1709841	% Solids	1709841-14	ES-18-B-17_SED_013-014CM	T	Percent Solids	57.2	[14]	57.2	J	HT	% BY WT.
1709841	% Solids	1709841-15	ES-18-B-17_SED_014-015CM	T	Percent Solids	58.9	[15]	58.9	J	HT	% BY WT.
1709842	% Solids	1709842-01	ES-18-B-17_SED_015-016CM	T	Percent Solids	58.9	[16]	58.9	J	HT	% BY WT.
1709842	% Solids	1709842-02	ES-18-B-17_SED_016-017CM	T	Percent Solids	48.7	[17]	48.7	J	HT	% BY WT.
1709842	% Solids	1709842-03	ES-18-B-17_SED_017-018CM	T	Percent Solids	58.7	[18]	58.7	J	HT	% BY WT.
1709842	% Solids	1709842-04	ES-18-B-17_SED_018-019CM	T	Percent Solids	59.1	[19]	59.1	J	HT	% BY WT.
1709842	% Solids	1709842-05	ES-18-B-17_SED_019-020CM	T	Percent Solids	58.1	[20]	58.1	J	HT	% BY WT.
1709842	% Solids	1709842-06	ES-18-B-17_SED_020-022CM	T	Percent Solids	58.7	[21]	58.7	J	HT	% BY WT.
1709842	% Solids	1709842-07	ES-18-B-17_SED_022-024CM	T	Percent Solids	58.1	O-04	58.1	J	HT	% BY WT.
1709842	% Solids	1709842-08	ES-18-B-17_SED_024-026CM	T	Percent Solids	59.9	O-04	59.9	J	HT	% BY WT.
1709842	% Solids	1709842-09	ES-18-B-17_SED_026-028CM	T	Percent Solids	61.2	O-04	61.2	J	HT	% BY WT.
1709842	% Solids	1709842-10	ES-18-B-17_SED_028-030CM	T	Percent Solids	59.9	O-04	59.9	J	HT	% BY WT.
1709842	% Solids	1709842-11	ES-18-B-17_SED_030-032CM	T	Percent Solids	59.5	O-04	59.5	J	HT	% BY WT.
1709842	% Solids	1709842-12	ES-18-B-17_SED_032-034CM	T	Percent Solids	58.6	O-04	58.6	J	HT	% BY WT.
1709842	% Solids	1709842-13	ES-18-B-17_SED_034-036CM	T	Percent Solids	57.7	O-04	57.7	J	HT	% BY WT.

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709842	% Solids	1709842-14	ES-18-B-17_SED_036-038CM	T	Percent Solids	58.9	O-04	58.9	J	HT	% BY WT.
1709842	% Solids	1709842-15	ES-18-B-17_SED_038-040CM	T	Percent Solids	60.3	O-04	60.3	J	HT	% BY WT.
1709844	% Solids	1709844-01	PBR-18-E-17_SED_015-016CM	T	Percent Solids	38.8	O-04	38.8	J	HT	% BY WT.
1709844	% Solids	1709844-02	PBR-18-E-17_SED_016-017CM	T	Percent Solids	35.2	O-04	35.2	J	HT	% BY WT.
1709844	% Solids	1709844-03	PBR-18-E-17_SED_017-018CM	T	Percent Solids	35	O-04	35	J	HT	% BY WT.
1709844	% Solids	1709844-04	PBR-18-E-17_SED_018-019CM	T	Percent Solids	36	O-04	36	J	HT	% BY WT.
1709844	% Solids	1709844-05	PBR-18-E-17_SED_019-020CM	T	Percent Solids	36.9	O-04	36.9	J	HT	% BY WT.
1709844	% Solids	1709844-06	PBR-18-E-17_SED_020-022CM	T	Percent Solids	39.8	O-04	39.8	J	HT	% BY WT.
1709844	% Solids	1709844-07	PBR-18-E-17_SED_022-024CM	T	Percent Solids	36.6	O-04	36.6	J	HT	% BY WT.
1709844	% Solids	1709844-08	PBR-18-E-17_SED_024-026CM	T	Percent Solids	37.8	O-04	37.8	J	HT	% BY WT.
1709844	% Solids	1709844-09	PBR-18-E-17_SED_026-028CM	T	Percent Solids	36.6	O-04	36.6	J	HT	% BY WT.
1709844	% Solids	1709844-10	PBR-18-E-17_SED_028-030CM	T	Percent Solids	37.2	O-04	37.2	J	HT	% BY WT.
1709844	% Solids	1709844-11	PBR-18-E-17_SED_030-032CM	T	Percent Solids	35.4	O-04	35.4	J	HT	% BY WT.
1709844	% Solids	1709844-12	PBR-18-E-17_SED_032-034CM	T	Percent Solids	35.9	O-04	35.9	J	HT	% BY WT.
1709844	% Solids	1709844-13	PBR-18-E-17_SED_034-036CM	T	Percent Solids	31	O-04	31	J	HT	% BY WT.
1709844	% Solids	1709844-14	PBR-18-E-17_SED_036-038CM	T	Percent Solids	36.3	O-04	36.3	J	HT	% BY WT.
1709844	% Solids	1709844-15	PBR-18-E-17_SED_038-040CM	T	Percent Solids	38.8	O-04	38.8	J	HT	% BY WT.
1709844	% Solids	1709844-16	PBR-18-E-17_SED_040-045CM	T	Percent Solids	45.1	O-04	45.1	J	HT	% BY WT.
1709844	% Solids	1709844-17	PBR-18-E-17_SED_045-050CM	T	Percent Solids	46.7	O-04	46.7	J	HT	% BY WT.
1709844	% Solids	1709844-18	PBR-18-E-17_SED_050-055CM	T	Percent Solids	39.4	O-04	39.4	J	HT	% BY WT.
1709844	% Solids	1709844-19	PBR-18-E-17_SED_055-060CM	T	Percent Solids	43.8	O-04	43.8	J	HT	% BY WT.
1709845	% Solids	1709845-01	ES-18-B-17_SED_040-045CM	T	Percent Solids	63.2	O-04	63.2	J	HT	% BY WT.
1709845	% Solids	1709845-02	ES-18-B-17_SED_045-050CM	T	Percent Solids	59.5	O-04	59.5	J	HT	% BY WT.
1709845	% Solids	1709845-03	ES-18-B-17_SED_050-055CM	T	Percent Solids	56.2	O-04	56.2	J	HT	% BY WT.
1709845	% Solids	1709845-04	ES-18-B-17_SED_055-060CM	T	Percent Solids	58	O-04	58	J	HT	% BY WT.
1709845	% Solids	1709845-05	ES-18-B-17_SED_060-065CM	T	Percent Solids	62.5	O-04	62.5	J	HT	% BY WT.
1709845	% Solids	1709845-06	ES-18-B-17_SED_065-070CM	T	Percent Solids	62.4	O-04	62.4	J	HT	% BY WT.
1709845	% Solids	1709845-07	ES-18-B-17_SED_070-075CM	T	Percent Solids	63.3	O-04	63.3	J	HT	% BY WT.

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710292	% Solids	1710292-01	MM-T2-C1-B-17_SED_000-001CM	T	Percent Solids	15.8	[1]	15.8	J	HT	% BY WT.
1710292	% Solids	1710292-02	MM-T2-C1-B-17_SED_001-002CM	T	Percent Solids	13.8	[2]	13.8	J	HT	% BY WT.
1710292	% Solids	1710292-03	MM-T2-C1-B-17_SED_002-003CM	T	Percent Solids	14.4	[3]	14.4	J	HT	% BY WT.
1710292	% Solids	1710292-04	MM-T2-C1-B-17_SED_003-004CM	T	Percent Solids	15.9	[4]	15.9	J	HT	% BY WT.
1710292	% Solids	1710292-05	MM-T2-C1-B-17_SED_004-005CM	T	Percent Solids	18.5	[5]	18.5	J	HT	% BY WT.
1710292	% Solids	1710292-06	MM-T2-C1-B-17_SED_005-006CM	T	Percent Solids	16.4	[6]	16.4	J	HT	% BY WT.
1710292	% Solids	1710292-07	MM-T2-C1-B-17_SED_006-007CM	T	Percent Solids	20	[7]	20	J	HT	% BY WT.
1710292	% Solids	1710292-08	MM-T2-C1-B-17_SED_007-008CM	T	Percent Solids	18	[8]	18	J	HT	% BY WT.
1710292	% Solids	1710292-09	MM-T2-C1-B-17_SED_008-009CM	T	Percent Solids	17	[9]	17	J	HT	% BY WT.
1710292	% Solids	1710292-10	MM-T2-C1-B-17_SED_009-010CM	T	Percent Solids	18.2	[10]	18.2	J	HT	% BY WT.
1710292	% Solids	1710292-11	MM-T2-C1-B-17_SED_010-011CM	T	Percent Solids	17.5	[11]	17.5	J	HT	% BY WT.
1710292	% Solids	1710292-12	MM-T2-C1-B-17_SED_011-012CM	T	Percent Solids	19	[12]	19	J	HT	% BY WT.
1710292	% Solids	1710292-13	MM-T2-C1-B-17_SED_012-013CM	T	Percent Solids	18.7	[13]	18.7	J	HT	% BY WT.
1710292	% Solids	1710292-14	MM-T2-C1-B-17_SED_013-014CM	T	Percent Solids	18	[14]	18	J	HT	% BY WT.
1710292	% Solids	1710292-15	MM-T2-C1-B-17_SED_014-015CM	T	Percent Solids	17.4	[15]	17.4	J	HT	% BY WT.
1710292	% Solids	1710292-16	MM-T2-C1-B-17_SED_015-016CM	T	Percent Solids	16.8	[16]	16.8	J	HT	% BY WT.
1710292	% Solids	1710292-17	MM-T2-C1-B-17_SED_016-017CM	T	Percent Solids	16.4	[17]	16.4	J	HT	% BY WT.
1710292	% Solids	1710292-18	MM-T2-C1-B-17_SED_017-018CM	T	Percent Solids	17.7	[18]	17.7	J	HT	% BY WT.
1710292	% Solids	1710292-19	MM-T2-C1-B-17_SED_018-019CM	T	Percent Solids	17.2	[19]	17.2	J	HT	% BY WT.
1710292	% Solids	1710292-20	MM-T2-C1-B-17_SED_019-020CM	T	Percent Solids	17.6	[20]	17.6	J	HT	% BY WT.
1710292	% Solids	1710292-21	MM-T2-C1-B-17_SED_020-022CM	T	Percent Solids	18.2	[21]	18.2	J	HT	% BY WT.
1710292	% Solids	1710292-22	MM-T2-C1-B-17_SED_022-024CM	T	Percent Solids	18.1	[22]	18.1	J	HT	% BY WT.
1710292	% Solids	1710292-23	MM-T2-C1-B-17_SED_024-026CM	T	Percent Solids	20.7	[23]	20.7	J	HT	% BY WT.
1710292	% Solids	1710292-24	MM-T2-C1-B-17_SED_026-028CM	T	Percent Solids	19.2	[24]	19.2	J	HT	% BY WT.
1710292	% Solids	1710292-25	MM-T2-C1-B-17_SED_028-030CM	T	Percent Solids	20.8	[25]	20.8	J	HT	% BY WT.
1710292	% Solids	1710292-26	MM-T2-C1-B-17_SED_030-032CM	T	Percent Solids	22	[26]	22	J	HT	% BY WT.
1710292	% Solids	1710292-27	MM-T2-C1-B-17_SED_032-034CM	T	Percent Solids	23.2	[27]	23.2	J	HT	% BY WT.

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710292	% Solids	1710292-28	MM-T2-C1-B-17_SED_034-036CM	T	Percent Solids	28.2	[28]	28.2	J	HT	% BY WT.
1710292	% Solids	1710292-29	MM-T2-C1-B-17_SED_036-038CM	T	Percent Solids	32.3	[29]	32.3	J	HT	% BY WT.
1710292	% Solids	1710292-30	MM-T2-C1-B-17_SED_038-040CM	T	Percent Solids	28	[30]	28	J	HT	% BY WT.
1710292	% Solids	1710292-31	MM-T2-C1-B-17_SED_040-045CM	T	Percent Solids	29.7	[31]	29.7	J	HT	% BY WT.
1710292	% Solids	1710292-32	MM-T2-C1-B-17_SED_045-050CM	T	Percent Solids	48.4	[32]	48.4	J	HT	% BY WT.
1710292	% Solids	1710292-33	MM-T2-C1-B-17_SED_050-055CM	T	Percent Solids	50.5	[33]	50.5	J	HT	% BY WT.
1710292	% Solids	1710292-34	MM-T2-C1-B-17_SED_055-060CM	T	Percent Solids	43.9	[34]	43.9	J	HT	% BY WT.
1710292	% Solids	1710292-35	MM-T2-C1-B-17_SED_060-065CM	T	Percent Solids	31.3	[35]	31.3	J	HT	% BY WT.
1710292	% Solids	1710292-36	MM-T2-C1-B-17_SED_065-070CM	T	Percent Solids	35.4	[36]	35.4	J	HT	% BY WT.
1710292	% Solids	1710292-37	MM-T2-C1-B-17_SED_070-075CM	T	Percent Solids	41	[37]	41	J	HT	% BY WT.
1710292	% Solids	1710292-38	MM-T2-C1-B-17_SED_075-080CM	T	Percent Solids	42	[38]	42	J	HT	% BY WT.
1710292	% Solids	1710292-39	MM-T2-C1-B-17_SED_080-085CM	T	Percent Solids	41.8	[39]	41.8	J	HT	% BY WT.
1710318	% Solids	1710318-01	UPB-MU11-GC-1-C2-17_SED_000-001CM	T	Percent Solids	32.9	O-04	32.9	J	HT	% BY WT.
1710318	% Solids	1710318-02	UPB-MU11-GC-1-C2-17_SED_001-002CM	T	Percent Solids	35.1	O-04	35.1	J	HT	% BY WT.
1710318	% Solids	1710318-03	UPB-MU11-GC-1-C2-17_SED_002-003CM	T	Percent Solids	40.3	O-04	40.3	J	HT	% BY WT.
1710318	% Solids	1710318-04	UPB-MU11-GC-1-C2-17_SED_003-004CM	T	Percent Solids	40.5	O-04	40.5	J	HT	% BY WT.
1710318	% Solids	1710318-05	UPB-MU11-GC-1-C2-17_SED_004-005CM	T	Percent Solids	37.4	O-04	37.4	J	HT	% BY WT.
1710318	% Solids	1710318-06	UPB-MU11-GC-1-C2-17_SED_005-006CM	T	Percent Solids	36.3	O-04	36.3	J	HT	% BY WT.
1710318	% Solids	1710318-07	UPB-MU11-GC-1-C2-17_SED_006-007CM	T	Percent Solids	38.2	O-04	38.2	J	HT	% BY WT.
1710318	% Solids	1710318-08	UPB-MU11-GC-1-C2-17_SED_007-008CM	T	Percent Solids	40.2	O-04	40.2	J	HT	% BY WT.
1710318	% Solids	1710318-09	UPB-MU11-GC-1-C2-17_SED_008-009CM	T	Percent Solids	33	O-04	33	J	HT	% BY WT.
1710318	% Solids	1710318-10	UPB-MU11-GC-1-C2-17_SED_009-010CM	T	Percent Solids	32.7	O-04	32.7	J	HT	% BY WT.
1710318	% Solids	1710318-11	UPB-MU11-GC-1-C2-17_SED_010-011CM	T	Percent Solids	37.6	O-04	37.6	J	HT	% BY WT.
1710318	% Solids	1710318-12	UPB-MU11-GC-1-C2-17_SED_011-012CM	T	Percent Solids	49.4	O-04	49.4	J	HT	% BY WT.
1710318	% Solids	1710318-13	UPB-MU11-GC-1-C2-17_SED_012-013CM	T	Percent Solids	47.1	O-04	47.1	J	HT	% BY WT.
1710318	% Solids	1710318-14	UPB-MU11-GC-1-C2-17_SED_013-014CM	T	Percent Solids	43.1	O-04	43.1	J	HT	% BY WT.
1710318	% Solids	1710318-15	UPB-MU11-GC-1-C2-17_SED_014-015CM	T	Percent Solids	43.6	O-04	43.6	J	HT	% BY WT.

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710318	% Solids	1710318-16	UPB-MU11-GC-1-C2-17_SED_015-016CM	T	Percent Solids	44	O-04	44	J	HT	% BY WT.
1710318	% Solids	1710318-17	UPB-MU11-GC-1-C2-17_SED_016-017CM	T	Percent Solids	40.8	O-04	40.8	J	HT	% BY WT.
1710318	% Solids	1710318-18	UPB-MU11-GC-1-C2-17_SED_017-018CM	T	Percent Solids	38.1	O-04	38.1	J	HT	% BY WT.
1710318	% Solids	1710318-19	UPB-MU11-GC-1-C2-17_SED_018-019CM	T	Percent Solids	36.1	O-04	36.1	J	HT	% BY WT.
1710318	% Solids	1710318-20	UPB-MU11-GC-1-C2-17_SED_019-020CM	T	Percent Solids	32.9	O-04	32.9	J	HT	% BY WT.
1710318	% Solids	1710318-21	UPB-MU11-GC-1-C2-17_SED_020-022CM	T	Percent Solids	33.7	O-04	33.7	J	HT	% BY WT.
1710318	% Solids	1710318-22	UPB-MU11-GC-1-C2-17_SED_022-024CM	T	Percent Solids	41.1	O-04	41.1	J	HT	% BY WT.
1710318	% Solids	1710318-23	UPB-MU11-GC-1-C2-17_SED_024-026CM	T	Percent Solids	42.4	O-04	42.4	J	HT	% BY WT.
1710318	% Solids	1710318-24	UPB-MU11-GC-1-C2-17_SED_026-028CM	T	Percent Solids	34.8	O-04	34.8	J	HT	% BY WT.
1710318	% Solids	1710318-25	UPB-MU11-GC-1-C2-17_SED_028-030CM	T	Percent Solids	35.8	O-04	35.8	J	HT	% BY WT.
1710318	% Solids	1710318-26	UPB-MU11-GC-1-C2-17_SED_030-032CM	T	Percent Solids	36.8	O-04	36.8	J	HT	% BY WT.
1710318	% Solids	1710318-27	UPB-MU11-GC-1-C2-17_SED_032-034CM	T	Percent Solids	41.2	O-04	41.2	J	HT	% BY WT.
1710318	% Solids	1710318-28	UPB-MU11-GC-1-C2-17_SED_034-036CM	T	Percent Solids	35.1	O-04	35.1	J	HT	% BY WT.
1710318	% Solids	1710318-29	UPB-MU11-GC-1-C2-17_SED_036-038CM	T	Percent Solids	43.1	O-04	43.1	J	HT	% BY WT.
1710318	% Solids	1710318-30	UPB-MU11-GC-1-C2-17_SED_038-040CM	T	Percent Solids	37.9	O-04	37.9	J	HT	% BY WT.
1710318	% Solids	1710318-31	UPB-MU11-GC-1-C2-17_SED_040-045CM	T	Percent Solids	39.5	O-04	39.5	J	HT	% BY WT.
1710318	% Solids	1710318-32	UPB-MU11-GC-1-C2-17_SED_045-050CM	T	Percent Solids	38.7	O-04	38.7	J	HT	% BY WT.
1710318	% Solids	1710318-33	UPB-MU11-GC-1-C2-17_SED_050-055CM	T	Percent Solids	37.1	O-04	37.1	J	HT	% BY WT.
1710318	% Solids	1710318-34	UPB-MU11-GC-1-C2-17_SED_055-060CM	T	Percent Solids	40.1	O-04	40.1	J	HT	% BY WT.
1710318	% Solids	1710318-35	UPB-MU11-GC-1-C2-17_SED_060-065CM	T	Percent Solids	41.2	O-04	41.2	J	HT	% BY WT.
1710318	% Solids	1710318-36	UPB-MU11-GC-1-C2-17_SED_065-070CM	T	Percent Solids	42	O-04	42	J	HT	% BY WT.
1710318	% Solids	1710318-37	UPB-MU11-GC-1-C2-17_SED_070-075CM	T	Percent Solids	43.5	O-04	43.5	J	HT	% BY WT.
1710318	% Solids	1710318-38	UPB-MU11-GC-1-C2-17_SED_075-080CM	T	Percent Solids	41.3	O-04	41.3	J	HT	% BY WT.
1710318	% Solids	1710318-39	UPB-MU11-GC-1-C2-17_SED_080-085CM	T	Percent Solids	42.2	O-04	42.2	J	HT	% BY WT.
1710318	% Solids	1710318-40	UPB-MU11-GC-1-C2-17_SED_085-090CM	T	Percent Solids	37	O-04	37	J	HT	% BY WT.
1710318	% Solids	1710318-41	UPB-MU11-GC-1-C2-17_SED_090-095CM	T	Percent Solids	37.8	O-04	37.8	J	HT	% BY WT.
1710318	% Solids	1710318-42	UPB-MU11-GC-1-C2-17_SED_095-100CM	T	Percent Solids	41.6	O-04	41.6	J	HT	% BY WT.
1710318	% Solids	1710318-43	UPB-MU11-GC-1-C2-17_SED_100-105CM	T	Percent Solids	36.9	O-04	36.9	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710322	% Solids	1710322-01	VN-MU3-GC-1-D-17_SED_000-001CM	T	Percent Solids	42.1	O-04	42.1	J	HT	% BY WT.
1710322	% Solids	1710322-02	VN-MU3-GC-1-D-17_SED_001-002CM	T	Percent Solids	46.1	O-04	46.1	J	HT	% BY WT.
1710322	% Solids	1710322-03	VN-MU3-GC-1-D-17_SED_002-003CM	T	Percent Solids	49.1	O-04	49.1	J	HT	% BY WT.
1710322	% Solids	1710322-04	VN-MU3-GC-1-D-17_SED_003-004CM	T	Percent Solids	48.8	O-04	48.8	J	HT	% BY WT.
1710322	% Solids	1710322-05	VN-MU3-GC-1-D-17_SED_004-005CM	T	Percent Solids	50	O-04	50	J	HT	% BY WT.
1710322	% Solids	1710322-06	VN-MU3-GC-1-D-17_SED_005-006CM	T	Percent Solids	50.1	O-04	50.1	J	HT	% BY WT.
1710322	% Solids	1710322-07	VN-MU3-GC-1-D-17_SED_006-007CM	T	Percent Solids	48.7	O-04	48.7	J	HT	% BY WT.
1710322	% Solids	1710322-08	VN-MU3-GC-1-D-17_SED_007-008CM	T	Percent Solids	45.9	O-04	45.9	J	HT	% BY WT.
1710322	% Solids	1710322-09	VN-MU3-GC-1-D-17_SED_008-009CM	T	Percent Solids	45.7	O-04	45.7	J	HT	% BY WT.
1710322	% Solids	1710322-10	VN-MU3-GC-1-D-17_SED_009-010CM	T	Percent Solids	46.5	O-04	46.5	J	HT	% BY WT.
1710322	% Solids	1710322-11	VN-MU3-GC-1-D-17_SED_010-011CM	T	Percent Solids	86.9	O-04	86.9	J	HT	% BY WT.
1710322	% Solids	1710322-12	VN-MU3-GC-1-D-17_SED_011-012CM	T	Percent Solids	44.4	O-04	44.4	J	HT	% BY WT.
1710322	% Solids	1710322-13	VN-MU3-GC-1-D-17_SED_012-013CM	T	Percent Solids	48.3	O-04	48.3	J	HT	% BY WT.
1710322	% Solids	1710322-14	VN-MU3-GC-1-D-17_SED_013-014CM	T	Percent Solids	50.5	O-04	50.5	J	HT	% BY WT.
1710322	% Solids	1710322-15	VN-MU3-GC-1-D-17_SED_014-015CM	T	Percent Solids	51	O-04	51	J	HT	% BY WT.
1710322	% Solids	1710322-16	VN-MU3-GC-1-D-17_SED_015-016CM	T	Percent Solids	52.5	O-04	52.5	J	HT	% BY WT.
1710322	% Solids	1710322-17	VN-MU3-GC-1-D-17_SED_016-017CM	T	Percent Solids	50.2	O-04	50.2	J	HT	% BY WT.
1710322	% Solids	1710322-18	VN-MU3-GC-1-D-17_SED_017-018CM	T	Percent Solids	54.1	O-04	54.1	J	HT	% BY WT.
1710322	% Solids	1710322-19	VN-MU3-GC-1-D-17_SED_018-019CM	T	Percent Solids	53.3	O-04	53.3	J	HT	% BY WT.
1710322	% Solids	1710322-20	VN-MU3-GC-1-D-17_SED_019-020CM	T	Percent Solids	54.7	O-04	54.7	J	HT	% BY WT.
1710322	% Solids	1710322-21	VN-MU3-GC-1-D-17_SED_020-022CM	T	Percent Solids	52.3	O-04	52.3	J	HT	% BY WT.
1710322	% Solids	1710322-22	VN-MU3-GC-1-D-17_SED_022-024CM	T	Percent Solids	52.7	O-04	52.7	J	HT	% BY WT.
1710322	% Solids	1710322-23	VN-MU3-GC-1-D-17_SED_024-026CM	T	Percent Solids	52.4	O-04	52.4	J	HT	% BY WT.
1710322	% Solids	1710322-24	VN-MU3-GC-1-D-17_SED_026-028CM	T	Percent Solids	52.3	O-04	52.3	J	HT	% BY WT.
1710322	% Solids	1710322-25	VN-MU3-GC-1-D-17_SED_028-030CM	T	Percent Solids	55.3	O-04	55.3	J	HT	% BY WT.
1710322	% Solids	1710322-26	VN-MU3-GC-1-D-17_SED_030-032CM	T	Percent Solids	58	O-04	58	J	HT	% BY WT.
1710322	% Solids	1710322-27	VN-MU3-GC-1-D-17_SED_032-034CM	T	Percent Solids	56.4	O-04	56.4	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710322	% Solids	1710322-28	VN-MU3-GC-1-D-17_SED_034-036CM	T	Percent Solids	60.1	O-04	60.1	J	HT	% BY WT.
1710322	% Solids	1710322-29	VN-MU3-GC-1-D-17_SED_036-038CM	T	Percent Solids	58.2	O-04	58.2	J	HT	% BY WT.
1710322	% Solids	1710322-30	VN-MU3-GC-1-D-17_SED_038-040CM	T	Percent Solids	57.4	O-04	57.4	J	HT	% BY WT.
1710322	% Solids	1710322-31	VN-MU3-GC-1-D-17_SED_040-045CM	T	Percent Solids	58.8	O-04	58.8	J	HT	% BY WT.
1710322	% Solids	1710322-32	VN-MU3-GC-1-D-17_SED_045-050CM	T	Percent Solids	54.3	O-04	54.3	J	HT	% BY WT.
1710322	% Solids	1710322-33	VN-MU3-GC-1-D-17_SED_050-055CM	T	Percent Solids	52.4	O-04	52.4	J	HT	% BY WT.
1710322	% Solids	1710322-34	VN-MU3-GC-1-D-17_SED_055-060CM	T	Percent Solids	56.3		56.3	J	HT	% BY WT.
1710322	% Solids	1710322-35	VN-MU3-GC-1-D-17_SED_060-065CM	T	Percent Solids	71.5	O-04	71.5	J	HT	% BY WT.
1710322	% Solids	1710322-36	VN-MU3-GC-1-D-17_SED_065-070CM	T	Percent Solids	71.9	O-04	71.9	J	HT	% BY WT.
1710322	% Solids	1710322-37	VN-MU3-GC-1-D-17_SED_070-075CM	T	Percent Solids	70.5	O-04	70.5	J	HT	% BY WT.
1710322	% Solids	1710322-38	VN-MU3-GC-1-D-17_SED_075-080CM	T	Percent Solids	69.3	O-04	69.3	J	HT	% BY WT.
1710322	% Solids	1710322-39	VN-MU3-GC-1-D-17_SED_080-085CM	T	Percent Solids	68	O-04	68	J	HT	% BY WT.
1710322	% Solids	1710322-40	VN-MU3-GC-1-D-17_SED_085-090CM	T	Percent Solids	68.5	O-04	68.5	J	HT	% BY WT.
1710322	% Solids	1710322-41	VN-MU3-GC-1-D-17_SED_090-095CM	T	Percent Solids	67.8	O-04	67.8	J	HT	% BY WT.
1710322	% Solids	1710322-42	VN-MU3-GC-1-D-17_SED_095-100CM	T	Percent Solids	69.8	O-04	69.8	J	HT	% BY WT.
1710322	% Solids	1710322-43	VN-MU3-GC-1-D-17_SED_100-105CM	T	Percent Solids	68.8	O-04	68.8	J	HT	% BY WT.
1710322	% Solids	1710322-44	VN-MU3-GC-1-D-17_SED_105-110CM	T	Percent Solids	68.8	O-04	68.8	J	HT	% BY WT.
1710323	% Solids	1710323-01	VE-MU4-GC-1-E-17_SED_000-001CM	T	Percent Solids	33.1	O-04	33.1	J	HT	% BY WT.
1710323	% Solids	1710323-02	VE-MU4-GC-1-E-17_SED_001-002CM	T	Percent Solids	34	O-04	34	J	HT	% BY WT.
1710323	% Solids	1710323-03	VE-MU4-GC-1-E-17_SED_002-003CM	T	Percent Solids	38	O-04	38	J	HT	% BY WT.
1710323	% Solids	1710323-04	VE-MU4-GC-1-E-17_SED_003-004CM	T	Percent Solids	42.7	O-04	42.7	J	HT	% BY WT.
1710323	% Solids	1710323-05	VE-MU4-GC-1-E-17_SED_004-005CM	T	Percent Solids	47.8	[1]	47.8	J	HT	% BY WT.
1710323	% Solids	1710323-06	VE-MU4-GC-1-E-17_SED_005-006CM	T	Percent Solids	50.4	[2]	50.4	J	HT	% BY WT.
1710323	% Solids	1710323-07	VE-MU4-GC-1-E-17_SED_006-007CM	T	Percent Solids	54.2	[3]	54.2	J	HT	% BY WT.
1710323	% Solids	1710323-08	VE-MU4-GC-1-E-17_SED_007-008CM	T	Percent Solids	53.2	[4]	53.2	J	HT	% BY WT.
1710323	% Solids	1710323-09	VE-MU4-GC-1-E-17_SED_008-009CM	T	Percent Solids	60.7	[5]	60.7	J	HT	% BY WT.
1710323	% Solids	1710323-10	VE-MU4-GC-1-E-17_SED_009-010CM	T	Percent Solids	63.7	[6]	63.7	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710323	% Solids	1710323-11	VE-MU4-GC-1-E-17_SED_010-011CM	T	Percent Solids	65.7	[7]	65.7	J	HT	% BY WT.
1710323	% Solids	1710323-12	VE-MU4-GC-1-E-17_SED_011-012CM	T	Percent Solids	67.3	[8]	67.3	J	HT	% BY WT.
1710323	% Solids	1710323-13	VE-MU4-GC-1-E-17_SED_012-013CM	T	Percent Solids	69.1	[9]	69.1	J	HT	% BY WT.
1710323	% Solids	1710323-14	VE-MU4-GC-1-E-17_SED_013-014CM	T	Percent Solids	70	[10]	70	J	HT	% BY WT.
1710323	% Solids	1710323-15	VE-MU4-GC-1-E-17_SED_014-015CM	T	Percent Solids	69.9	[11]	69.9	J	HT	% BY WT.
1710323	% Solids	1710323-16	VE-MU4-GC-1-E-17_SED_015-016CM	T	Percent Solids	70.7	[12]	70.7	J	HT	% BY WT.
1710323	% Solids	1710323-17	VE-MU4-GC-1-E-17_SED_016-017CM	T	Percent Solids	70.1	[13]	70.1	J	HT	% BY WT.
1710323	% Solids	1710323-18	VE-MU4-GC-1-E-17_SED_017-018CM	T	Percent Solids	70.9	[14]	70.9	J	HT	% BY WT.
1710323	% Solids	1710323-19	VE-MU4-GC-1-E-17_SED_018-019CM	T	Percent Solids	71	[15]	71	J	HT	% BY WT.
1710323	% Solids	1710323-20	VE-MU4-GC-1-E-17_SED_019-020CM	T	Percent Solids	70.1	[16]	70.1	J	HT	% BY WT.
1710323	% Solids	1710323-21	VE-MU4-GC-1-E-17_SED_020-022CM	T	Percent Solids	70.4	[17]	70.4	J	HT	% BY WT.
1710323	% Solids	1710323-22	VE-MU4-GC-1-E-17_SED_022-024CM	T	Percent Solids	68.8	[18]	68.8	J	HT	% BY WT.
1710323	% Solids	1710323-23	VE-MU4-GC-1-E-17_SED_024-026CM	T	Percent Solids	69.5	[19]	69.5	J	HT	% BY WT.
1710323	% Solids	1710323-24	VE-MU4-GC-1-E-17_SED_026-028CM	T	Percent Solids	72.3	[20]	72.3	J	HT	% BY WT.
1710323	% Solids	1710323-25	VE-MU4-GC-1-E-17_SED_028-030CM	T	Percent Solids	72	O-04	72	J	HT	% BY WT.
1710323	% Solids	1710323-26	VE-MU4-GC-1-E-17_SED_030-032CM	T	Percent Solids	70.8	O-04	70.8	J	HT	% BY WT.
1710323	% Solids	1710323-27	VE-MU4-GC-1-E-17_SED_032-034CM	T	Percent Solids	73.5	O-04	73.5	J	HT	% BY WT.
1710323	% Solids	1710323-28	VE-MU4-GC-1-E-17_SED_034-036CM	T	Percent Solids	75.5	O-04	75.5	J	HT	% BY WT.
1710323	% Solids	1710323-29	VE-MU4-GC-1-E-17_SED_036-038CM	T	Percent Solids	78	O-04	78	J	HT	% BY WT.
1710323	% Solids	1710323-30	VE-MU4-GC-1-E-17_SED_038-040CM	T	Percent Solids	76.2	O-04	76.2	J	HT	% BY WT.
1710323	% Solids	1710323-31	VE-MU4-GC-1-E-17_SED_040-045CM	T	Percent Solids	75.9	O-04	75.9	J	HT	% BY WT.
1710323	% Solids	1710323-32	VE-MU4-GC-1-E-17_SED_045-050CM	T	Percent Solids	74.8	O-04	74.8	J	HT	% BY WT.
1710323	% Solids	1710323-33	VE-MU4-GC-1-E-17_SED_050-055CM	T	Percent Solids	75.8	O-04	75.8	J	HT	% BY WT.
1710323	% Solids	1710323-34	VE-MU4-GC-1-E-17_SED_055-060CM	T	Percent Solids	77	O-04	77	J	HT	% BY WT.
1710323	% Solids	1710323-35	VE-MU4-GC-1-E-17_SED_060-065CM	T	Percent Solids	82.7	O-04	82.7	J	HT	% BY WT.
1710903	% Solids	1710903-01	FF-MU7-GC-1-B-17_SED_000-001CM	T	Percent Solids	51.1	[1]	51.1	J	HT	% BY WT.
1710903	% Solids	1710903-02	FF-MU7-GC-1-B-17_SED_001-002CM	T	Percent Solids	71	[2]	71	J	HT	% BY WT.

TABLE 2
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710903	% Solids	1710903-03	FF-MU7-GC-1-B-17_SED_002-003CM	T	Percent Solids	75.9	[3]	75.9	J	HT	% BY WT.
1710903	% Solids	1710903-04	FF-MU7-GC-1-B-17_SED_003-004CM	T	Percent Solids	79.9	[4]	79.9	J	HT	% BY WT.
1710903	% Solids	1710903-05	FF-MU7-GC-1-B-17_SED_004-005CM	T	Percent Solids	83.2	[5]	83.2	J	HT	% BY WT.
1710903	% Solids	1710903-06	FF-MU7-GC-1-B-17_SED_005-006CM	T	Percent Solids	83.5	[6]	83.5	J	HT	% BY WT.
1710903	% Solids	1710903-07	FF-MU7-GC-1-B-17_SED_006-007CM	T	Percent Solids	82	[7]	82	J	HT	% BY WT.
1710903	% Solids	1710903-08	FF-MU7-GC-1-B-17_SED_007-008CM	T	Percent Solids	79.1	[8]	79.1	J	HT	% BY WT.
1710903	% Solids	1710903-09	FF-MU7-GC-1-B-17_SED_008-009CM	T	Percent Solids	81.1	[9]	81.1	J	HT	% BY WT.
1710903	% Solids	1710903-10	FF-MU7-GC-1-B-17_SED_009-010CM	T	Percent Solids	83.1	[10]	83.1	J	HT	% BY WT.
1710903	% Solids	1710903-11	FF-MU7-GC-1-B-17_SED_010-011CM	T	Percent Solids	82.4	[11]	82.4	J	HT	% BY WT.
1710903	% Solids	1710903-12	FF-MU7-GC-1-B-17_SED_011-012CM	T	Percent Solids	82.4	[12]	82.4	J	HT	% BY WT.
1710903	% Solids	1710903-13	FF-MU7-GC-1-B-17_SED_012-013CM	T	Percent Solids	78.3	[13]	78.3	J	HT	% BY WT.
1710903	% Solids	1710903-14	FF-MU7-GC-1-B-17_SED_013-014CM	T	Percent Solids	82.1	[14]	82.1	J	HT	% BY WT.
1710903	% Solids	1710903-15	FF-MU7-GC-1-B-17_SED_014-015CM	T	Percent Solids	77.6	[15]	77.6	J	HT	% BY WT.
1710903	% Solids	1710903-16	FF-MU7-GC-1-B-17_SED_015-016CM	T	Percent Solids	75.8	[16]	75.8	J	HT	% BY WT.
1710903	% Solids	1710903-17	FF-MU7-GC-1-B-17_SED_016-017CM	T	Percent Solids	76	[17]	76	J	HT	% BY WT.
1710903	% Solids	1710903-18	FF-MU7-GC-1-B-17_SED_017-018CM	T	Percent Solids	75	[18]	75	J	HT	% BY WT.
1710903	% Solids	1710903-19	FF-MU7-GC-1-B-17_SED_018-019CM	T	Percent Solids	74.4	[19]	74.4	J	HT	% BY WT.
1710903	% Solids	1710903-20	FF-MU7-GC-1-B-17_SED_019-020CM	T	Percent Solids	70.9	[20]	70.9	J	HT	% BY WT.
1710903	% Solids	1710903-21	FF-MU7-GC-1-B-17_SED_020-022CM	T	Percent Solids	69.9	[21]	69.9	J	HT	% BY WT.
1710903	% Solids	1710903-22	FF-MU7-GC-1-B-17_SED_022-024CM	T	Percent Solids	71.4	[22]	71.4	J	HT	% BY WT.
1710903	% Solids	1710903-23	FF-MU7-GC-1-B-17_SED_024-026CM	T	Percent Solids	74.3	[23]	74.3	J	HT	% BY WT.
1710903	% Solids	1710903-24	FF-MU7-GC-1-B-17_SED_026-028CM	T	Percent Solids	71	[24]	71	J	HT	% BY WT.
1710903	% Solids	1710903-25	FF-MU7-GC-1-B-17_SED_028-030CM	T	Percent Solids	69	[25]	69	J	HT	% BY WT.
1710903	% Solids	1710903-26	FF-MU7-GC-1-B-17_SED_030-032CM	T	Percent Solids	71.5	[26]	71.5	J	HT	% BY WT.
1710903	% Solids	1710903-27	FF-MU7-GC-1-B-17_SED_032-034CM	T	Percent Solids	74.4	[27]	74.4	J	HT	% BY WT.
1710903	% Solids	1710903-28	FF-MU7-GC-1-B-17_SED_034-036CM	T	Percent Solids	68	[28]	68	J	HT	% BY WT.
1710903	% Solids	1710903-29	FF-MU7-GC-1-B-17_SED_036-038CM	T	Percent Solids	68	[29]	68	J	HT	% BY WT.

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DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710903	% Solids	1710903-30	FF-MU7-GC-1-B-17_SED_038-040CM	T	Percent Solids	67.8	[30]	67.8	J	HT	% BY WT.
1710903	% Solids	1710903-31	FF-MU7-GC-1-B-17_SED_040-045CM	T	Percent Solids	67.3	[31]	67.3	J	HT	% BY WT.
1710903	% Solids	1710903-32	FF-MU7-GC-1-B-17_SED_045-050CM	T	Percent Solids	68.2	[32]	68.2	J	HT	% BY WT.
1710903	% Solids	1710903-33	FF-MU7-GC-1-B-17_SED_050-055CM	T	Percent Solids	69	[33]	69	J	HT	% BY WT.
1710903	% Solids	1710903-34	FF-MU7-GC-1-B-17_SED_055-060CM	T	Percent Solids	67.7	[34]	67.7	J	HT	% BY WT.
1710903	% Solids	1710903-35	FF-MU7-GC-1-B-17_SED_060-065CM	T	Percent Solids	69.5	[35]	69.5	J	HT	% BY WT.
1710903	% Solids	1710903-36	FF-MU7-GC-1-B-17_SED_065-070CM	T	Percent Solids	68.1	[36]	68.1	J	HT	% BY WT.
1710903	% Solids	1710903-37	FF-MU7-GC-1-B-17_SED_070-075CM	T	Percent Solids	64.7	[37]	64.7	J	HT	% BY WT.
1710903	% Solids	1710903-38	FF-MU7-GC-1-B-17_SED_075-080CM	T	Percent Solids	66.6	[38]	66.6	J	HT	% BY WT.
1710903	% Solids	1710903-39	FF-MU7-GC-1-B-17_SED_080-085CM	T	Percent Solids	65.1	[39]	65.1	J	HT	% BY WT.
1710903	% Solids	1710903-40	FF-MU7-GC-1-B-17_SED_085-090CM	T	Percent Solids	63.4	[40]	63.4	J	HT	% BY WT.
1711168	% Solids	1711168-01	MM-T4-C2-D-17_SED_000-001CM	T	Percent Solids	57.1	O-04	57.1	J	HT	% BY WT.
1711168	% Solids	1711168-02	MM-T4-C2-D-17_SED_001-002CM	T	Percent Solids	48	O-04	48	J	HT	% BY WT.
1711168	% Solids	1711168-03	MM-T4-C2-D-17_SED_002-003CM	T	Percent Solids	43.4	O-04	43.4	J	HT	% BY WT.
1711168	% Solids	1711168-04	MM-T4-C2-D-17_SED_003-004CM	T	Percent Solids	42.4	O-04	42.4	J	HT	% BY WT.
1711168	% Solids	1711168-05	MM-T4-C2-D-17_SED_004-005CM	T	Percent Solids	43	O-04	43	J	HT	% BY WT.
1711168	% Solids	1711168-06	MM-T4-C2-D-17_SED_005-006CM	T	Percent Solids	53.7	O-04	53.7	J	HT	% BY WT.
1711168	% Solids	1711168-07	MM-T4-C2-D-17_SED_006-007CM	T	Percent Solids	57.6	O-04	57.6	J	HT	% BY WT.
1711168	% Solids	1711168-08	MM-T4-C2-D-17_SED_007-008CM	T	Percent Solids	54.3	O-04	54.3	J	HT	% BY WT.
1711168	% Solids	1711168-09	MM-T4-C2-D-17_SED_008-009CM	T	Percent Solids	57.2	O-04	57.2	J	HT	% BY WT.
1711168	% Solids	1711168-10	MM-T4-C2-D-17_SED_009-010CM	T	Percent Solids	59.8	O-04	59.8	J	HT	% BY WT.
1711168	% Solids	1711168-11	MM-T4-C2-D-17_SED_010-011CM	T	Percent Solids	48.4	O-04	48.4	J	HT	% BY WT.
1711168	% Solids	1711168-12	MM-T4-C2-D-17_SED_011-012CM	T	Percent Solids	48.1	O-04	48.1	J	HT	% BY WT.
1711168	% Solids	1711168-13	MM-T4-C2-D-17_SED_012-013CM	T	Percent Solids	40.6	O-04	40.6	J	HT	% BY WT.
1711168	% Solids	1711168-14	MM-T4-C2-D-17_SED_013-014CM	T	Percent Solids	41.5	O-04	41.5	J	HT	% BY WT.
1711168	% Solids	1711168-15	MM-T4-C2-D-17_SED_014-015CM	T	Percent Solids	39.9	O-04	39.9	J	HT	% BY WT.
1711168	% Solids	1711168-16	MM-T4-C2-D-17_SED_015-016CM	T	Percent Solids	38.9	O-04	38.9	J	HT	% BY WT.

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1711168	% Solids	1711168-17	MM-T4-C2-D-17_SED_016-017CM	T	Percent Solids	37.9	O-04	37.9	J	HT	% BY WT.
1711168	% Solids	1711168-18	MM-T4-C2-D-17_SED_017-018CM	T	Percent Solids	37.7	O-04	37.7	J	HT	% BY WT.
1711168	% Solids	1711168-19	MM-T4-C2-D-17_SED_018-019CM	T	Percent Solids	38.2	O-04	38.2	J	HT	% BY WT.
1711168	% Solids	1711168-20	MM-T4-C2-D-17_SED_019-020CM	T	Percent Solids	39.7	O-04	39.7	J	HT	% BY WT.
1711168	% Solids	1711168-21	MM-T4-C2-D-17_SED_020-022CM	T	Percent Solids	40.5	O-04	40.5	J	HT	% BY WT.
1711168	% Solids	1711168-22	MM-T4-C2-D-17_SED_022-024CM	T	Percent Solids	38.4	O-04	38.4	J	HT	% BY WT.
1711168	% Solids	1711168-23	MM-T4-C2-D-17_SED_024-026CM	T	Percent Solids	36.5	O-04	36.5	J	HT	% BY WT.
1711168	% Solids	1711168-24	MM-T4-C2-D-17_SED_026-028CM	T	Percent Solids	35.1	O-04	35.1	J	HT	% BY WT.
1711168	% Solids	1711168-25	MM-T4-C2-D-17_SED_028-030CM	T	Percent Solids	34.9	O-04	34.9	J	HT	% BY WT.
1711168	% Solids	1711168-26	MM-T4-C2-D-17_SED_030-032CM	T	Percent Solids	37.1	O-04	37.1	J	HT	% BY WT.
1711168	% Solids	1711168-27	MM-T4-C2-D-17_SED_032-034CM	T	Percent Solids	37.2	O-04	37.2	J	HT	% BY WT.
1711168	% Solids	1711168-28	MM-T4-C2-D-17_SED_034-036CM	T	Percent Solids	38.3	O-04	38.3	J	HT	% BY WT.
1711168	% Solids	1711168-29	MM-T4-C2-D-17_SED_036-038CM	T	Percent Solids	40	O-04	40	J	HT	% BY WT.
1711168	% Solids	1711168-30	MM-T4-C2-D-17_SED_038-040CM	T	Percent Solids	41.3	O-04	41.3	J	HT	% BY WT.
1711168	% Solids	1711168-31	MM-T4-C2-D-17_SED_040-045CM	T	Percent Solids	43.6	O-04	43.6	J	HT	% BY WT.
1711168	% Solids	1711168-32	MM-T4-C2-D-17_SED_045-050CM	T	Percent Solids	42.4	O-04	42.4	J	HT	% BY WT.
1711168	% Solids	1711168-33	MM-T4-C2-D-17_SED_050-055CM	T	Percent Solids	41.3	O-04	41.3	J	HT	% BY WT.
1711168	% Solids	1711168-34	MM-T4-C2-D-17_SED_055-060CM	T	Percent Solids	42.6	O-04	42.6	J	HT	% BY WT.
1711168	% Solids	1711168-35	MM-T4-C2-D-17_SED_060-065CM	T	Percent Solids	42.8	O-04	42.8	J	HT	% BY WT.
1711168	% Solids	1711168-36	MM-T4-C2-D-17_SED_065-070CM	T	Percent Solids	43.3	O-04	43.3	J	HT	% BY WT.
1711168	% Solids	1711168-37	MM-T4-C2-D-17_SED_070-075CM	T	Percent Solids	46	O-04	46	J	HT	% BY WT.
1711168	% Solids	1711168-38	MM-T4-C2-D-17_SED_075-080CM	T	Percent Solids	54.8	O-04	54.8	J	HT	% BY WT.
1711168	% Solids	1711168-39	MM-T4-C2-D-17_SED_080-085CM	T	Percent Solids	51	O-04	51	J	HT	% BY WT.
1711168	% Solids	1711168-40	MM-T4-C2-D-17_SED_085-090CM	T	Percent Solids	34.3	O-04	34.3	J	HT	% BY WT.
1711170	% Solids	1711170-01	OR-T2-C5-B-17_SED_000-001CM	T	Percent Solids	45.6	O-04	45.6	J	HT	% BY WT.
1711170	% Solids	1711170-02	OR-T2-C5-B-17_SED_001-002CM	T	Percent Solids	44	O-04	44	J	HT	% BY WT.
1711170	% Solids	1711170-03	OR-T2-C5-B-17_SED_002-003CM	T	Percent Solids	45	O-04	45	J	HT	% BY WT.

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1711170	% Solids	1711170-04	OR-T2-C5-B-17_SED_003-004CM	T	Percent Solids	45.7	O-04	45.7	J	HT	% BY WT.
1711170	% Solids	1711170-05	OR-T2-C5-B-17_SED_004-005CM	T	Percent Solids	45.5	O-04	45.5	J	HT	% BY WT.
1711170	% Solids	1711170-06	OR-T2-C5-B-17_SED_005-006CM	T	Percent Solids	45.6	O-04	45.6	J	HT	% BY WT.
1711170	% Solids	1711170-07	OR-T2-C5-B-17_SED_006-007CM	T	Percent Solids	44.9	O-04	44.9	J	HT	% BY WT.
1711170	% Solids	1711170-08	OR-T2-C5-B-17_SED_007-008CM	T	Percent Solids	14.4	O-04	14.4	J	HT	% BY WT.
1711170	% Solids	1711170-09	OR-T2-C5-B-17_SED_008-009CM	T	Percent Solids	39.6	O-04	39.6	J	HT	% BY WT.
1711170	% Solids	1711170-10	OR-T2-C5-B-17_SED_009-010CM	T	Percent Solids	42.4	O-04	42.4	J	HT	% BY WT.
1711170	% Solids	1711170-11	OR-T2-C5-B-17_SED_010-011CM	T	Percent Solids	42	O-04	42	J	HT	% BY WT.
1711170	% Solids	1711170-12	OR-T2-C5-B-17_SED_011-012CM	T	Percent Solids	43.3	O-04	43.3	J	HT	% BY WT.
1711170	% Solids	1711170-13	OR-T2-C5-B-17_SED_012-013CM	T	Percent Solids	39.9	O-04	39.9	J	HT	% BY WT.
1711170	% Solids	1711170-14	OR-T2-C5-B-17_SED_013-014CM	T	Percent Solids	40.4	O-04	40.4	J	HT	% BY WT.
1711170	% Solids	1711170-15	OR-T2-C5-B-17_SED_014-015CM	T	Percent Solids	41.5	O-04	41.5	J	HT	% BY WT.
1711170	% Solids	1711170-16	OR-T2-C5-B-17_SED_015-016CM	T	Percent Solids	44.8	O-04	44.8	J	HT	% BY WT.
1711170	% Solids	1711170-17	OR-T2-C5-B-17_SED_016-017CM	T	Percent Solids	37.8	O-04	37.8	J	HT	% BY WT.
1711170	% Solids	1711170-18	OR-T2-C5-B-17_SED_017-018CM	T	Percent Solids	43.6	O-04	43.6	J	HT	% BY WT.
1711170	% Solids	1711170-19	OR-T2-C5-B-17_SED_018-019CM	T	Percent Solids	43.8	O-04	43.8	J	HT	% BY WT.
1711170	% Solids	1711170-20	OR-T2-C5-B-17_SED_019-020CM	T	Percent Solids	44.7	O-04	44.7	J	HT	% BY WT.
1711170	% Solids	1711170-21	OR-T2-C5-B-17_SED_020-022CM	T	Percent Solids	45.5	O-04	45.5	J	HT	% BY WT.
1711170	% Solids	1711170-22	OR-T2-C5-B-17_SED_022-024CM	T	Percent Solids	44.9	O-04	44.9	J	HT	% BY WT.
1711170	% Solids	1711170-23	OR-T2-C5-B-17_SED_024-026CM	T	Percent Solids	44.9	O-04	44.9	J	HT	% BY WT.
1711170	% Solids	1711170-24	OR-T2-C5-B-17_SED_026-028CM	T	Percent Solids	42.4	O-04	42.4	J	HT	% BY WT.
1711170	% Solids	1711170-25	OR-T2-C5-B-17_SED_028-030CM	T	Percent Solids	40.4	O-04	40.4	J	HT	% BY WT.
1711170	% Solids	1711170-26	OR-T2-C5-B-17_SED_030-032CM	T	Percent Solids	43.4	O-04	43.4	J	HT	% BY WT.
1711170	% Solids	1711170-27	OR-T2-C5-B-17_SED_032-034CM	T	Percent Solids	43.8	O-04	43.8	J	HT	% BY WT.
1711170	% Solids	1711170-28	OR-T2-C5-B-17_SED_034-036CM	T	Percent Solids	45.1	O-04	45.1	J	HT	% BY WT.
1711170	% Solids	1711170-29	OR-T2-C5-B-17_SED_036-038CM	T	Percent Solids	43	O-04	43	J	HT	% BY WT.
1711170	% Solids	1711170-30	OR-T2-C5-B-17_SED_038-040CM	T	Percent Solids	41.9	O-04	41.9	J	HT	% BY WT.

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SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1711170	% Solids	1711170-31	OR-T2-C5-B-17_SED_040-045CM	T	Percent Solids	15.7	O-04	15.7	J	HT	% BY WT.
1711170	% Solids	1711170-32	OR-T2-C5-B-17_SED_045-050CM	T	Percent Solids	40.2	O-04	40.2	J	HT	% BY WT.
1711170	% Solids	1711170-33	OR-T2-C5-B-17_SED_050-055CM	T	Percent Solids	41.7	O-04	41.7	J	HT	% BY WT.
1711170	% Solids	1711170-34	OR-T2-C5-B-17_SED_055-060CM	T	Percent Solids	42.1	O-04	42.1	J	HT	% BY WT.
1711170	% Solids	1711170-35	OR-T2-C5-B-17_SED_060-065CM	T	Percent Solids	40.3	O-04	40.3	J	HT	% BY WT.
1711170	% Solids	1711170-36	OR-T2-C5-B-17_SED_065-070CM	T	Percent Solids	45.2	O-04	45.2	J	HT	% BY WT.
1711170	% Solids	1711170-37	OR-T2-C5-B-17_SED_070-075CM	T	Percent Solids	39.1	O-04	39.1	J	HT	% BY WT.
1711170	% Solids	1711170-38	OR-T2-C5-B-17_SED_075-080CM	T	Percent Solids	38.7	O-04	38.7	J	HT	% BY WT.
1711170	% Solids	1711170-39	OR-T2-C5-B-17_SED_080-085CM	T	Percent Solids	37.9	O-04	37.9	J	HT	% BY WT.
1711170	% Solids	1711170-40	OR-T2-C5-B-17_SED_085-090CM	T	Percent Solids	35.7	O-04	35.7	J	HT	% BY WT.
1711172	% Solids	1711172-01	OR-T3-C5-D-17_SED_000-001CM	T	Percent Solids	44.1	O-04	44.1	J	HT	% BY WT.
1711172	% Solids	1711172-02	OR-T3-C5-D-17_SED_001-002CM	T	Percent Solids	38	O-04	38	J	HT	% BY WT.
1711172	% Solids	1711172-03	OR-T3-C5-D-17_SED_002-003CM	T	Percent Solids	35.1	O-04	35.1	J	HT	% BY WT.
1711172	% Solids	1711172-04	OR-T3-C5-D-17_SED_003-004CM	T	Percent Solids	44	O-04	44	J	HT	% BY WT.
1711172	% Solids	1711172-05	OR-T3-C5-D-17_SED_004-005CM	T	Percent Solids	40.8	O-04	40.8	J	HT	% BY WT.
1711172	% Solids	1711172-06	OR-T3-C5-D-17_SED_005-006CM	T	Percent Solids	45.1	O-04	45.1	J	HT	% BY WT.
1711172	% Solids	1711172-07	OR-T3-C5-D-17_SED_006-007CM	T	Percent Solids	45.1	O-04	45.1	J	HT	% BY WT.
1711172	% Solids	1711172-08	OR-T3-C5-D-17_SED_007-008CM	T	Percent Solids	39.4	O-04	39.4	J	HT	% BY WT.
1711172	% Solids	1711172-09	OR-T3-C5-D-17_SED_008-009CM	T	Percent Solids	39	O-04	39	J	HT	% BY WT.
1711172	% Solids	1711172-10	OR-T3-C5-D-17_SED_009-010CM	T	Percent Solids	35.5	O-04	35.5	J	HT	% BY WT.
1711172	% Solids	1711172-11	OR-T3-C5-D-17_SED_010-011CM	T	Percent Solids	42.4	O-04	42.4	J	HT	% BY WT.
1711172	% Solids	1711172-12	OR-T3-C5-D-17_SED_011-012CM	T	Percent Solids	41.2	O-04	41.2	J	HT	% BY WT.
1711172	% Solids	1711172-13	OR-T3-C5-D-17_SED_012-013CM	T	Percent Solids	24.9	O-04	24.9	J	HT	% BY WT.
1711172	% Solids	1711172-14	OR-T3-C5-D-17_SED_013-014CM	T	Percent Solids	42.3	O-04	42.3	J	HT	% BY WT.
1711172	% Solids	1711172-15	OR-T3-C5-D-17_SED_014-015CM	T	Percent Solids	42.2	O-04	42.2	J	HT	% BY WT.
1711172	% Solids	1711172-16	OR-T3-C5-D-17_SED_015-016CM	T	Percent Solids	41.8	O-04	41.8	J	HT	% BY WT.
1711172	% Solids	1711172-17	OR-T3-C5-D-17_SED_016-017CM	T	Percent Solids	44.5	O-04	44.5	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1711172	% Solids	1711172-18	OR-T3-C5-D-17_SED_017-018CM	T	Percent Solids	43.9	O-04	43.9	J	HT	% BY WT.
1711172	% Solids	1711172-19	OR-T3-C5-D-17_SED_018-019CM	T	Percent Solids	43.8	O-04	43.8	J	HT	% BY WT.
1711172	% Solids	1711172-20	OR-T3-C5-D-17_SED_019-020CM	T	Percent Solids	40.6	O-04	40.6	J	HT	% BY WT.
1711172	% Solids	1711172-21	OR-T3-C5-D-17_SED_020-022CM	T	Percent Solids	45.5	O-04	45.5	J	HT	% BY WT.
1711172	% Solids	1711172-22	OR-T3-C5-D-17_SED_022-024CM	T	Percent Solids	47.4	O-04	47.4	J	HT	% BY WT.
1711172	% Solids	1711172-23	OR-T3-C5-D-17_SED_024-026CM	T	Percent Solids	47.1	O-04	47.1	J	HT	% BY WT.
1711172	% Solids	1711172-24	OR-T3-C5-D-17_SED_026-028CM	T	Percent Solids	40.9	O-04	40.9	J	HT	% BY WT.
1711172	% Solids	1711172-25	OR-T3-C5-D-17_SED_028-030CM	T	Percent Solids	44.4	O-04	44.4	J	HT	% BY WT.
1711172	% Solids	1711172-26	OR-T3-C5-D-17_SED_030-032CM	T	Percent Solids	46.4	O-04	46.4	J	HT	% BY WT.
1711172	% Solids	1711172-27	OR-T3-C5-D-17_SED_032-034CM	T	Percent Solids	49.5	O-04	49.5	J	HT	% BY WT.
1711172	% Solids	1711172-28	OR-T3-C5-D-17_SED_034-036CM	T	Percent Solids	52.1	O-04	52.1	J	HT	% BY WT.
1711172	% Solids	1711172-29	OR-T3-C5-D-17_SED_036-038CM	T	Percent Solids	54.5	O-04	54.5	J	HT	% BY WT.
1711172	% Solids	1711172-30	OR-T3-C5-D-17_SED_038-040CM	T	Percent Solids	57	O-04	57	J	HT	% BY WT.
1711172	% Solids	1711172-31	OR-T3-C5-D-17_SED_040-045CM	T	Percent Solids	58	O-04	58	J	HT	% BY WT.
1711172	% Solids	1711172-32	OR-T3-C5-D-17_SED_045-050CM	T	Percent Solids	59.5	O-04	59.5	J	HT	% BY WT.
1711172	% Solids	1711172-33	OR-T3-C5-D-17_SED_050-055CM	T	Percent Solids	63.6	O-04	63.6	J	HT	% BY WT.
1711172	% Solids	1711172-34	OR-T3-C5-D-17_SED_055-060CM	T	Percent Solids	65.3	O-04	65.3	J	HT	% BY WT.
1711172	% Solids	1711172-35	OR-T3-C5-D-17_SED_060-065CM	T	Percent Solids	68.7	O-04	68.7	J	HT	% BY WT.
1711172	% Solids	1711172-36	OR-T3-C5-D-17_SED_065-070CM	T	Percent Solids	68.4	O-04	68.4	J	HT	% BY WT.
1711172	% Solids	1711172-37	OR-T3-C5-D-17_SED_070-075CM	T	Percent Solids	71.8	O-04	71.8	J	HT	% BY WT.
1711304	% Solids	1711304-01	UPB-MU11-GC-1-D-17_SED_000-001CM	T	Percent Solids	41.3	O-04	41.3	J	HT	% BY WT.
1711304	% Solids	1711304-02	UPB-MU11-GC-1-D-17_SED_001-002CM	T	Percent Solids	40.6	O-04	40.6	J	HT	% BY WT.
1711304	% Solids	1711304-03	UPB-MU11-GC-1-D-17_SED_004-005CM	T	Percent Solids	41.7	O-04	41.7	J	HT	% BY WT.
1711304	% Solids	1711304-04	UPB-MU11-GC-1-D-17_SED_011-012CM	T	Percent Solids	40.1	O-04	40.1	J	HT	% BY WT.
1711304	% Solids	1711304-05	UPB-MU11-GC-1-D-17_SED_014-015CM	T	Percent Solids	48.3	O-04	48.3	J	HT	% BY WT.
1711304	% Solids	1711304-06	UPB-MU11-GC-1-D-17_SED_015-016CM	T	Percent Solids	46	O-04	46	J	HT	% BY WT.
1711304	% Solids	1711304-07	UPB-MU11-GC-1-D-17_SED_016-017CM	T	Percent Solids	49	O-04	49	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1711304	% Solids	1711304-08	UPB-MU11-GC-1-D-17_SED_017-018CM	T	Percent Solids	43.5	O-04	43.5	J	HT	% BY WT.
1711304	% Solids	1711304-09	UPB-MU11-GC-1-D-17_SED_019-020CM	T	Percent Solids	39.4	O-04	39.4	J	HT	% BY WT.
1711304	% Solids	1711304-10	UPB-MU11-GC-1-D-17_SED_020-022CM	T	Percent Solids	39.8	O-04	39.8	J	HT	% BY WT.
1711304	% Solids	1711304-11	UPB-MU11-GC-1-D-17_SED_022-024CM	T	Percent Solids	40.6	O-04	40.6	J	HT	% BY WT.
1711304	% Solids	1711304-12	UPB-MU11-GC-1-D-17_SED_024-026CM	T	Percent Solids	38.9	O-04	38.9	J	HT	% BY WT.
1711304	% Solids	1711304-13	UPB-MU11-GC-1-D-17_SED_026-028CM	T	Percent Solids	37.3	O-04	37.3	J	HT	% BY WT.
1711304	% Solids	1711304-14	UPB-MU11-GC-1-D-17_SED_028-030CM	T	Percent Solids	39.7	O-04	39.7	J	HT	% BY WT.
1711304	% Solids	1711304-15	UPB-MU11-GC-1-D-17_SED_030-032CM	T	Percent Solids	38.8	O-04	38.8	J	HT	% BY WT.
1711304	% Solids	1711304-16	UPB-MU11-GC-1-D-17_SED_032-034CM	T	Percent Solids	42.1	O-04	42.1	J	HT	% BY WT.
1711304	% Solids	1711304-17	UPB-MU11-GC-1-D-17_SED_034-036CM	T	Percent Solids	42.5	O-04	42.5	J	HT	% BY WT.
1711304	% Solids	1711304-18	UPB-MU11-GC-1-D-17_SED_036-038CM	T	Percent Solids	39.9	O-04	39.9	J	HT	% BY WT.
1711304	% Solids	1711304-19	UPB-MU11-GC-1-D-17_SED_038-040CM	T	Percent Solids	41.5	O-04	41.5	J	HT	% BY WT.
1711304	% Solids	1711304-20	UPB-MU11-GC-1-D-17_SED_040-045CM	T	Percent Solids	40.3	O-04	40.3	J	HT	% BY WT.
1711304	% Solids	1711304-21	UPB-MU11-GC-1-D-17_SED_045-050CM	T	Percent Solids	40.8	O-04	40.8	J	HT	% BY WT.
1711304	% Solids	1711304-22	UPB-MU11-GC-1-D-17_SED_050-055CM	T	Percent Solids	44.2	O-04	44.2	J	HT	% BY WT.
1711304	% Solids	1711304-23	UPB-MU11-GC-1-D-17_SED_055-060CM	T	Percent Solids	40.9	O-04	40.9	J	HT	% BY WT.
1711304	% Solids	1711304-24	UPB-MU11-GC-1-D-17_SED_060-065CM	T	Percent Solids	47.6	O-04	47.6	J	HT	% BY WT.
1711304	% Solids	1711304-25	UPB-MU11-GC-1-D-17_SED_065-070CM	T	Percent Solids	39.6	O-04	39.6	J	HT	% BY WT.
L1739126	LLOYD_KAHN	L1739126-04	FF-MU7-GC-1-B-17_SED_005-006CM	T	Total Organic Carbon	1.0495		1.0495	J	MS-H,MS-RPD	PERCENT
L1739126	LLOYD_KAHN	L1739126-21	FF-MU7-GC-1-B-17_SED_024-026CM	T	Total Organic Carbon	1.825		1.825	J	LD	PERCENT
L1739126	LLOYD_KAHN	L1739126-25	FF-MU7-GC-1-B-17_SED_032-034CM	T	Total Organic Carbon	1.59		1.59	J	MS-H	PERCENT
1709843	% Solids	1709843-01	PBR-18-E-17_SED_000-001CM	T	Percent Solids	32.4	O-04	32.4	J	HT	% BY WT.
1709843	% Solids	1709843-02	PBR-18-E-17_SED_001-002CM	T	Percent Solids	33	O-04	33	J	HT	% BY WT.
1709843	% Solids	1709843-03	PBR-18-E-17_SED_002-003CM	T	Percent Solids	34.3	O-04	34.3	J	HT	% BY WT.
1709843	% Solids	1709843-04	PBR-18-E-17_SED_003-004CM	T	Percent Solids	33.6	O-04	33.6	J	HT	% BY WT.
1709843	% Solids	1709843-05	PBR-18-E-17_SED_004-005CM	T	Percent Solids	35.5	O-04	35.5	J	HT	% BY WT.
1709843	% Solids	1709843-06	PBR-18-E-17_SED_005-006CM	T	Percent Solids	34.5	O-04	34.5	J	HT	% BY WT.
1709843	% Solids	1709843-07	PBR-18-E-17_SED_006-007CM	T	Percent Solids	33.3	O-04	33.3	J	HT	% BY WT.
1709843	% Solids	1709843-08	PBR-18-E-17_SED_007-008CM	T	Percent Solids	33	O-04	33	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709843	% Solids	1709843-09	PBR-18-E-17_SED_008-009CM	T	Percent Solids	30.5	O-04	30.5	J	HT	% BY WT.
1709843	% Solids	1709843-10	PBR-18-E-17_SED_009-010CM	T	Percent Solids	31.7	O-04	31.7	J	HT	% BY WT.
1709843	% Solids	1709843-11	PBR-18-E-17_SED_010-011CM	T	Percent Solids	31.5	O-04	31.5	J	HT	% BY WT.
1709843	% Solids	1709843-12	PBR-18-E-17_SED_011-012CM	T	Percent Solids	32	O-04	32	J	HT	% BY WT.
1709843	% Solids	1709843-13	PBR-18-E-17_SED_012-013CM	T	Percent Solids	41.5	O-04	41.5	J	HT	% BY WT.
1709843	% Solids	1709843-14	PBR-18-E-17_SED_013-014CM	T	Percent Solids	36.3	O-04	36.3	J	HT	% BY WT.
1709843	% Solids	1709843-15	PBR-18-E-17_SED_014-015CM	T	Percent Solids	38.3	O-04	38.3	J	HT	% BY WT.

Units

NG/G = Nanogram per gram

Validation Qualifier:

J = Value is estimated

Validation Reason Codes:

LD = Lab duplicate limit exceeded

MS-H = MS and/or MSD recovery high

MS-L = MS and/or MSD recovery low

MS-RPD = MS/MSD RPD limit exceeded

LR = Lab replicate limit exceeded

HT = Hold time exceeded

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709433, 1709434, 1709435, 1709837, 1709838, 1709839, 1709840, 1709841, 1709842, 1709843, 1709844, 1709845, 1710292, 1710318, 1710322, 1710323, 1710903, 1711168, 1711170, 1711172, 1711304, L1732772, L1732773, L1735008, L1735009, L1735010, L1735011, L1736452, L1736457, L1736459, L1736460, L1739126, L1740286, L1740288, L1740290 and L1741134

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_000-001CM	FS	36	J	1480			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_001-002CM	FS	35	J	1700			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_002-003CM	FS	36.5	J	1370			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_003-004CM	FS	37	J	1520			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_004-005CM	FS	38	J	1760			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_005-006CM	FS	37.3	J	1800			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_006-007CM	FS	37.5	J	1840			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_007-008CM	FS	37.4	J	1900			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_008-009CM	FS	40.7	J	1440			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_009-010CM	FS	37.3	J	1660			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_010-011CM	FS	38.8	J	1250			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_011-012CM	FS	37.1	J	1080			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_012-013CM	FS	33.2	J	769			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_013-014CM	FS	32.2	J	585			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_014-015CM	FS	37.6	J	1410			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_015-016CM	FS	35.9	J	463			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_016-017CM	FS	35.9	J	493			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_017-018CM	FS	31.5	J	561			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_018-019CM	FS	30.4	J	585			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_019-020CM	FS	36	J	509			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_020-022CM	FS	48	J	326			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_022-024CM	FS	36.8	J	413			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_024-026CM	FS	37.8	J	400			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_026-028CM	FS	36.6	J	388			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method Parameter Unit Fraction		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_028-030CM	FS	39.6	J	366			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_030-032CM	FS	30.4	J	533			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_032-034CM	FS	36.7	J	405			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_034-036CM	FS	37.5	J	410			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_036-038CM	FS	38.7	J	354			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_038-040CM	FS	40.5	J	390			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_040-045CM	FS	39.1	J	488			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_045-050CM	FS	35.7	J	372			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_050-055CM	FS	37.8	J	290			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_055-060CM	FS	37	J	315			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_060-065CM	FS	38.5	J	321			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_065-070CM	FS	36.2	J	417			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_070-075CM	FS	37.8	J	426			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_075-080CM	FS	41.9	J	247			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_080-085CM	FS	40	J	296			
1709433	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_085-090CM	FS	39.6	J	387			
1709433	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_090-095CM	FS	45.4	J	187			
1709433	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_095-100CM	FS	48.7	J	160			
1709433	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_100-105CM	FS	53.4	J	94.3			
1709433	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_105-110CM	FS	56.3	J	79.2			
1709433	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_110-115CM	FS	56.7	J	89.6			
1709433	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_115-120CM	FS	60.2	J	60			
1709433	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_120-125CM	FS	61.7	J	51.6			
1709433	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_125-130CM	FS	63	J	33.2			
1709433	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_130-135CM	FS	61.7	J	36.2			
1709433	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_135-140CM	FS	64.2	J	34.9			
1709433	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_140-145CM	FS	61.5	J	26.1			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_000-001CM	FS	46.9	J	681			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_001-002CM	FS	46.7	J	505			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_002-003CM	FS	55.9	J	652			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_003-004CM	FS	61.6	J	734			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_004-005CM	FS	63.4	J	660			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_005-006CM	FS	58.5	J	670			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_006-007CM	FS	62.7	J	589			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_007-008CM	FS	68.1	J	399			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_008-009CM	FS	63.2	J	289			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_009-010CM	FS	68.9	J	222			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_010-011CM	FS	72.6	J	205			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_011-012CM	FS	74	J	48.9			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_012-013CM	FS	74	J	71			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_013-014CM	FS	75.5	J	58.2			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_014-015CM	FS	75.6	J	36.4			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_015-016CM	FS	82	J	44.5			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_016-017CM	FS	73.3	J	49.8			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_017-018CM	FS	70.7	J	48.7			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_018-019CM	FS	70.2	J	42.3			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_019-020CM	FS	74.8	J	35			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_020-022CM	FS	70.4	J	42.5			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_022-024CM	FS	67.7	J	29.5			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_024-026CM	FS	62.8	J	35.1			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_026-028CM	FS	78.3	J	37.7			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_028-030CM	FS	62.5	J	30.1			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_030-032CM	FS	61.5	J	39.7			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_032-034CM	FS	63.6	J	31.3			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_034-036CM	FS	66.4	J	26.1			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_036-038CM	FS	66.8	J	21.5			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_038-040CM	FS	68.1	J	31.9			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_040-045CM	FS	67.7	J	25.3			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_045-050CM	FS	70.7	J	37.3			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_050-055CM	FS	68.6	J	26.2			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_055-060CM	FS	67.1	J	28			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_060-065CM	FS	70.2	J	31.6			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_065-070CM	FS	68.4	J	20.3			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_070-075CM	FS	65.7	J	25.1			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_075-080CM	FS	71.3	J	16.6			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_080-085CM	FS	63	J	22.4			
1709434	PBR-26-A	9/11/2017	PBR-26-A-17_SED_085-090CM	FS	65	J	19			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_000-001CM	FS	33.4	J	707			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_001-002CM	FS	33.4	J	669			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_002-003CM	FS	36.9	J	671			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_003-004CM	FS	33.2	J	848			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_004-005CM	FS	38.6	J	865			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_005-006CM	FS	35	J	852			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_006-007CM	FS	37.4	J	603			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_007-008CM	FS	36.8	J	976			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_008-009CM	FS	36.4	J	1080			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_009-010CM	FS	37.6	J	982			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_010-011CM	FS	36.5	J	1070			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_011-012CM	FS	37.4	J	1100			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_012-013CM	FS	48	J	1040			
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_013-014CM	FS	40.4	J	1230			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method Parameter Unit Fraction		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1709835	ES-01-C3	9/25/2017	ES-01-C3-17_SED_014-015CM	FS	38.4	J	1010			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_015-016CM	FS	50.1	J	52			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_016-017CM	FS	50.8	J	47.7			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_017-018CM	FS	56	J	65.2			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_018-019CM	FS	59.8	J	33.5			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_019-020CM	FS	60	J	32.8			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_020-022CM	FS	62	J	30.1			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_022-024CM	FS	63.8	J	24.8			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_024-026CM	FS	57	J	28.5			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_026-028CM	FS	61.6	J	24.5			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_028-030CM	FS	60.5	J	23.8			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_030-032CM	FS	65.1	J	23.2			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_032-034CM	FS	65.7	J	22.6			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_034-036CM	FS	65.9	J	22.6			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_036-038CM	FS	62.3	J	30.2			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_038-040CM	FS	57.2	J	114			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_040-045CM	FS	59.9	J	28.3			
1709837	PBR-20-E	9/26/2017	PBR-20-E-17_SED_045-050CM	FS	62.5	J	23.6			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_015-016CM	FS	41.6	J	752			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_016-017CM	FS	39.7	J	613			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_017-018CM	FS	42.1	J	569			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_018-019CM	FS	41.1	J	433			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_019-020CM	FS	42.3	J	372			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_020-022CM	FS	42.5	J	334			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_022-024CM	FS	43.9	J	332			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_024-026CM	FS	44.6	J	280			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_026-028CM	FS	45.2	J	268			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method Parameter Unit Fraction		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_028-030CM	FS	43.7	J	327			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_030-032CM	FS	42.9	J	318			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_032-034CM	FS	46.2	J	253			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_034-036CM	FS	45.6	J	205			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_036-038CM	FS	57.1	J	195			
1709838	ES-01-C3	9/25/2017	ES-01-C3-17_SED_038-040CM	FS	48.2	J	129			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_040-045CM	FS	47.1	J	188			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_045-050CM	FS	46.2	J	127			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_050-055CM	FS	46.6	J	77.3			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_055-060CM	FS	47.8	J	69.6			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_060-065CM	FS	50.9	J	47.3			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_065-070CM	FS	50	J	29.6			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_070-075CM	FS	55.6	J	30.9			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_075-080CM	FS	53.9	J	16.2			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_080-085CM	FS	53.2	J	15			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_085-090CM	FS	60	J	19.8			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_090-095CM	FS	59.7	J	12.8			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_095-100CM	FS	56	J	14.7			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_100-105CM	FS	58.6	J	11.4			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_105-110CM	FS	65.4	J	9.92			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_110-115CM	FS	60.5	J	12.7			
1709839	ES-01-C3	9/25/2017	ES-01-C3-17_SED_115-120CM	FS	65.1	J	9.76			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_000-001CM	FS	53.7	J	1070			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_001-002CM	FS	50.2	J	1290			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_002-003CM	FS	53.6	J	1200			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_003-004CM	FS	56.6	J	1130			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_004-005CM	FS	58	J	941			

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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_005-006CM	FS	53.5	J	1230			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_006-007CM	FS	65.6	J	571			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_007-008CM	FS	60.2	J	212			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_008-009CM	FS	60.6	J	101			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_009-010CM	FS	61.2	J	65.8			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_010-011CM	FS	60.8	J	44.4			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_011-012CM	FS	60.4	J	39.5			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_012-013CM	FS	60.6	J	35.6			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_013-014CM	FS	57.3	J	43.4			
1709840	PBR-20-E	9/26/2017	PBR-20-E-17_SED_014-015CM	FS	51.6	J	53			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_000-001CM	FS	49.1	J	706			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_001-002CM	FS	53	J	601			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_002-003CM	FS	50.9	J	648			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_003-004CM	FS	51.5	J	549			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_004-005CM	FS	50.7	J	424			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_005-006CM	FS	49.8	J	425			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_006-007CM	FS	52	J	316			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_007-008CM	FS	53.5	J	253			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_008-009CM	FS	54.4	J	252			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_009-010CM	FS	55.4	J	288			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_010-011CM	FS	54.5	J	235			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_011-012CM	FS	56.5	J	180			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_012-013CM	FS	61.8	J	208			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_013-014CM	FS	57.2	J	173			
1709841	ES-18-B	9/25/2017	ES-18-B-17_SED_014-015CM	FS	58.9	J	129			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_015-016CM	FS	58.9	J	124			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_016-017CM	FS	48.7	J	143			

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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_017-018CM	FS	58.7	J	101			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_018-019CM	FS	59.1	J	92.9			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_019-020CM	FS	58.1	J	70.2			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_020-022CM	FS	58.7	J	56.1			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_022-024CM	FS	58.1	J	51.1			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_024-026CM	FS	59.9	J	25			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_026-028CM	FS	61.2	J	21.3			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_028-030CM	FS	59.9	J	33.4			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_030-032CM	FS	59.5	J	21.3			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_032-034CM	FS	58.6	J	16.9			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_034-036CM	FS	57.7	J	15.9			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_036-038CM	FS	58.9	J	17.8			
1709842	ES-18-B	9/25/2017	ES-18-B-17_SED_038-040CM	FS	60.3	J	16.3			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_000-001CM	FS	32.4	J	854			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_001-002CM	FS	33	J	841			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_002-003CM	FS	34.3	J	858			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_003-004CM	FS	33.6	J	1,020			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_004-005CM	FS	35.5	J	983			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_005-006CM	FS	34.5	J	915			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_006-007CM	FS	33.3	J	863			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_007-008CM	FS	33	J	999			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_008-009CM	FS	30.5	J	1,050			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_009-010CM	FS	31.7	J	970			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_010-011CM	FS	31.5	J	1,170			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_011-012CM	FS	32	J	1,120			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_012-013CM	FS	41.5	J	652			
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_013-014CM	FS	36.3	J	859			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1709843	PBR-18-E	9/26/2017	PBR-18-E-17_SED_014-015CM	FS	38.3	J	821			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_015-016CM	FS	38.8	J	881			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_016-017CM	FS	35.2	J	1020			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_017-018CM	FS	35	J	1090			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_018-019CM	FS	36	J	1020			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_019-020CM	FS	36.9	J	1180			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_020-022CM	FS	39.8	J	1350			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_022-024CM	FS	36.6	J	1560			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_024-026CM	FS	37.8	J	1490			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_026-028CM	FS	36.6	J	1760			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_028-030CM	FS	37.2	J	1890			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_030-032CM	FS	35.4	J	2240			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_032-034CM	FS	35.9	J	1990			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_034-036CM	FS	31	J	2880			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_036-038CM	FS	36.3	J	2800			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_038-040CM	FS	38.8	J	2200			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_040-045CM	FS	45.1	J	1440			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_045-050CM	FS	46.7	J	2270			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_050-055CM	FS	39.4	J	951			
1709844	PBR-18-E	9/26/2017	PBR-18-E-17_SED_055-060CM	FS	43.8	J	440			
1709845	ES-18-B	9/25/2017	ES-18-B-17_SED_040-045CM	FS	63.2	J	16.7			
1709845	ES-18-B	9/25/2017	ES-18-B-17_SED_045-050CM	FS	59.5	J	13.5			
1709845	ES-18-B	9/25/2017	ES-18-B-17_SED_050-055CM	FS	56.2	J	15.8			
1709845	ES-18-B	9/25/2017	ES-18-B-17_SED_055-060CM	FS	58	J	14.2			
1709845	ES-18-B	9/25/2017	ES-18-B-17_SED_060-065CM	FS	62.5	J	10.1			
1709845	ES-18-B	9/25/2017	ES-18-B-17_SED_065-070CM	FS	62.4	J	11.8			
1709845	ES-18-B	9/25/2017	ES-18-B-17_SED_070-075CM	FS	63.3	J	10.5			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method Parameter Unit Fraction		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1710292	MM-T2-C1-B	9/29/2017	MM-T2-C1-B-17_SED_000-001CM	FS	15.8	J	173			
1710292	MM-T2-C1-B	9/29/2017	MM-T2-C1-B-17_SED_001-002CM	FS	13.8	J	151			
1710292	MM-T2-C1-B	9/29/2017	MM-T2-C1-B-17_SED_002-003CM	FS	14.4	J	159			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_003-004CM	FS	15.9	J	337			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_004-005CM	FS	18.5	J	653			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_005-006CM	FS	16.4	J	716			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_006-007CM	FS	20	J	1050			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_007-008CM	FS	18	J	702			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_008-009CM	FS	17	J	728			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_009-010CM	FS	18.2	J	400			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_010-011CM	FS	17.5	J	283			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_011-012CM	FS	19	J	93.9			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_012-013CM	FS	18.7	J	94.2			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_013-014CM	FS	18	J	57.5			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_014-015CM	FS	17.4	J	62.6			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_015-016CM	FS	16.8	J	44.8			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_016-017CM	FS	16.4	J	37.7			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_017-018CM	FS	17.7	J	61.5			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_018-019CM	FS	17.2	J	44			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_019-020CM	FS	17.6	J	38.5			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_020-022CM	FS	18.2	J	34.4			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_022-024CM	FS	18.1	J	33.5			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_024-026CM	FS	20.7	J	23.5			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_026-028CM	FS	19.2	J	23			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_028-030CM	FS	20.8	J	17.9	J		
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_030-032CM	FS	22	J	26.6			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_032-034CM	FS	23.2	J	16.3			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_034-036CM	FS	28.2	J	14.2			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_036-038CM	FS	32.3	J	13.5			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_038-040CM	FS	28	J	16.5			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_040-045CM	FS	29.7	J	18			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_045-050CM	FS	48.4	J	9.91			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_050-055CM	FS	50.5	J	15.5			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_055-060CM	FS	43.9	J	19.7			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_060-065CM	FS	31.3	J	21.1			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_065-070CM	FS	35.4	J	21.2			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_070-075CM	FS	41	J	22.7			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_075-080CM	FS	42	J	21.4			
1710292	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_080-085CM	FS	41.8	J	23.9			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_000-001CM	FS	32.9	J	680			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_001-002CM	FS	35.1	J	655			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_002-003CM	FS	40.3	J	559			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_003-004CM	FS	40.5	J	517			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_004-005CM	FS	37.4	J	576			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_005-006CM	FS	36.3	J	577			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_006-007CM	FS	38.2	J	723			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_007-008CM	FS	40.2	J	690			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_008-009CM	FS	33	J	600			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_009-010CM	FS	32.7	J	633			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_010-011CM	FS	37.6	J	511			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_011-012CM	FS	49.4	J	464			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_012-013CM	FS	47.1	J	397			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_013-014CM	FS	43.1	J	436			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_014-015CM	FS	43.6	J	525			

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_015-016CM	FS	44	J	629			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_016-017CM	FS	40.8	J	590			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_017-018CM	FS	38.1	J	601			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_018-019CM	FS	36.1	J	527			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_019-020CM	FS	32.9	J	649			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_020-022CM	FS	33.7	J	647			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_022-024CM	FS	41.1	J	628			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_024-026CM	FS	42.4	J	706			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_026-028CM	FS	34.8	J	783			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_028-030CM	FS	35.8	J	854			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_030-032CM	FS	36.8	J	882			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_032-034CM	FS	41.2	J	903			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_034-036CM	FS	35.1	J	852			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_036-038CM	FS	43.1	J	900			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_038-040CM	FS	37.9	J	985			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_040-045CM	FS	39.5	J	1010			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_045-050CM	FS	38.7	J	1210			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_050-055CM	FS	37.1	J	1120			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_055-060CM	FS	40.1	J	1490			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_060-065CM	FS	41.2	J	1820			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_065-070CM	FS	42	J	1670			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_070-075CM	FS	43.5	J	1950			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_075-080CM	FS	41.3	J	733			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_080-085CM	FS	42.2	J	498			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_085-090CM	FS	37	J	318			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_090-095CM	FS	37.8	J	299			
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_095-100CM	FS	41.6	J	371			

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710318	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_100-105CM	FS	36.9	J	312			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_000-001CM	FS	42.1	J	711			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_001-002CM	FS	46.1	J	569			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_002-003CM	FS	49.1	J	603			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_003-004CM	FS	48.8	J	606			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_004-005CM	FS	50	J	658			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_005-006CM	FS	50.1	J	685			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_006-007CM	FS	48.7	J	771			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_007-008CM	FS	45.9	J	802			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_008-009CM	FS	45.7	J	781			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_009-010CM	FS	46.5	J	758			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_010-011CM	FS	86.9	J	416			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_011-012CM	FS	44.4	J	926			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_012-013CM	FS	48.3	J	795			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_013-014CM	FS	50.5	J	724			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_014-015CM	FS	51	J	708			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_015-016CM	FS	52.5	J	781			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_016-017CM	FS	50.2	J	745			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_017-018CM	FS	54.1	J	712			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_018-019CM	FS	53.3	J	721			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_019-020CM	FS	54.7	J	736			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_020-022CM	FS	52.3	J	777			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_022-024CM	FS	52.7	J	820			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_024-026CM	FS	52.4	J	785			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_026-028CM	FS	52.3	J	885			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_028-030CM	FS	55.3	J	856			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_030-032CM	FS	58	J	850			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method Parameter Unit Fraction		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_032-034CM	FS	56.4	J	1070			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_034-036CM	FS	60.1	J	1280			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_036-038CM	FS	58.2	J	1510			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_038-040CM	FS	57.4	J	1490			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_040-045CM	FS	58.8	J	838			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_045-050CM	FS	54.3	J	377			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_050-055CM	FS	52.4	J	185			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_055-060CM	FS	56.3	J	78.5			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_060-065CM	FS	71.5	J	17.2			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_065-070CM	FS	71.9	J	13.8			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_070-075CM	FS	70.5	J	15.5			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_075-080CM	FS	69.3	J	16.3			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_080-085CM	FS	68	J	17.9			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_085-090CM	FS	68.5	J	16.1			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_090-095CM	FS	67.8	J	18.2			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_095-100CM	FS	69.8	J	14.8			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_100-105CM	FS	68.8	J	15			
1710322	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_105-110CM	FS	68.8	J	21.6			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_000-001CM	FS	33.1	J	953			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_001-002CM	FS	34	J	952			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_002-003CM	FS	38	J	672			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_003-004CM	FS	42.7	J	393			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_004-005CM	FS	47.8	J	187			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_005-006CM	FS	50.4	J	143			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_006-007CM	FS	54.2	J	124			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_007-008CM	FS	53.2	J	99.6			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_008-009CM	FS	60.7	J	99.5			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_009-010CM	FS	63.7	J	80.5			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_010-011CM	FS	65.7	J	70.1			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_011-012CM	FS	67.3	J	67.3			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_012-013CM	FS	69.1	J	75.6			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_013-014CM	FS	70	J	53.9			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_014-015CM	FS	69.9	J	51.2			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_015-016CM	FS	70.7	J	40			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_016-017CM	FS	70.1	J	34.5			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_017-018CM	FS	70.9	J	28.8			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_018-019CM	FS	71	J	36.8			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_019-020CM	FS	70.1	J	33.1			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_020-022CM	FS	70.4	J	30.8			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_022-024CM	FS	68.8	J	38.6			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_024-026CM	FS	69.5	J	30.9			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_026-028CM	FS	72.3	J	27.4			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_028-030CM	FS	72	J	22.8			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_030-032CM	FS	70.8	J	23.8			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_032-034CM	FS	73.5	J	20.3			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_034-036CM	FS	75.5	J	20.8			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_036-038CM	FS	78	J	12.2			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_038-040CM	FS	76.2	J	14.6			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_040-045CM	FS	75.9	J	9.74			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_045-050CM	FS	74.8	J	11.8			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_050-055CM	FS	75.8	J	7.92			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_055-060CM	FS	77	J	7.23			
1710323	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_060-065CM	FS	82.7	J	4.43			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_000-001CM	FS	51.1	J	349			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_001-002CM	FS	71	J	84.7			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_002-003CM	FS	75.9	J	53.7			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_003-004CM	FS	79.9	J	41.6			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_004-005CM	FS	83.2	J	25			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_005-006CM	FS	83.5	J	25.2			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_006-007CM	FS	82	J	19			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_007-008CM	FS	79.1	J	18.8			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_008-009CM	FS	81.1	J	20			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_009-010CM	FS	83.1	J	14.7			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_010-011CM	FS	82.4	J	19			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_011-012CM	FS	82.4	J	22.8			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_012-013CM	FS	78.3	J	25			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_013-014CM	FS	82.1	J	21.3			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_014-015CM	FS	77.6	J	18.5			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_015-016CM	FS	75.8	J	20.6			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_016-017CM	FS	76	J	18.8			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_017-018CM	FS	75	J	20.7			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_018-019CM	FS	74.4	J	17.9			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_019-020CM	FS	70.9	J	17.6			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_020-022CM	FS	69.9	J	17.9			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_022-024CM	FS	71.4	J	19.6			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_024-026CM	FS	74.3	J	19.4			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_026-028CM	FS	71	J	21.3			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_028-030CM	FS	69	J	19			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_030-032CM	FS	71.5	J	25.9			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_032-034CM	FS	74.4	J	22.7			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_034-036CM	FS	68	J	17.8			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_036-038CM	FS	68	J	22.3			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_038-040CM	FS	67.8	J	20.5			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_040-045CM	FS	67.3	J	24.1			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_045-050CM	FS	68.2	J	21.8			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_050-055CM	FS	69	J	24			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_055-060CM	FS	67.7	J	23.8			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_060-065CM	FS	69.5	J	24.2			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_065-070CM	FS	68.1	J	23.2			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_070-075CM	FS	64.7	J	19.5			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_075-080CM	FS	66.6	J	23			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_080-085CM	FS	65.1	J	20			
1710903	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_085-090CM	FS	63.4	J	22.8			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_000-001CM	FS	57.1	J	317			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_001-002CM	FS	48	J	568			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_002-003CM	FS	43.4	J	707			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_003-004CM	FS	42.4	J	722			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_004-005CM	FS	43	J	744			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_005-006CM	FS	53.7	J	459			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_006-007CM	FS	57.6	J	358			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_007-008CM	FS	54.3	J	488			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_008-009CM	FS	57.2	J	397			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_009-010CM	FS	59.8	J	369			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_010-011CM	FS	48.4	J	627			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_011-012CM	FS	48.1	J	619			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_012-013CM	FS	40.6	J	791			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_013-014CM	FS	41.5	J	838			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_014-015CM	FS	39.9	J	907			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method Parameter Unit Fraction		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_015-016CM	FS	38.9	J	800			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_016-017CM	FS	37.9	J	840			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_017-018CM	FS	37.7	J	895			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_018-019CM	FS	38.2	J	780			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_019-020CM	FS	39.7	J	775			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_020-022CM	FS	40.5	J	699			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_022-024CM	FS	38.4	J	792			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_024-026CM	FS	36.5	J	832			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_026-028CM	FS	35.1	J	884			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_028-030CM	FS	34.9	J	590			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_030-032CM	FS	37.1	J	870			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_032-034CM	FS	37.2	J	893			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_034-036CM	FS	38.3	J	900			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_036-038CM	FS	40	J	910			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_038-040CM	FS	41.3	J	837			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_040-045CM	FS	43.6	J	810			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_045-050CM	FS	42.4	J	859			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_050-055CM	FS	41.3	J	845			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_055-060CM	FS	42.6	J	830			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_060-065CM	FS	42.8	J	939			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_065-070CM	FS	43.3	J	872			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_070-075CM	FS	46	J	858			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_075-080CM	FS	54.8	J	733			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_080-085CM	FS	51	J	889			
1711168	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_085-090CM	FS	34.3	J	1210			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_000-001CM	FS	45.6	J	715			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_001-002CM	FS	44	J	740			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_002-003CM	FS	45	J	678			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_003-004CM	FS	45.7	J	786			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_004-005CM	FS	45.5	J	683			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_005-006CM	FS	45.6	J	681			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_006-007CM	FS	44.9	J	659			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_007-008CM	FS	14.4	J	2000			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_008-009CM	FS	39.6	J	813			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_009-010CM	FS	42.4	J	808			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_010-011CM	FS	42	J	863			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_011-012CM	FS	43.3	J	822			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_012-013CM	FS	39.9	J	917			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_013-014CM	FS	40.4	J	942			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_014-015CM	FS	41.5	J	891			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_015-016CM	FS	44.8	J	806			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_016-017CM	FS	37.8	J	981			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_017-018CM	FS	43.6	J	938			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_018-019CM	FS	43.8	J	945			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_019-020CM	FS	44.7	J	985			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_020-022CM	FS	45.5	J	822			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_022-024CM	FS	44.9	J	885			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_024-026CM	FS	44.9	J	1060			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_026-028CM	FS	42.4	J	1150			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_028-030CM	FS	40.4	J	1180			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_030-032CM	FS	43.4	J	1190			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_032-034CM	FS	43.8	J	1480			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_034-036CM	FS	45.1	J	1770			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_036-038CM	FS	43	J	2200			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_038-040CM	FS	41.9	J	2620			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_040-045CM	FS	15.7	J	5260			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_045-050CM	FS	40.2	J	2340			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_050-055CM	FS	41.7	J	1640			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_055-060CM	FS	42.1	J	412			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_060-065CM	FS	40.3	J	285			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_065-070CM	FS	45.2	J	259			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_070-075CM	FS	39.1	J	238			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_075-080CM	FS	38.7	J	251			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_080-085CM	FS	37.9	J	234			
1711170	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_085-090CM	FS	35.7	J	251			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_000-001CM	FS	44.1	J	669			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_001-002CM	FS	38	J	648			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_002-003CM	FS	35.1	J	708			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_003-004CM	FS	44	J	536			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_004-005CM	FS	40.8	J	653			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_005-006CM	FS	45.1	J	740			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_006-007CM	FS	45.1	J	808			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_007-008CM	FS	39.4	J	795			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_008-009CM	FS	39	J	752			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_009-010CM	FS	35.5	J	975			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_010-011CM	FS	42.4	J	714			
1711172	OR-T3-C5-D	10/24/2017	OR-T3-C5-D-17_SED_011-012CM	FS	41.2	J	762			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_012-013CM	FS	24.9	J	463			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_013-014CM	FS	42.3	J	835			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_014-015CM	FS	42.2	J	862			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_015-016CM	FS	41.8	J	875			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_016-017CM	FS	44.5	J	894			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_017-018CM	FS	43.9	J	951			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_018-019CM	FS	43.8	J	946			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_019-020CM	FS	40.6	J	979			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_020-022CM	FS	45.5	J	1200			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_022-024CM	FS	47.4	J	1230			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_024-026CM	FS	47.1	J	1310			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_026-028CM	FS	40.9	J	1450			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_028-030CM	FS	44.4	J	1430			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_030-032CM	FS	46.4	J	1310			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_032-034CM	FS	49.5	J	641			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_034-036CM	FS	52.1	J	455			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_036-038CM	FS	54.5	J	234			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_038-040CM	FS	57	J	203			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_040-045CM	FS	58	J	128			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_045-050CM	FS	59.5	J	84.8			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_050-055CM	FS	63.6	J	51.8			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_055-060CM	FS	65.3	J	46			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_060-065CM	FS	68.7	J	20.2			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_065-070CM	FS	68.4	J	21.8			
1711172	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_070-075CM	FS	71.8	J	27.2			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_000-001CM	FS	41.3	J	668			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_001-002CM	FS	40.6	J	680			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_004-005CM	FS	41.7	J	631			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_011-012CM	FS	40.1	J	935			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_014-015CM	FS	48.3	J	754			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_015-016CM	FS	46	J	682			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_016-017CM	FS	49	J	541			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_017-018CM	FS	43.5	J	878			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_019-020CM	FS	39.4	J	723			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_020-022CM	FS	39.8	J	786			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_022-024CM	FS	40.6	J	968			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_024-026CM	FS	38.9	J	979			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_026-028CM	FS	37.3	J	986			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_028-030CM	FS	39.7	J	936			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_030-032CM	FS	38.8	J	1010			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_032-034CM	FS	42.1	J	1010			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_034-036CM	FS	42.5	J	1090			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_036-038CM	FS	39.9	J	1220			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_038-040CM	FS	41.5	J	1170			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_040-045CM	FS	40.3	J	1260			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_045-050CM	FS	40.8	J	1530			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_050-055CM	FS	44.2	J	1440			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_055-060CM	FS	40.9	J	1800			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_060-065CM	FS	47.6	J	1630			
1711304	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_065-070CM	FS	39.6	J	3190			
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_000-001CM	FS					5.195	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_001-002CM	FS					3.475	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_003-004CM	FS					3.295	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_005-006CM	FS					3.405	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_006-007CM	FS					2.81	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_007-008CM	FS					2.375	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_014-015CM	FS					1.155	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_017-018CM	FS					1.305	

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DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_020-022CM	FS					2.26	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_022-024CM	FS					2.645	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_024-026CM	FS					2.255	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_026-028CM	FS					1.965	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_028-030CM	FS					2.45	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_030-032CM	FS					2.285	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_032-034CM	FS					2.33	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_034-036CM	FS					2.14	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_036-038CM	FS					1.585	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_038-040CM	FS					1.72	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_040-045CM	FS					1.65	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_045-050CM	FS					1.75	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_050-055CM	FS					1.66	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_055-060CM	FS					1.58	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_060-065CM	FS					1.415	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_065-070CM	FS					1.63	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_070-075CM	FS					3.32	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_075-080CM	FS					1.645	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_080-085CM	FS					2.02	
L1732772	PBR-26-A	9/11/2017	PBR-26-A-17_SED_085-090CM	FS					1.895	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_000-001CM	FS					9.925	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_001-002CM	FS					9.875	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_003-004CM	FS					8.38	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_004-005CM	FS					8.095	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_005-006CM	FS	36.8				7.69	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_006-007CM	FS	38.7				8.715	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_007-008CM	FS	34.4				7.855	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_008-009CM	FS	40.8				7.705	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_009-010CM	FS	37.2				8.655	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_010-011CM	FS					8.615	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_011-012CM	FS	37.8				9.405	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_012-013CM	FS	34.5				8.655	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_014-015CM	FS	36.9				9.06	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_015-016CM	FS	35.2				9.695	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_016-017CM	FS					10.53	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_017-018CM	FS					11.8	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_018-019CM	FS					13.55	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_019-020CM	FS	36				8.945	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_020-022CM	FS	36.4				9.845	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_022-024CM	FS	36.3				8.505	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_024-026CM	FS	35.6				9.165	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_026-028CM	FS	35.6				10.035	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_028-030CM	FS	37.8				10.65	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_030-032CM	FS	40.9				8.835	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_032-034CM	FS	37.1				9.9	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_034-036CM	FS	38				9.015	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_036-038CM	FS	39.3				8.335	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_038-040CM	FS	39.5				9.04	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_040-045CM	FS	38.8				9.37	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_045-050CM	FS	35.5				10.85	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_050-055CM	FS	36.7				8.995	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_055-060CM	FS	36.8				9.695	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_060-065CM	FS	36.8				9.58	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_065-070CM	FS	34.5				10.015	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method Parameter Unit Fraction		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_070-075CM	FS	37.8				10.2	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_075-080CM	FS	41.6				8.22	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_080-085CM	FS	41.1				9.09	
L1732773	OR-T3-C2-C	9/12/2017	OR-T3-C2-C-17_SED_085-090CM	FS	40.4				8.52	
L1732773	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_090-095CM	FS	42.7				6.89	
L1732773	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_095-100CM	FS	48.3				5.49	
L1732773	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_100-105CM	FS	51.1				4.95	
L1732773	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_105-110CM	FS	52				4.34	
L1732773	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_110-115CM	FS	55.4				3.84	
L1732773	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_115-120CM	FS	59.1				2.875	
L1732773	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_120-125CM	FS	61.5				2.56	
L1732773	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_125-130CM	FS	60.7				2.28	
L1732773	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_130-135CM	FS	61.4				2.76	
L1732773	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_135-140CM	FS	62.2				2.415	
L1732773	OR-T3-C2-C	9/13/2017	OR-T3-C2-C-17_SED_140-145CM	FS	60.6				2.37	J
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_000-001CM	FS	11.3	J			3.845	J
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_001-002CM	FS	39				4.045	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_002-003CM	FS	38.6				4.21	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_003-004CM	FS	44.2				3.92	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_004-005CM	FS	42.4				4.535	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_015-016CM	FS	39.4				3.8	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_017-018CM	FS	41.6				3.69	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_020-022CM	FS	43.5				3.005	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_022-024CM	FS	43.1				2.93	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_024-026CM	FS	49.5				2.7	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_026-028CM	FS	9.71				2.775	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_028-030CM	FS	37.7				3.1	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_030-032CM	FS	41.7				2.91	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_032-034CM	FS	52.9				2.615	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_034-036CM	FS	53.4				1.96	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_036-038CM	FS	52.8				2.05	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_038-040CM	FS	40.8				2.19	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_040-045CM	FS	8.52				1.7	J
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_045-050CM	FS	59.4				2.425	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_050-055CM	FS	46.5				1.295	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_055-060CM	FS	53.7				1.865	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_060-065CM	FS	50				1.67	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_065-070CM	FS	55.2				1.66	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_070-075CM	FS	50.5				1.645	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_075-080CM	FS	53.3				1.645	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_080-085CM	FS	60.9				1.44	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_085-090CM	FS	55.3				1.68	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_090-095CM	FS	57.9				1.225	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_095-100CM	FS	56.9				1.495	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_100-105CM	FS	65.8				1.265	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_105-110CM	FS	63.6				0.9625	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_110-115CM	FS	59.5				1.38	
L1735008	ES-01-C3	9/25/2017	ES-01-C3-17_SED_115-120CM	FS	65.7				1.225	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_001-002CM	FS	51.9				2.53	J
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_002-003CM	FS	56.2				2.56	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_003-004CM	FS	49.7				2.965	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_004-005CM	FS	51				3.355	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_005-006CM	FS	51.3				3.1	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_007-008CM	FS	49.3				2.53	

**TABLE 3
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_008-009CM	FS	50.4				3.345	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_010-011CM	FS	54				2.725	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_011-012CM	FS	49.1				2.495	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_012-013CM	FS	57.4				1.99	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_013-014CM	FS	16.7				3.195	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_014-015CM	FS	58				1.78	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_015-016CM	FS	47.9				1.745	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_016-017CM	FS	59				2.27	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_017-018CM	FS	56.8				1.975	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_018-019CM	FS	57.8				1.505	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_019-020CM	FS	60.8				1.65	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_020-022CM	FS	57.1				1.485	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_022-024CM	FS	56				1.545	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_024-026CM	FS	59.1				1.215	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_026-028CM	FS	61.2				1.24	J
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_028-030CM	FS	62.2				1.25	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_030-032CM	FS	59.1				1.475	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_032-034CM	FS	31.2				1.355	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_034-036CM	FS	61.4				1.555	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_036-038CM	FS	57.8				1.465	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_038-040CM	FS	57.7				1.395	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_040-045CM	FS	60.3				1.45	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_045-050CM	FS	60.1				1.385	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_050-055CM	FS	57.4				1.485	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_055-060CM	FS	58.7				1.3	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_060-065CM	FS	68.3				1.0085	
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_065-070CM	FS	65.8				1.19	

**TABLE 3
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1735009	ES-18-B	9/25/2017	ES-18-B-17_SED_070-075CM	FS	30				1.18	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_001-002CM	FS	29	J			7.25	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_002-003CM	FS	38.2				7.375	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_008-009CM	FS	21.9				9.04	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_010-011CM	FS	29.1				9.755	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_014-015CM	FS	37.1				7.54	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_018-019CM	FS	32.4				8.835	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_019-020CM	FS	37.7				8.385	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_020-022CM	FS	35.8				8.11	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_022-024CM	FS	37.5				8.69	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_024-026CM	FS	13.2				9.19	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_026-028CM	FS	33.3				9.24	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_028-030CM	FS	36.7	J			8.955	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_030-032CM	FS	34.9				9.53	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_032-034CM	FS	35.1				8.97	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_034-036CM	FS	32.4				12.55	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_036-038CM	FS	37				10.6	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_038-040CM	FS	39.3				9.505	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_040-045CM	FS	45				10.27	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_045-050CM	FS	40				10.075	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_050-055CM	FS	13.2				9.855	
L1735010	PBR-18-E	9/26/2017	PBR-18-E-17_SED_055-060CM	FS	47.3				8.65	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_000-001CM	FS	55.3				4.825	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_001-002CM	FS	51.5				5.625	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_002-003CM	FS	36.4				5.085	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_003-004CM	FS	55.6				4.225	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_004-005CM	FS	23.7				6.105	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_006-007CM	FS	59.6				4.46	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_008-009CM	FS	59.8				3.42	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_009-010CM	FS	40				2.74	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_011-012CM	FS	60.2				2.84	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_012-013CM	FS	60.4				2.8	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_013-014CM	FS	38.2				3.575	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_016-017CM	FS	36.5				5.69	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_017-018CM	FS	53.9				3.475	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_018-019CM	FS	56.2				2.925	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_020-022CM	FS	63.1				2.245	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_022-024CM	FS	61.5				3	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_024-026CM	FS	54.4				3.39	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_026-028CM	FS	60.6				3.04	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_028-030CM	FS	60.8				2.7	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_030-032CM	FS	60.3				2.15	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_032-034CM	FS	64.2				2.72	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_034-036CM	FS	51.8				1.405	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_036-038CM	FS	47.8				2.745	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_038-040CM	FS	57.4				3.19	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_040-045CM	FS	60.2				2.885	
L1735011	PBR-20-E	9/26/2017	PBR-20-E-17_SED_045-050CM	FS	63.8				2.255	
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_030-032CM	FS					13.85	
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_036-038CM	FS					8.915	
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_038-040CM	FS					10.5	
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_040-045CM	FS	28.8				8.91	
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_045-050CM	FS	45.1				4.045	
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_050-055CM	FS	47.7				4.025	

TABLE 3
DATA VALIDATION SUMMARY
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_055-060CM	FS	38				6.085	
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_060-065CM	FS	28.1				8.29	
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_065-070CM	FS	31.3				7.45	
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_070-075CM	FS	37				5.6	
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_075-080CM	FS	39.7				5.455	
L1736452	MM-T2-C1-B	10/2/2017	MM-T2-C1-B-17_SED_080-085CM	FS	41.8				5.855	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_002-003CM	FS	40				4.32	J
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_011-012CM	FS	18.3				3.47	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_014-015CM	FS	25.8				4.01	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_015-016CM	FS	40.5				4.125	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_019-020CM	FS	33.3				4.815	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_020-022CM	FS	36.4				4.96	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_022-024CM	FS	34.8				4.435	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_024-026CM	FS	13.6				4.245	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_026-028CM	FS	24.1				5.11	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_028-030CM	FS	33.3				5.335	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_030-032CM	FS	27.8				5.38	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_032-034CM	FS	35.2				5.63	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_034-036CM	FS	32.9				5.58	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_036-038CM	FS	35				4.84	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_038-040CM	FS	33.3				6.045	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_040-045CM	FS	34.5				6.3	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_045-050CM	FS	37				5.76	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_050-055CM	FS	33.3				6.47	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_055-060CM	FS	41.4				5.79	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_060-065CM	FS	39				7.165	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_065-070CM	FS	42.6				5.88	

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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_070-075CM	FS	41.6				5.81	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_075-080CM	FS	7.73				9.435	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_080-085CM	FS	42.9				5.94	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_085-090CM	FS	23.3				7.065	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_090-095CM	FS	25.4				7.81	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_095-100CM	FS	38.7				6.27	
L1736457	UPB-MU11-GC-1-C2	9/27/2017	UPB-MU11-GC-1-C2-17_SED_100-105CM	FS	33.3				8.855	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_000-001CM	FS					9.88	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_001-002CM	FS	36				10.9	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_002-003CM	FS	33.3				7.505	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_003-004CM	FS					6.15	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_004-005CM	FS	16.8				4.305	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_005-006CM	FS	42.5				2.77	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_006-007CM	FS	43.9				8.455	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_007-008CM	FS	59				1.095	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_008-009CM	FS	49.2				1.64	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_009-010CM	FS	59.1				1.73	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_010-011CM	FS	59.4				1.335	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_011-012CM	FS	66.9				0.9665	J
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_012-013CM	FS	64.8				1.41	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_013-014CM	FS	68.3				1.19	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_014-015CM	FS	67.4				1.16	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_015-016CM	FS	65.5				1.385	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_016-017CM	FS	62.8				2.16	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_017-018CM	FS	67.7				1.49	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_018-019CM	FS	62.3				1.465	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_019-020CM	FS	69				1.98	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_020-022CM	FS	67				1.465	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_022-024CM	FS	67.5				1.086	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_024-026CM	FS	66.2				1.64	J
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_026-028CM	FS	69.2				1.405	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_028-030CM	FS	69.2				1.565	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_030-032CM	FS	70.8				1.73	J
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_032-034CM	FS	71.2				1.215	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_034-036CM	FS	73				1.0915	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_036-038CM	FS	73.6				2.09	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_038-040CM	FS	77.5				1.58	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_040-045CM	FS	72				2.065	J
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_045-050CM	FS	66.7				1.03	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_050-055CM	FS	62.3				1.08	
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_055-060CM	FS	85.9				1.177	J
L1736459	VE-MU4-GC-1-E	9/27/2017	VE-MU4-GC-1-E-17_SED_060-065CM	FS	82.3				0.988	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_020-022CM	FS	54.3				4.715	J
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_022-024CM	FS	50.5				4.52	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_024-026CM	FS	17.9				5.545	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_026-028CM	FS	53.4				3.275	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_028-030CM	FS	54.6				3.82	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_030-032CM	FS	53.6				3.055	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_032-034CM	FS	55.6				3.155	J
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_034-036CM	FS	57.8				2.355	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_036-038CM	FS	56.8				4.62	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_038-040CM	FS	54.4				3.065	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_040-045CM	FS	58.3				2.59	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_045-050CM	FS	54.4				2.505	J

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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_050-055CM	FS	38.9				4.01	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_055-060CM	FS	57.3				2.305	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_060-065CM	FS	72.2				1.4	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_065-070CM	FS	75.5				1.24	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_070-075CM	FS	66.7				1.61	J
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_075-080CM	FS	71.8				1.51	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_080-085CM	FS	66.1				1.595	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_085-090CM	FS	67.6				1.775	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_090-095CM	FS	67				1.435	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_095-100CM	FS	69.3				1.34	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_100-105CM	FS	46.7				1.5	
L1736460	VN-MU3-GC-1-D	9/27/2017	VN-MU3-GC-1-D-17_SED_105-110CM	FS	67.1				1.5	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_000-001CM	FS	49.3				4.595	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_003-004CM	FS	77.3				1.15	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_004-005CM	FS	83.6				0.7975	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_005-006CM	FS	79.4				1.0495	J
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_006-007CM	FS					0.9695	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_007-008CM	FS	81.2				1.0555	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_008-009CM	FS	81.4				1.175	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_009-010CM	FS	81.2				1.09	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_010-011CM	FS	84				1	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_011-012CM	FS	81.2				1.1	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_012-013CM	FS	77.6				1.245	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_013-014CM	FS	80.2				1.147	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_014-015CM	FS	78.6				1.425	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_015-016CM	FS					1.43	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_016-017CM	FS	78.6				1.285	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_017-018CM	FS	75.8				1.155	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_018-019CM	FS	73.2				1.62	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_019-020CM	FS	69.7				1.775	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_020-022CM	FS	69.6				1.52	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_022-024CM	FS	72.6				1.875	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_024-026CM	FS	70.6				1.825	J
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_026-028CM	FS	71.7				1.955	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_028-030CM	FS	70.3				1.35	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_030-032CM	FS	73.8				2.03	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_032-034CM	FS	76.6				1.59	J
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_034-036CM	FS	70.2				1.58	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_036-038CM	FS	69.8				1.54	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_038-040CM	FS	72.2				1.635	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_040-045CM	FS	67.8				1.605	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_045-050CM	FS	66.1				2.115	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_050-055CM	FS	72.3				1.895	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_055-060CM	FS	68.7				1.68	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_060-065CM	FS	69.1				1.635	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_065-070CM	FS	67.7				1.685	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_070-075CM	FS	66.1				1.67	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_075-080CM	FS	66.4				1.94	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_080-085CM	FS	62.9				1.965	
L1739126	FF-MU7-GC-1-B	10/18/2017	FF-MU7-GC-1-B-17_SED_085-090CM	FS	61.4				2.21	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_020-022CM	FS	37.2				7.63	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_022-024CM	FS	41.8				7.985	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_024-026CM	FS	39.7				9.415	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_026-028CM	FS	32.5				9.29	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	Mercury		TOC	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_028-030CM	FS	38.5				9.01	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_030-032CM	FS	34.6				9.845	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_032-034CM	FS	39				9.5	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_034-036CM	FS	38.6				9.175	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_036-038CM	FS	39.2				8.395	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_038-040CM	FS	41.6				8.055	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_040-045CM	FS	42.8				7.015	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_045-050CM	FS	42.9				7.63	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_050-055CM	FS	43				8.105	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_055-060CM	FS	42.7				8.02	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_060-065CM	FS	43.4				8.44	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_065-070CM	FS	42.9				8.13	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_070-075CM	FS	46.6				7.805	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_075-080CM	FS	56.8				4.325	J
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_080-085CM	FS	53.5				6.085	
L1740286	MM-T4-C2-D	10/26/2017	MM-T4-C2-D-17_SED_085-090CM	FS	49.4				7.505	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_020-022CM	FS	43.8				5.455	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_022-024CM	FS	42.2				5.825	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_024-026CM	FS	38.9				5.445	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_026-028CM	FS	40				6.7	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_028-030CM	FS	38.3				7.68	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_030-032CM	FS	41.1				6.71	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_032-034CM	FS	40.7				6.8	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_034-036CM	FS	43.9				7.375	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_036-038CM	FS	40				7.465	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_038-040CM	FS	38.7				8.735	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_040-045CM	FS	36.2				8.955	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method Parameter Unit Fraction		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_045-050CM	FS	37.4				9.415	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_050-055CM	FS	38.9				8.375	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_055-060CM	FS	40.6				9.11	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_060-065CM	FS	36.8				8.335	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_065-070CM	FS	43.9				6.695	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_070-075CM	FS	37.4				8.065	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_075-080CM	FS	36.4				10.435	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_080-085CM	FS	38.6				8.135	
L1740288	OR-T2-C5-B	10/31/2017	OR-T2-C5-B-17_SED_085-090CM	FS	34.4				7.325	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_020-022CM	FS	41.2				7.28	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_022-024CM	FS	46.8				6.63	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_024-026CM	FS	44.8				6.645	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_026-028CM	FS	36.7				8.195	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_028-030CM	FS	40.6				8.17	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_032-034CM	FS	48.5				7.25	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_034-036CM	FS	51.6				6.71	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_036-038CM	FS	54.3				6.22	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_038-040CM	FS	56.2				5.435	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_040-045CM	FS	56.2				4.78	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_045-050CM	FS	58.8				4.31	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_050-055CM	FS	61.7				3.57	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_055-060CM	FS	68.6				2.82	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_060-065CM	FS	62.8				2.285	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_065-070CM	FS	68.2				2.2	
L1740290	OR-T3-C5-D	10/25/2017	OR-T3-C5-D-17_SED_070-075CM	FS	68.8				2.165	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_000-001CM	FS	41.7				5.74	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_004-005CM	FS	42.4				5.525	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT		EPA 1631 Mercury NG/G		LLOYD KAHN TOC PERCENT	
					Total Final Result	Total Final Qualifier	Total Final Result	Total Final Qualifier	Total Final Result	Total Final Qualifier
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_016-017CM	FS					3.975	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_020-022CM	FS	48				5.5	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_022-024CM	FS	40.2				5.87	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_024-026CM	FS	40.9				5.825	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_026-028CM	FS	38.7				5.975	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_028-030CM	FS	37.8				5.65	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_030-032CM	FS	37.7				5.85	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_032-034CM	FS	37.7				5.38	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_034-036CM	FS	40				5.925	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_036-038CM	FS	41.8				5.68	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_038-040CM	FS	37.6				6.245	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_040-045CM	FS	39.6				6.42	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_045-050CM	FS	38.2				7.15	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_050-055CM	FS	42.7				5.765	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_055-060CM	FS	39.7				7.085	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_060-065CM	FS	44.4				5.62	
L1741134	UPB-MU11-GC-1-D	11/1/2017	UPB-MU11-GC-1-D-17_SED_065-070CM	FS	42.6				5.535	

Notes:

NG/G = Nanogram per gram

FS = Field Sample

J = Value is estimated

SDG = Sample Delivery Group

**Data Validation Summary
 2017 Geochronology Interval Core Sediment Sampling
 Penobscot River Estuary Phase III – Engineering Evaluation
 Penobscot River, Maine**

1.0 INTRODUCTION

Sediment samples were collected in August through November 2017 from the Penobscot River located in Maine. Samples were analyzed by Flett Research, Ltd. (Flett) located in Winnipeg, Manitoba, Canada and included cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28. Samples were analyzed by the following: United States Environmental Protection Agency (EPA) SW-846 Compendium:

Laboratory	Parameter	Analytical Method	Validation Level
Flett Research, Ltd.	Mercury, total	EPA Method 7473M	10% Stage III/ 90% Stage IIB

Stage IIB data validation was performed on all samples. Stage III data validation was performed on ten percent of samples. Data validation was completed in accordance with National Functional Guidelines for Inorganic Superfund Data Review (USEPA, 2017), EPA New England Environmental Data Review Supplement for Regional Data Review Elements, and Superfund Specific Guidance/Procedures (USEPA, 2013) as applicable. Data quality evaluations were completed using quality control (QC) limits specified in the draft Penobscot River Estuary Phase III Engineering Evaluation Quality Assurance Project Plan (QAPP) [Amec Foster Wheeler, 2016]. The project laboratory reported results using a combination of two detection limits: the reporting limit (RL) and the method detection limit (MDL). Results for compounds that are not detected in samples are reported as U qualified results at the RL. Positive detections between the MDL and RL are qualified as estimated (J) by the laboratory.

Data validation review and qualification actions are discussed in the following subsections. It should be noted that only instances that result in an impact to data quality are presented in this report. There may be QC elements outside of QAPP and/or method control limits not presented in this report if there is no impact on data quality. Samples included in this data evaluation are presented in Table 1.

Data qualifications were completed, if necessary, in accordance with the guidelines or the professional judgment of the project chemist. The following qualifiers as applied during data validation or reported by the laboratory are included in the final data set:

- J = The reported concentration is considered an estimated value
- U = The target compound was not detected above the method detection limit

Validation reason codes were applied to results associated with QC measurements outside project QC limits. The validation qualification actions and associated validation reason codes applied to sample results are summarized in Table 2. The following data validation reason codes were applied to one or more sample results:

LR = Laboratory replicate % relative standard deviation (RSD) limit exceeded, potential analytical imprecision.

A complete summary of final sample results is provided in Table 3.

Data were evaluated based on the following parameters:

- * Data Completeness and Chain of Custody
- * Holding Times and Preservation
- * Blanks
- * Initial Calibration
- * Continuing Calibration
- * Laboratory Control Sample (LCS)
- * Matrix Spike/Matrix Spike Duplicates (MS/MSD)
- Laboratory Duplicates
- * Field Duplicates
- * Detection Limits
- * Sample Result Verification/Electronic Evaluation Verification (EDD)
- * Ongoing Precision Recovery

* indicates that criteria were met and/or that there was no impact to data quality for this parameter

With the exception of the following item, results were determined to be usable as reported by the laboratory.

2.0 Mercury – 7473

Laboratory Triplicate

TMDSOL092717AL1 – A laboratory triplicate was performed on sample PBR-04-C-17_SED_014-015CM. The RSD (29.7%) exceeded the QC limit of 20%. The sample result for PBR-04-C-17_SED_014-015CM was qualified as estimated due to potential analytical imprecision. (J-LR)

References:

Amec Foster Wheeler, 2016. "Draft Penobscot River Estuary Phase III – Engineering Study Quality Assurance Project Plan", Penobscot River, Maine, July 2016.

U.S. Environmental Protection Agency (USEPA), 2004. "Final Update IIIB and Method 9071B of Final Update IIIA"; Test Methods for Evaluating Solid Waste Physical/Chemical Methods SW-846; Office of Solid Waste and Emergency Response, EPA-SW-846-03-03B; November 2004.

U.S. Environmental Protection Agency (USEPA), 2009. "Guidance for Labeling Externally Validated Laboratory Analytical data for Superfund Use"; Office of Solid Waste and Emergency Response; EPA 540-R-08-005; January 13, 2009.

U.S. Environmental Protection Agency (USEPA), 2017. "National Functional Guidelines for Inorganic Superfund Data Review"; Office of Superfund Remediation and Technology Innovation; EPA-540-R-2017-001; January 2017.

U.S. Environmental Protection Agency (USEPA), 2013. "EPA New England Environmental Data Review Supplement for Regional Data Review Elements and Superfund Specific Guidance/Procedures"; Quality Assurance Unit Staff; Office of Environmental Measurement and Evaluation; April 22, 2013.

Data Validator: Bjorn Ottosson

December 27, 2017



Senior Reviewer: Denise King

January 2, 2018

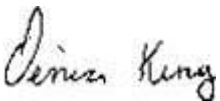


TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 7473 Count
					Analysis Method	% Solids Count	
ES-17	SED	ES-17-C	ES-17-C-17_SED_000-001CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_001-002CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_002-003CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_003-004CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_004-005CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_005-006CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_006-007CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_007-008CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_008-009CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_009-010CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_010-011CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_011-012CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_012-013CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_013-014CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_014-015CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_015-016CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_016-017CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_017-018CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_018-019CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_019-020CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_020-022CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_022-024CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_024-026CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_026-028CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_028-030CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_030-032CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_032-034CM	08/17/17	FS	1	1

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
ES-17	SED	ES-17-C	ES-17-C-17_SED_034-036CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_036-038CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_038-040CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_040-045CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_045-050CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_050-055CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_055-060CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_060-065CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_065-070CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_070-075CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_075-080CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_080-085CM	08/17/17	FS	1	1
ES-17	SED	ES-17-C	ES-17-C-17_SED_085-090CM	08/17/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_000-001CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_001-002CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_002-003CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_003-004CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_004-005CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_005-006CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_006-007CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_007-008CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_008-009CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_009-010CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_010-011CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_011-012CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_012-013CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_013-014CM	09/15/17	FS	1	1

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
ES-20	SED	ES-20-A	ES-20-A-17_SED_014-015CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_015-016CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_016-017CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_017-018CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_018-019CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_019-020CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_020-022CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_022-024CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_024-026CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_026-028CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_028-030CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_030-032CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_032-034CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_034-036CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_036-038CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_038-040CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_040-045CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_045-050CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_050-055CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_055-060CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_060-065CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_065-070CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_070-075CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_075-080CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_080-085CM	09/15/17	FS	1	1
ES-20	SED	ES-20-A	ES-20-A-17_SED_085-090CM	09/15/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_000-001CM	09/27/17	FS	1	1

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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 7473 Count
					Analysis Method	% Solids Count	
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_001-002CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_002-003CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_003-004CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_004-005CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_005-006CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_006-007CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_007-008CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_008-009CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_009-010CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_010-011CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_011-012CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_012-013CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_013-014CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_014-015CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_015-016CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_016-017CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_017-018CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_018-019CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_019-020CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_020-022CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_022-024CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_024-026CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_026-028CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_028-030CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_030-032CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_032-034CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_034-036CM	09/27/17	FS	1	1

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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_036-038CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_038-040CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_040-045CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_045-050CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_050-055CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_055-060CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_060-065CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_065-070CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_070-075CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_075-080CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_080-085CM	09/27/17	FS	1	1
MM-C2	SED	MM-C2-C	MM-C2-C-17_SED_085-090CM	09/27/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_000-001CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_001-002CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_002-003CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_003-004CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_004-005CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_005-006CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_006-007CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_007-008CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_008-009CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_009-010CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_010-011CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_011-012CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_012-013CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_013-014CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_014-015CM	10/17/17	FS	1	1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 7473 Count
					Analysis Method	% Solids Count	
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_015-016CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_016-017CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_017-018CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_018-019CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_019-020CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_020-022CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_022-024CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_024-026CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_026-028CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_028-030CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_030-032CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_032-034CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_034-036CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_036-038CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_038-040CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_040-045CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_045-050CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_050-055CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_055-060CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_060-065CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_065-070CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_070-075CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_075-080CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_080-085CM	10/17/17	FS	1	1
MM-C3	SED	MM-C3-A	MM-C3-A-17_SED_085-090CM	10/17/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_000-001CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_001-002CM	10/24/17	FS	1	1

TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_002-003CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_003-004CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_004-005CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_005-006CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_006-007CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_007-008CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_008-009CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_009-010CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_010-011CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_011-012CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_012-013CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_013-014CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_014-015CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_015-016CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_016-017CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_017-018CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_018-019CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_019-020CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_020-022CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_022-024CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_024-026CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_026-028CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_028-030CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_030-032CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_032-034CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_034-036CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_036-038CM	10/24/17	FS	1	1

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2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_038-040CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_040-045CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_045-050CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_050-055CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_055-060CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_060-065CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_065-070CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_070-075CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_075-080CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_080-085CM	10/24/17	FS	1	1
MM-T2-C2	SED	MM-T2-C2-A	MM-T2-C2-A-17_SED_085-090CM	10/24/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_000-001CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_001-002CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_002-003CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_003-004CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_004-005CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_005-006CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_006-007CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_007-008CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_008-009CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_009-010CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_010-011CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_011-012CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_012-013CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_013-014CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_014-015CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_015-016CM	10/10/17	FS	1	1

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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 7473 Count
					Analysis Method	% Solids Count	
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_016-017CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_017-018CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_018-019CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_019-020CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_020-022CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_022-024CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_024-026CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_026-028CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_028-030CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_030-032CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_032-034CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_034-036CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_036-038CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_038-040CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_040-045CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_045-050CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_050-055CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_055-060CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_060-065CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_065-070CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_070-075CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_075-080CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_080-085CM	10/10/17	FS	1	1
MM-T2-C3	SED	MM-T2-C3-A	MM-T2-C3-A-17_SED_085-090CM	10/10/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_000-001CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_001-002CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_002-003CM	10/03/17	FS	1	1

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 7473 Count
					Analysis Method	% Solids Count	
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_003-004CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_004-005CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_005-006CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_006-007CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_007-008CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_008-009CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_009-010CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_010-011CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_011-012CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_012-013CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_013-014CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_014-015CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_015-016CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_016-017CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_017-018CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_018-019CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_019-020CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_020-022CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_022-024CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_024-026CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_026-028CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_028-030CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_030-032CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_032-034CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_034-036CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_036-038CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_038-040CM	10/03/17	FS	1	1

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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 7473 Count
					Analysis Method	% Solids Count	
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_040-045CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_045-050CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_050-055CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_055-060CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_060-065CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_065-070CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_070-075CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_075-080CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_080-085CM	10/03/17	FS	1	1
MM-T3-C5	SED	MM-T3-C5-C	MM-T3-C5-C-17_SED_085-090CM	10/03/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_000-001CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_001-002CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_002-003CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_003-004CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_004-005CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_005-006CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_006-007CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_007-008CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_008-009CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_009-010CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_010-011CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_011-012CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_012-013CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_013-014CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_014-015CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_015-016CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_016-017CM	10/28/17	FS	1	1

TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 7473 Count
					Analysis Method	% Solids Count	
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_017-018CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_018-019CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_019-020CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_020-022CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_022-024CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_024-026CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_026-028CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_028-030CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_030-032CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_032-034CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_034-036CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_036-038CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_038-040CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_040-045CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_045-050CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_050-055CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_055-060CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_060-065CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_065-070CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_070-075CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_075-080CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_080-085CM	10/28/17	FS	1	1
MM-T4-C3	SED	MM-T4-C3-C	MM-T4-C3-C-17_SED_085-090CM	10/28/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_000-001CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_001-002CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_002-003CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_003-004CM	10/24/17	FS	1	1

TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 7473 Count
					Analysis Method	% Solids Count	
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_004-005CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_005-006CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_006-007CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_007-008CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_008-009CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_009-010CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_010-011CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_011-012CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_012-013CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_013-014CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_014-015CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_015-016CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_016-017CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_017-018CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_018-019CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_019-020CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_020-022CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_022-024CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_024-026CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_026-028CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_028-030CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_030-032CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_032-034CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_034-036CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_036-038CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_038-040CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_040-045CM	10/24/17	FS	1	1

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2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_045-050CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_050-055CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_055-060CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_060-065CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_065-070CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_070-075CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_075-080CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_080-085CM	10/24/17	FS	1	1
MM-T4-C4	SED	MM-T4-C4-A	MM-T4-C4-A-17_SED_085-090CM	10/24/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_000-001CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_001-002CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_002-003CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_003-004CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_004-005CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_005-006CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_006-007CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_007-008CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_008-009CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_009-010CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_010-011CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_011-012CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_012-013CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_013-014CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_014-015CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_015-016CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_016-017CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_017-018CM	10/12/17	FS	1	1

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2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_018-019CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_019-020CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_020-022CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_022-024CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_024-026CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_026-028CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_028-030CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_030-032CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_032-034CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_034-036CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_036-038CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_038-040CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_040-045CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_045-050CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_050-055CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_055-060CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_060-065CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_065-070CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_070-075CM	10/12/17	FS	1	1
OR-C1	SED	OR-C1-A	OR-C1-A-17_SED_075-079CM	10/12/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_000-001CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_001-002CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_002-003CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_003-004CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_004-005CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_005-006CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_006-007CM	10/28/17	FS	1	1

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_007-008CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_008-009CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_009-010CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_010-011CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_011-012CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_012-013CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_013-014CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_014-015CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_015-016CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_016-017CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_017-018CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_018-019CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_019-020CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_020-022CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_022-024CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_024-026CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_026-028CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_028-030CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_030-032CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_032-034CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_034-036CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_036-038CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_038-040CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_040-045CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_045-050CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_050-055CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_055-060CM	10/28/17	FS	1	1

TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_060-065CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_065-070CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_070-075CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_075-080CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_080-085CM	10/28/17	FS	1	1
OR-T1-C1	SED	OR-T1-C1	OR-T1-C1-17_SED_085-090CM	10/28/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_000-001CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_001-002CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_002-003CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_003-004CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_004-005CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_005-006CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_006-007CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_007-008CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_008-009CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_009-010CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_010-011CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_011-012CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_012-013CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_013-014CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_014-015CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_015-016CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_016-017CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_017-018CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_018-019CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_019-020CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_020-022CM	10/20/17	FS	1	1

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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_022-024CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_024-026CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_026-028CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_028-030CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_030-032CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_032-034CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_034-036CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_036-038CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_038-040CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_040-045CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_045-050CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_050-055CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_055-060CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_060-065CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_065-070CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_070-075CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_075-080CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_080-085CM	10/20/17	FS	1	1
OR-T2-C2	SED	OR-T2-C2-D	OR-T2-C2-D-17_SED_085-090CM	10/20/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_000-001CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_001-002CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_002-003CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_003-004CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_004-005CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_005-006CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_006-007CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_007-008CM	09/08/17	FS	1	1

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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 7473 Count
					Analysis Method	% Solids Count	
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_008-009CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_009-010CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_010-011CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_011-012CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_012-013CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_013-014CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_014-015CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_015-016CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_016-017CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_017-018CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_018-019CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_019-020CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_020-022CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_022-024CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_024-026CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_026-028CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_028-030CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_030-032CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_032-034CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_034-036CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_036-038CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_038-040CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_040-045CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_045-050CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_050-055CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_055-060CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_060-065CM	09/08/17	FS	1	1

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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_065-070CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_070-075CM	09/08/17	FS	1	1
PBR-04	SED	PBR-04-C	PBR-04-C-17_SED_075-080CM	09/08/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_000-001CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_001-002CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_002-003CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_003-004CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_004-005CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_005-006CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_006-007CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_007-008CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_008-009CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_009-010CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_010-011CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_011-012CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_012-013CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_013-014CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_014-015CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_015-016CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_016-017CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_017-018CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_018-019CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_019-020CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_020-022CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_022-024CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_024-026CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_026-028CM	09/06/17	FS	1	1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_028-030CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_030-032CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_032-034CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_034-036CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_036-038CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_038-040CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_040-045CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_045-050CM	09/06/17	FS	1	1
PBR-10	SED	PBR-10-A	PBR-10-A-17_SED_045-050CM	09/06/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_000-001CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_001-002CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_002-003CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_003-004CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_004-005CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_005-006CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_006-007CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_007-008CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_008-009CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_009-010CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_010-011CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_011-012CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_012-013CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_013-014CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_014-015CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_015-016CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_016-017CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_017-018CM	11/28/17	FS	1	1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 7473 Count
					Analysis Method	% Solids Count	
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_018-019CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_019-020CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_020-022CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_022-024CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_024-026CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_026-028CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_028-030CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_030-032CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_032-034CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_034-036CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_036-038CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_038-040CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_040-045CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_045-050CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_050-055CM	11/28/17	FS	1	1
PBR-16	SED	PBR-16-C	PBR-16-C-17_SED_055-057CM	11/28/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_000-001CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_001-002CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_002-003CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_003-004CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_004-005CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_005-006CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_006-007CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_007-008CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_008-009CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_009-010CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_010-011CM	08/17/17	FS	1	1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_011-012CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_012-013CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_013-014CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_014-015CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_015-016CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_016-017CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_017-018CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_018-019CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_019-020CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_020-022CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_022-024CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_024-026CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_026-028CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_028-030CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_030-032CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_032-034CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_034-036CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_036-038CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_038-040CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_040-045CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_045-050CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_050-055CM	08/17/17	FS	1	1
PBR-19	SED	PBR-19-A	PBR-19-A-17_SED_055-059CM	08/17/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_000-001CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_001-002CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_002-003CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_003-004CM	10/03/17	FS	1	1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_004-005CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_005-006CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_006-007CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_007-008CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_008-009CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_009-010CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_010-011CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_011-012CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_012-013CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_013-014CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_014-015CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_015-016CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_016-017CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_017-018CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_018-019CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_019-020CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_020-022CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_022-024CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_024-026CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_026-028CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_028-030CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_030-032CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_032-034CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_034-036CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_036-038CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_038-040CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_040-045CM	10/03/17	FS	1	1

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class	% Solids Count	Mercury
					Analysis Method QC Code		EPA 7473 Count
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_045-050CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_050-055CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_055-060CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_060-065CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_065-070CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_070-075CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_075-080CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_080-085CM	10/03/17	FS	1	1
PBR-28	SED	PBR-28-C	PBR-28-C-17_SED_085-090CM	10/03/17	FS	1	1

Notes:

- Count = # of analytes
- FD = Field Duplicate
- FS = Field Sample
- SDG = Sample Delivery Group
- SED = Sediment

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Fraction	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
PBR-04	EPA7473	84074	PBR-04-C-17_SED_014-015CM	T	Mercury	2.26		2.26	J	LR	NG/G

Units

NG/G = Nanograms per gram

Validation Qualifier:

J = Value is estimated

Validatio Reason Codes:

LR = Lab Replicate RSD limit exceeded

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	% Solids	Mercury
					Unit	PERCENT	NG/G
					Fraction	Total	Total
						Final Result	Final Qualifier
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_000-001CM	FS		63.3	583
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_001-002CM	FS		62.7	530
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_002-003CM	FS		63.2	551
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_003-004CM	FS		63.4	544
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_004-005CM	FS		61.6	499
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_005-006CM	FS		63.4	533
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_006-007CM	FS		61	457
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_007-008CM	FS		61.7	498
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_008-009CM	FS		61.7	514
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_009-010CM	FS		63.7	630
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_010-011CM	FS		63.2	712
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_011-012CM	FS		62.4	868
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_012-013CM	FS		62.7	780
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_013-014CM	FS		61.8	788
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_014-015CM	FS		61.7	933
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_015-016CM	FS		60.8	845
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_016-017CM	FS		60.1	973
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_017-018CM	FS		59.6	926
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_018-019CM	FS		59.3	995
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_019-020CM	FS		58.9	789
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_020-022CM	FS		61.3	1,110
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_022-024CM	FS		61.8	1,160
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_024-026CM	FS		61.6	1,100
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_026-028CM	FS		60.9	1,150

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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473		
					Parameter	Mercury		
					Unit	NG/G		
					Fraction	Total		
					Final Result	Final Qualifier	Final Result	Final Qualifier
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_028-030CM	FS	61.2		1,200	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_030-032CM	FS	59.6		950	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_032-034CM	FS	57.5		758	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_034-036CM	FS	58.8		903	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_036-038CM	FS	57.5		713	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_038-040CM	FS	56.8		555	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_040-045CM	FS	55		369	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_045-050CM	FS	51.1		348	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_050-055CM	FS	48.7		113	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_055-060CM	FS	47.6		68.1	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_060-065CM	FS	46.1		34.9	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_065-070CM	FS	44.6		29.9	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_070-075CM	FS	44.1		25.6	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_075-080CM	FS	47.3		19.4	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_080-085CM	FS	42.7		18.4	
ES-17	ES-17-C	08/17/17	ES-17-C-17_SED_085-090CM	FS	41.9		17.9	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_000-001CM	FS	61.4		586	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_001-002CM	FS	59.7		657	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_002-003CM	FS	59.6		598	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_003-004CM	FS	59.1		634	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_004-005CM	FS	58.8		637	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_005-006CM	FS	58.5		617	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_006-007CM	FS	59		632	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_007-008CM	FS	59.5		643	

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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	% Solids	Mercury
					Unit	PERCENT	NG/G
					Fraction	Total	Total
						Final Result	Final Qualifier
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_008-009CM	FS		58.7	679
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_009-010CM	FS		59.5	889
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_010-011CM	FS		60.6	1,390
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_011-012CM	FS		60.5	1,620
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_012-013CM	FS		59.8	1,550
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_013-014CM	FS		59.5	1,440
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_014-015CM	FS		58.5	1,270
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_015-016CM	FS		58.4	1,080
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_016-017CM	FS		59.6	746
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_017-018CM	FS		60.1	642
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_018-019CM	FS		60.2	630
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_019-020CM	FS		59.3	512
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_020-022CM	FS		58.6	588
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_022-024CM	FS		59.2	494
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_024-026CM	FS		58.5	347
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_026-028CM	FS		56.5	255
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_028-030CM	FS		57.3	220
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_030-032CM	FS		56.5	225
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_032-034CM	FS		54.5	153
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_034-036CM	FS		53.9	138
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_036-038CM	FS		53	122
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_038-040CM	FS		54.3	87.4
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_040-045CM	FS		50.7	75.5
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_045-050CM	FS		49.8	62.6

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473			
					Parameter	% Solids	Mercury		
					Unit	PERCENT	NG/G		
					Fraction	Total	Total		
						Final Result	Final Qualifier		
						Final Result	Final Qualifier		
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_050-055CM	FS		47.6		33.8	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_055-060CM	FS		49.7		32.4	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_060-065CM	FS		51.1		29.5	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_065-070CM	FS		50.2		27.5	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_070-075CM	FS		48.3		22.1	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_075-080CM	FS		48.1		21	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_080-085CM	FS		46.5		18	
ES-20	ES-20-A	09/15/17	ES-20-A-17_SED_085-090CM	FS		47.2		17.3	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_000-001CM	FS		56.1		584	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_001-002CM	FS		87.7		620	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_002-003CM	FS		54.5		559	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_003-004CM	FS		55.2		635	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_004-005CM	FS		53.9		757	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_005-006CM	FS		55.8		639	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_006-007CM	FS		55.8		823	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_007-008CM	FS		61.1		796	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_008-009CM	FS		57.3		715	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_009-010CM	FS		55.8		842	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_010-011CM	FS		53.9		871	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_011-012CM	FS		54.7		899	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_012-013CM	FS		56.9		1,180	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_013-014CM	FS		57		1,020	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_014-015CM	FS		56.9		1,100	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_015-016CM	FS		55.1		1,380	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473			
					Parameter	Mercury			
					Unit	% Solids	NG/G		
					Fraction	PERCENT	Total		
						Final Result	Final Qualifier		
						Final Result	Final Qualifier		
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_016-017CM	FS		57.7		1,320	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_017-018CM	FS		56.3		1,590	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_018-019CM	FS		56		1,620	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_019-020CM	FS		56.6		1,870	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_020-022CM	FS		55.9		2,440	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_022-024CM	FS		55.9		2,540	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_024-026CM	FS		61.2		3,980	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_026-028CM	FS		61.5		4,310	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_028-030CM	FS		61.8		2,380	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_030-032CM	FS		62.5		2,760	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_032-034CM	FS		63.4		3,280	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_034-036CM	FS		63.9		2,940	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_036-038CM	FS		66.2		3,140	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_038-040CM	FS		60.4		3,250	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_040-045CM	FS		59.3		1,850	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_045-050CM	FS		55.2		821	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_050-055CM	FS		60.3		676	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_055-060CM	FS		61		369	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_060-065CM	FS		59.6		307	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_065-070CM	FS		59.2		321	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_070-075CM	FS		58.7		343	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_075-080CM	FS		56.9		340	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_080-085CM	FS		55.8		354	
MM-C2	MM-C2-C	09/27/17	MM-C2-C-17_SED_085-090CM	FS		58.5		340	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	Mercury	
					Unit	NG/G	
					Fraction	Total	
						% Solids	
						PERCENT	
						Total	Total
						Final Result	Final Qualifier
						Final Result	Final Qualifier
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_000-001CM	FS		63.8	665
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_001-002CM	FS		63.6	787
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_002-003CM	FS		61.4	782
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_003-004CM	FS		64.4	705
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_004-005CM	FS		62.5	710
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_005-006CM	FS		62.2	728
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_006-007CM	FS		61.4	800
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_007-008CM	FS		62.7	1,150
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_008-009CM	FS		63.1	981
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_009-010CM	FS		60.7	989
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_010-011CM	FS		61.4	1,110
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_011-012CM	FS		61.9	1,640
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_012-013CM	FS		62.7	2,410
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_013-014CM	FS		60.7	2,950
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_014-015CM	FS		59	3,820
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_015-016CM	FS		60.3	5,180
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_016-017CM	FS		63.4	5,570
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_017-018CM	FS		63.8	4,620
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_018-019CM	FS		61	3,260
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_019-020CM	FS		55.2	1,910
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_020-022CM	FS		51	2,020
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_022-024CM	FS		58.6	2,850
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_024-026CM	FS		46	664
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_026-028CM	FS		47.2	919

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	Mercury	
					Unit	% Solids	NG/G
					Fraction	PERCENT	Total
						Final Result	Final Qualifier
						Final Result	Final Qualifier
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_028-030CM	FS		58.6	3,220
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_030-032CM	FS		55.3	2,250
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_032-034CM	FS		63.5	2,380
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_034-036CM	FS		62.1	1,560
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_036-038CM	FS		61.8	687
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_038-040CM	FS		64.4	470
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_040-045CM	FS		63.5	353
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_045-050CM	FS		62.1	342
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_050-055CM	FS		63.1	373
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_055-060CM	FS		63.2	399
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_060-065CM	FS		61.2	404
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_065-070CM	FS		63.2	376
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_070-075CM	FS		58.7	338
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_075-080CM	FS		57.6	277
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_080-085CM	FS		58.3	236
MM-C3	MM-C3-A	10/17/17	MM-C3-A-17_SED_085-090CM	FS		56.1	187
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_000-001CM	FS		69.8	570
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_001-002CM	FS		66.8	621
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_002-003CM	FS		69.2	549
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_003-004CM	FS		67.4	706
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_004-005CM	FS		67.9	612
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_005-006CM	FS		68.2	640
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_006-007CM	FS		68.2	708
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_007-008CM	FS		67.1	832

TABLE 3
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2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	Mercury	
					Unit	% Solids	NG/G
					Fraction	PERCENT	Total
						Final Result	Final Qualifier
						Final Result	Final Qualifier
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_008-009CM	FS		66.7	914
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_009-010CM	FS		67.8	1,140
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_010-011CM	FS		66.1	1,290
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_011-012CM	FS		67.9	1,700
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_012-013CM	FS		68.8	2,030
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_013-014CM	FS		69.1	2,460
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_014-015CM	FS		67	3,220
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_015-016CM	FS		66.8	3,960
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_016-017CM	FS		67	4,280
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_017-018CM	FS		67.9	4,650
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_018-019CM	FS		70.8	4,730
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_019-020CM	FS		71.4	5,490
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_020-022CM	FS		66.7	3,250
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_022-024CM	FS		69.6	1,340
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_024-026CM	FS		67.7	434
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_026-028CM	FS		61.5	288
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_028-030CM	FS		61.5	279
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_030-032CM	FS		60	317
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_032-034CM	FS		60.3	266
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_034-036CM	FS		58.5	291
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_036-038CM	FS		58.4	329
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_038-040CM	FS		56.4	194
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_040-045CM	FS		59.6	160
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_045-050CM	FS		60.3	78.9

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	Mercury	
					Unit	% Solids	NG/G
					Fraction	PERCENT	Total
						Final Result	Final Qualifier
						Final Result	Final Qualifier
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_050-055CM	FS		54.6	73.7
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_055-060CM	FS		53.8	24.8
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_060-065CM	FS		49.5	31.3
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_065-070CM	FS		51.5	29.1
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_070-075CM	FS		49.1	32.4
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_075-080CM	FS		50.4	30.5
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_080-085CM	FS		51.8	37.7
MM-T2-C2	MM-T2-C2-A	10/24/17	MM-T2-C2-A-17_SED_085-090CM	FS		50.4	30.6
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_000-001CM	FS		55.8	705
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_001-002CM	FS		56.7	696
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_002-003CM	FS		55.1	868
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_003-004CM	FS		52.7	881
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_004-005CM	FS		54.3	1,020
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_005-006CM	FS		54.3	1,190
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_006-007CM	FS		54.2	1,320
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_007-008CM	FS		52.5	1,540
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_008-009CM	FS		53.6	1,800
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_009-010CM	FS		53.6	2,010
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_010-011CM	FS		54.6	2,390
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_011-012CM	FS		52.4	3,280
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_012-013CM	FS		50.1	3,710
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_013-014CM	FS		42.5	933
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_014-015CM	FS		42.1	379
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_015-016CM	FS		45	817

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	Mercury	
					Unit	% Solids	NG/G
					Fraction	PERCENT	Total
						Final Result	Final Qualifier
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_016-017CM	FS		57.5	5,490
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_017-018CM	FS		55.6	3,440
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_018-019CM	FS		55.1	2,670
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_019-020CM	FS		48.8	1,830
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_020-022CM	FS		41.5	705
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_022-024CM	FS		28.1	74.5
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_024-026CM	FS		25.1	54.3
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_026-028CM	FS		24	47.6
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_028-030CM	FS		26.9	32.8
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_030-032CM	FS		32.7	31
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_032-034CM	FS		34.2	36.3
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_034-036CM	FS		34.9	34.6
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_036-038CM	FS		36.2	35.5
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_038-040CM	FS		34.9	41.3
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_040-045CM	FS		38.6	33.5
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_045-050CM	FS		42.1	38.9
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_050-055CM	FS		44.6	30.9
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_055-060CM	FS		41.4	28.3
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_060-065CM	FS		56.2	67.9
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_065-070CM	FS		50.3	50.8
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_070-075CM	FS		49.1	52.7
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_075-080CM	FS		47.2	30.5
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_080-085CM	FS		49.4	32
MM-T2-C3	MM-T2-C3-A	10/10/17	MM-T2-C3-A-17_SED_085-090CM	FS		52.4	29.5

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473		
					Parameter	% Solids	Mercury	
					Unit	PERCENT	NG/G	
					Fraction	Total	Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_000-001CM	FS		60.5	602	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_001-002CM	FS		60.1	654	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_002-003CM	FS		62.8	708	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_003-004CM	FS		62.3	758	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_004-005CM	FS		61.9	751	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_005-006CM	FS		62.4	750	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_006-007CM	FS		63.9	815	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_007-008CM	FS		63	933	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_008-009CM	FS		63.7	768	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_009-010CM	FS		62.5	850	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_010-011CM	FS		61.9	848	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_011-012CM	FS		53.5	905	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_012-013CM	FS		61.5	915	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_013-014CM	FS		63.4	1,720	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_014-015CM	FS		60.4	1,390	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_015-016CM	FS		64	1,690	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_016-017CM	FS		60.5	3,450	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_017-018CM	FS		63.4	2,800	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_018-019CM	FS		64.7	2,580	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_019-020CM	FS		64.9	4,540	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_020-022CM	FS		61	5,000	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_022-024CM	FS		67	3,460	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_024-026CM	FS		66.6	2,710	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_026-028CM	FS		70.6	3,130	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473		
					Parameter	Mercury		
					Unit	NG/G		
					Fraction	Total		
					Final Result	Final Qualifier	Final Result	Final Qualifier
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_028-030CM	FS	65.7		2,700	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_030-032CM	FS	62.7		2,390	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_032-034CM	FS	65.8		932	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_034-036CM	FS	64.5		637	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_036-038CM	FS	64.1		489	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_038-040CM	FS	61.9		375	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_040-045CM	FS	59.9		330	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_045-050CM	FS	57.2		292	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_050-055CM	FS	58.2		264	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_055-060CM	FS	59.2		231	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_060-065CM	FS	54.6		204	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_065-070CM	FS	57.7		174	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_070-075CM	FS	57.9		117	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_075-080CM	FS	56.6		95.2	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_080-085CM	FS	53.9		89.4	
MM-T3-C5	MM-T3-C5-C	10/03/17	MM-T3-C5-C-17_SED_085-090CM	FS	52.9		76.8	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_000-001CM	FS	51.1		674	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_001-002CM	FS	50.9		713	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_002-003CM	FS	50.8		836	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_003-004CM	FS	50.8		687	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_004-005CM	FS	49.2		685	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_005-006CM	FS	49.9		650	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_006-007CM	FS	45.5		757	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_007-008CM	FS	48.1		698	

TABLE 3
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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	Mercury	
					Unit	% Solids	NG/G
					Fraction	PERCENT	Total
						Final Result	Final Qualifier
						Final Result	Final Qualifier
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_008-009CM	FS		47.7	618
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_009-010CM	FS		48.1	782
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_010-011CM	FS		50.1	695
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_011-012CM	FS		52.1	770
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_012-013CM	FS		49.4	1,010
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_013-014CM	FS		49.2	1,210
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_014-015CM	FS		49.1	1,170
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_015-016CM	FS		50	893
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_016-017CM	FS		49.1	893
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_017-018CM	FS		44.6	785
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_018-019CM	FS		40.2	756
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_019-020CM	FS		45.2	808
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_020-022CM	FS		49.5	890
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_022-024CM	FS		47.9	931
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_024-026CM	FS		48.5	1,040
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_026-028CM	FS		52.4	1,130
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_028-030CM	FS		48.4	1,120
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_030-032CM	FS		52.1	1,180
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_032-034CM	FS		51	1,230
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_034-036CM	FS		51.5	1,300
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_036-038CM	FS		51.2	1,230
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_038-040CM	FS		49.8	1,610
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_040-045CM	FS		52.9	1,330
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_045-050CM	FS		53.5	1,390

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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473			
					Parameter	Mercury			
					Unit	NG/G			
					Fraction	Total			
					Final Result	Final Qualifier	Final Result	Final Qualifier	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_050-055CM	FS		52.4		1,460	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_055-060CM	FS		52.7		1,430	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_060-065CM	FS		52.9		1,400	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_065-070CM	FS		53.4		1,410	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_070-075CM	FS		55.7		1,510	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_075-080CM	FS		57.6		1,750	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_080-085CM	FS		55.4		1,490	
MM-T4-C3	MM-T4-C3-C	10/28/17	MM-T4-C3-C-17_SED_085-090CM	FS		54.9		1,500	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_000-001CM	FS		65.2		278	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_001-002CM	FS		64.1		297	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_002-003CM	FS		65.6		358	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_003-004CM	FS		70.1		483	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_004-005CM	FS		72.6		485	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_005-006CM	FS		69.9		534	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_006-007CM	FS		69.3		733	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_007-008CM	FS		70		919	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_008-009CM	FS		64.1		922	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_009-010CM	FS		66.2		946	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_010-011CM	FS		67.7		1,280	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_011-012CM	FS		73		2,330	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_012-013CM	FS		72.8		1,610	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_013-014CM	FS		72.3		1,300	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_014-015CM	FS		70.7		800	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_015-016CM	FS		72.1		698	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473			
					Parameter	Mercury			
					Unit	NG/G			
					Fraction	Total			
					Final Result	Final Qualifier	Final Result	Final Qualifier	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_016-017CM	FS		72.9		454	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_017-018CM	FS		73.7		391	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_018-019CM	FS		76		517	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_019-020CM	FS		74.9		522	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_020-022CM	FS		73.4		233	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_022-024CM	FS		68.2		180	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_024-026CM	FS		60.6		121	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_026-028CM	FS		68.6		128	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_028-030CM	FS		64.4		92.9	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_030-032CM	FS		62.8		81.7	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_032-034CM	FS		64.2		78.7	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_034-036CM	FS		60.4		72.6	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_036-038CM	FS		56.3		43.7	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_038-040CM	FS		50.7		32.2	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_040-045CM	FS		55.8		26.2	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_045-050CM	FS		57		21.8	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_050-055CM	FS		60.4		29.3	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_055-060CM	FS		58.1		31.1	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_060-065CM	FS		51.1		15.8	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_065-070CM	FS		57.7		17.2	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_070-075CM	FS		48.8		30.9	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_075-080CM	FS		49.7		31.4	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_080-085CM	FS		45.6		26.7	
MM-T4-C4	MM-T4-C4-A	10/24/17	MM-T4-C4-A-17_SED_085-090CM	FS		49.9		29.1	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	% Solids	Mercury
					Unit	PERCENT	NG/G
					Fraction	Total	Total
						Final Result	Final Qualifier
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_000-001CM	FS		56.3	863
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_001-002CM	FS		55.2	766
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_002-003CM	FS		53.3	780
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_003-004CM	FS		53.2	688
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_004-005CM	FS		54.2	796
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_005-006CM	FS		53.3	767
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_006-007CM	FS		52.6	780
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_007-008CM	FS		53.6	700
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_008-009CM	FS		54.3	759
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_009-010CM	FS		52.7	788
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_010-011CM	FS		50.7	766
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_011-012CM	FS		50.4	880
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_012-013CM	FS		51.9	867
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_013-014CM	FS		51.9	897
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_014-015CM	FS		51.3	888
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_015-016CM	FS		53.4	1,080
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_016-017CM	FS		55	1,190
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_017-018CM	FS		54	1,270
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_018-019CM	FS		55	1,300
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_019-020CM	FS		55.2	1,240
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_020-022CM	FS		55.9	1,440
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_022-024CM	FS		58.9	1,690
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_024-026CM	FS		57.7	1,600
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_026-028CM	FS		51.4	1,310

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	Mercury	
					Unit	% Solids	NG/G
					Fraction	PERCENT	Total
						Final Result	Final Qualifier
						Final Result	Final Qualifier
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_028-030CM	FS		54.9	1,560
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_030-032CM	FS		57.7	1,780
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_032-034CM	FS		54.4	1,800
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_034-036CM	FS		58.3	2,140
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_036-038CM	FS		61.6	2,310
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_038-040CM	FS		63	2,950
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_040-045CM	FS		65.9	2,580
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_045-050CM	FS		67.3	940
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_050-055CM	FS		51.9	203
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_055-060CM	FS		41.3	85.8
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_060-065CM	FS		38.8	22.7
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_065-070CM	FS		38.9	20.6
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_070-075CM	FS		37.8	23.3
OR-C1	OR-C1-A	10/12/17	OR-C1-A-17_SED_075-079CM	FS		37.2	23.2
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_000-001CM	FS		56.8	951
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_001-002CM	FS		57.5	774
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_002-003CM	FS		57.5	733
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_003-004CM	FS		56.8	688
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_004-005CM	FS		57.9	718
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_005-006CM	FS		57.2	694
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_006-007CM	FS		57.9	708
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_007-008CM	FS		58.1	741
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_008-009CM	FS		57.8	809
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_009-010CM	FS		58.5	915

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473		
					Parameter Unit Fraction	% Solids PERCENT Total	Mercury NG/G Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_010-011CM	FS			927	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_011-012CM	FS			830	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_012-013CM	FS			840	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_013-014CM	FS			823	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_014-015CM	FS			896	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_015-016CM	FS			877	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_016-017CM	FS			904	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_017-018CM	FS			990	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_018-019CM	FS			997	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_019-020CM	FS			1,110	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_020-022CM	FS			1,300	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_022-024CM	FS			1,380	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_024-026CM	FS			1,450	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_026-028CM	FS			1,500	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_028-030CM	FS			1,880	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_030-032CM	FS			1,810	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_032-034CM	FS			2,100	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_034-036CM	FS			2,280	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_036-038CM	FS			2,770	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_038-040CM	FS			2,800	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_040-045CM	FS			3,860	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_045-050CM	FS			4,300	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_050-055CM	FS			2,880	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_055-060CM	FS			1,730	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473		
					Parameter Unit Fraction	% Solids PERCENT Total	Mercury NG/G Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_060-065CM	FS			458	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_065-070CM	FS			364	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_070-075CM	FS			24.7	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_075-080CM	FS			23.4	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_080-085CM	FS			20.3	
OR-T1-C1	OR-T1-C1-B	10/28/17	OR-T1-C1-B-17_SED_085-090CM	FS			19.4	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_000-001CM	FS			924	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_001-002CM	FS			1,210	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_002-003CM	FS			977	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_003-004CM	FS			852	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_004-005CM	FS			1,030	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_005-006CM	FS			1,010	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_006-007CM	FS			815	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_007-008CM	FS			926	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_008-009CM	FS			1,130	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_009-010CM	FS			997	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_010-011CM	FS			1,060	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_011-012CM	FS			988	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_012-013CM	FS			1,290	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_013-014CM	FS			1,220	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_014-015CM	FS			1,110	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_015-016CM	FS			1,000	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_016-017CM	FS			995	
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_017-018CM	FS			1,020	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	Mercury	
					Unit	% Solids	NG/G
					Fraction	PERCENT	Total
						Final Result	Final Qualifier
						Final Result	Final Qualifier
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_018-019CM	FS		54.3	1,050
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_019-020CM	FS		60.3	1,340
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_020-022CM	FS		56.5	1,080
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_022-024CM	FS		54.1	1,010
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_024-026CM	FS		55.1	1,170
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_026-028CM	FS		56.8	1,260
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_028-030CM	FS		53.6	1,380
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_030-032CM	FS		51.8	1,550
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_032-034CM	FS		55	2,090
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_034-036CM	FS		58.3	2,730
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_036-038CM	FS		59.3	3,230
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_038-040CM	FS		59.8	3,410
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_040-045CM	FS		61.4	3,250
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_045-050CM	FS		71.1	1,830
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_050-055CM	FS		57.8	1,020
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_055-060CM	FS		58.7	333
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_060-065CM	FS		59.9	570
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_065-070CM	FS		55	241
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_070-075CM	FS		56.3	205
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_075-080CM	FS		52.9	198
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_080-085CM	FS		42.3	87.9
OR-T2-C2	OR-T2-C2-D	10/20/17	OR-T2-C2-D-17_SED_085-090CM	FS		27.5	20.8
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_000-001CM	FS		13.5	2.39
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_001-002CM	FS		12.1	1.94

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473		
					Parameter Unit Fraction	% Solids PERCENT Total	Mercury NG/G Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_002-003CM	FS			1.49	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_003-004CM	FS			1.4	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_004-005CM	FS			2.12	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_005-006CM	FS			1.85	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_006-007CM	FS			1.81	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_007-008CM	FS			2.14	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_008-009CM	FS			1.65	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_009-010CM	FS			2.04	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_010-011CM	FS			1.73	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_011-012CM	FS			1.9	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_012-013CM	FS			1.75	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_013-014CM	FS			2.17	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_014-015CM	FS			2.26	J
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_015-016CM	FS			1.8	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_016-017CM	FS			2.02	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_017-018CM	FS			2.41	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_018-019CM	FS			3.2	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_019-020CM	FS			2.3	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_020-022CM	FS			3.23	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_022-024CM	FS			2.09	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_024-026CM	FS			2.51	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_026-028CM	FS			2.38	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_028-030CM	FS			2.28	
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_030-032CM	FS			2.55	

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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	Mercury	
					Unit	% Solids	NG/G
					Fraction	PERCENT	Total
						Final Result	Final Qualifier
						Final Result	Final Qualifier
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_032-034CM	FS		11.5	2.07
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_034-036CM	FS		11.1	2.24
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_036-038CM	FS		11	4.31
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_038-040CM	FS		10.8	3.05
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_040-045CM	FS		10.3	2.23
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_045-050CM	FS		5.9	3.38
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_050-055CM	FS		10.3	2.3
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_055-060CM	FS		12.3	1.71
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_060-065CM	FS		14.2	2.32
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_065-070CM	FS		12.6	2.48
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_070-075CM	FS		11.8	2.86
PBR-04	PBR-04-C	09/08/17	PBR-04-C-17_SED_075-080CM	FS		9.5	3.62
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_000-001CM	FS		63.8	983
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_001-002CM	FS		59.2	740
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_002-003CM	FS		56.1	840
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_003-004CM	FS		58.6	945
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_004-005CM	FS		55.5	939
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_005-006CM	FS		53.1	860
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_006-007CM	FS		52.5	844
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_007-008CM	FS		52.4	759
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_008-009CM	FS		52.5	941
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_009-010CM	FS		55.8	1,170
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_010-011CM	FS		54.2	996
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_011-012CM	FS		56.5	1,170

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Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	Mercury	
					Unit	% Solids	NG/G
					Fraction	PERCENT	Total
						Final Result	Final Qualifier
						Final Result	Final Qualifier
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_012-013CM	FS		57.1	1,260
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_013-014CM	FS		55.5	1,170
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_014-015CM	FS		53.7	1,140
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_015-016CM	FS		51.5	1,070
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_016-017CM	FS		53.2	1,130
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_017-018CM	FS		48.1	1,020
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_018-019CM	FS		52.6	1,260
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_019-020CM	FS		54.5	1,310
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_020-022CM	FS		60.1	2,040
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_022-024CM	FS		59.4	2,060
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_024-026CM	FS		56.5	1,680
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_026-028CM	FS		55.5	1,520
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_028-030CM	FS		58.5	2,040
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_030-032CM	FS		65.6	3,270
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_032-034CM	FS		58.4	2,110
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_034-036CM	FS		49.3	1,150
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_036-038CM	FS		51.6	1,730
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_038-040CM	FS		34	728
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_040-045CM	FS		40.3	699
PBR-10	PBR-10-A	09/06/17	PBR-10-A-17_SED_045-050CM	FS		101.7	1,202
PBR-10	PBR-16-C	11/28/17	PBR-16-C-17_SED_000-001CM	FS		39.73289	1,070
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_001-002CM	FS		32.8619	688
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_002-003CM	FS		34.03185	1,340
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_003-004CM	FS		56.91667	8,390

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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473	
					Parameter	Mercury	
					Unit	NG/G	
					Fraction	Total	
						% Solids	
						PERCENT	
						Total	Total
						Final Result	Final Qualifier
						Final Result	Final Qualifier
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_004-005CM	FS		60.11645	11,100
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_005-006CM	FS		64.78599	25,200
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_006-007CM	FS		63.72022	100,200
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_007-008CM	FS		64.32906	66,000
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_008-009CM	FS		57.6324	22,600
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_009-010CM	FS		63.11239	7,580
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_010-011CM	FS		62.73991	4,120
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_011-012CM	FS		63.96181	2,690
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_012-013CM	FS		60.29823	1,340
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_013-014CM	FS		62.68861	905
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_014-015CM	FS		63	658
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_015-016CM	FS		63.8	598
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_016-017CM	FS		60.4	563
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_017-018CM	FS		57.2	503
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_018-019CM	FS		51.5	424
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_019-020CM	FS		47	367
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_020-022CM	FS		41.2	345
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_022-024CM	FS		52.1	279
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_024-026CM	FS		52.9	265
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_026-028CM	FS		47.2	373
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_028-030CM	FS		44.2	108
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_030-032CM	FS		43.1	89.9
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_032-034CM	FS		37.5	61.3
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_034-036CM	FS		42.6	71.8

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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473		
					Parameter Unit Fraction	% Solids PERCENT Total	Mercury NG/G Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_036-038CM	FS			78.8	
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_038-040CM	FS			63.7	
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_040-045CM	FS			59.8	
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_045-050CM	FS			40.3	
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_050-055CM	FS			17.4	
PBR-16	PBR-16-C	11/28/17	PBR-16-C-17_SED_055-057CM	FS			10.3	
PBR-16	PBR-19-A	08/17/17	PBR-19-A-17_SED_000-001CM	FS			1,164	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_001-002CM	FS			1,210	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_002-003CM	FS			1,148	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_003-004CM	FS			1,442	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_004-005CM	FS			993	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_005-006CM	FS			1,325	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_006-007CM	FS			1,961	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_007-008CM	FS			1,582	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_008-009CM	FS			1,732	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_009-010CM	FS			1,959	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_010-011CM	FS			1,631	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_011-012CM	FS			1,956	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_012-013CM	FS			1,916	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_013-014CM	FS			1,847	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_014-015CM	FS			2,189	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_015-016CM	FS			2,131	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_016-017CM	FS			2,437	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_017-018CM	FS			2,682	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473		
					Parameter	Mercury		
					Unit	NG/G		
					Fraction	Total		
					Final Result	Final Qualifier	Final Result	Final Qualifier
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_018-019CM	FS		67.6	2,533	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_019-020CM	FS		67.9	2,522	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_020-022CM	FS		67.3	2,310	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_022-024CM	FS		67.1	2,040	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_024-026CM	FS		68.9	1,920	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_026-028CM	FS		70	2,170	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_028-030CM	FS		62.5	1,790	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_030-032CM	FS		54.8	1,300	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_032-034CM	FS		42.1	366	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_034-036CM	FS		40.1	144	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_036-038CM	FS		36.5	46.5	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_038-040CM	FS		39.5	130	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_040-045CM	FS		41.9	176	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_045-050CM	FS		40.2	69.8	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_050-055CM	FS		41	101	
PBR-19	PBR-19-A	08/17/17	PBR-19-A-17_SED_055-059CM	FS		39.3	74.3	
PBR-19	PBR-28-C	10/03/17	PBR-28-C-17_SED_000-001CM	FS		50.6	713	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_001-002CM	FS		49.4	681	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_002-003CM	FS		49.4	725	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_003-004CM	FS		49.4	728	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_004-005CM	FS		48.9	759	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_005-006CM	FS		52.9	891	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_006-007CM	FS		55.5	836	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_007-008CM	FS		51.3	806	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473		
					Parameter Unit Fraction	% Solids PERCENT Total	Mercury NG/G Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_008-009CM	FS			812	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_009-010CM	FS			808	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_010-011CM	FS			777	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_011-012CM	FS			796	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_012-013CM	FS			810	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_013-014CM	FS			822	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_014-015CM	FS			790	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_015-016CM	FS			750	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_016-017CM	FS			495	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_017-018CM	FS			272	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_018-019CM	FS			333	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_019-020CM	FS			497	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_020-022CM	FS			402	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_022-024CM	FS			170	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_024-026CM	FS			125	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_026-028CM	FS			55.5	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_028-030CM	FS			21.3	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_030-032CM	FS			24.5	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_032-034CM	FS			21.3	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_034-036CM	FS			21.7	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_036-038CM	FS			23	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_038-040CM	FS			18.3	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_040-045CM	FS			17.8	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_045-050CM	FS			23.4	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL CORE SEDIMENT SAMPLING - FLETT
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

Cores ES-17, ES-20, MM-C2, MM-C3, MM-T2-C2, MM-T2-C3, MM-T3-C5, MM-T4-C3, MM-T4-C4, OR-C1, OR-T1-C1, OR-T2-C2, PBR-04, PBR-10, PBR-16, PBR-19, and PBR-28

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	EPA 7473			
					Parameter	Mercury			
					Unit	NG/G			
					Fraction	Total			
					Final Result	Final Qualifier	Final Result	Final Qualifier	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_050-055CM	FS		32.2		18.5	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_055-060CM	FS		32.4		20.4	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_060-065CM	FS		30		17.7	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_065-070CM	FS		33.5		21.4	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_070-075CM	FS		32.6		22.6	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_075-080CM	FS		34.6		20.6	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_080-085CM	FS		34.1		19.5	
PBR-28	PBR-28-C	10/03/17	PBR-28-C-17_SED_085-090CM	FS		34.2		19	

Notes:

% = Percent
 NG/G = Nanogram per gram
 FD = Field Duplicate
 FS = Field Sample
 SDG = Sample Delivery Group
 TOC = Total Organic Carbon

Qualifiers:

J = Value is estimated

**Data Validation Summary
 2017 Geochronology Interval Cores – Report 3
 Penobscot River Estuary Phase III – Engineering Evaluation
 Penobscot River, Maine**

1.0 INTRODUCTION

Sediment samples were collected in September, October and November 2017 from the Penobscot River located in Maine. Samples were analyzed by Eurofins Frontier Global Sciences, Inc. (Eurofins) located in Bothell, Washington and included in sample delivery groups (SDGs) 1709432, 1709552, 1709555, 1709558, 1709562, 1709563, 1709564, 1709565, 1709566, 1709567, 1709568, 1709569, 1709570, 1709571, 1709572, 1709574, 1710289, 1710294, 1710307, 1710310, 1710313, 1710315, 1710633, 1710634, 1710637, 1710639, 1710641, 1710682, 1710684, 1710685, 1710728, 1710729, 1710730, 1710731, 1710732, 1710733, 1710907, 1710910, 1710913, 1710916, 1710917, 1710918, 1711046, 1711047, 1711050, 1711056, 1711057, 1711058, 1711059, 1711060, 1711061, 1711062, 1711063, 1711064, 1711065, 1711066, 1711067, 1711068, 1711069, 1711070, 1711071, 1711073, 1711077, 1711083, 1711084, 1711085, 1711151, 1711156, 1711171, 1711173, 1711174, 1711328, 1712044, 1712045, and 1712047. Samples were also analyzed by Alpha Analytical located in Mansfield, Massachusetts and are reported in SDGs L1732774, L1733612, L1733618, L1733619, L1733620, L1733621, L1736451, L1736453, L1736454, L1736455, L1736456, L1736458, L1737040, L1737041, L1737042, L1737043, L1737044, L1737045, L1737046, L1737047, L1738093, L1738103, L1738104, L1738105, L1738106, L1738128, L1739120, L1739121, L1739122, L1739123, L1739124, L1739127, L1739536, L1739537, L1739540, L1739541, L1739542, L1739572, L1739573, L1739577, L1739578, L1739579, L1739580, L1739581, L1739593, L1739594, L1739595, L1739596, L1739597, L1739598, L1739599, L1739601, L1739602, L1739653, L1739656, L1739691, L1740283, L1740284, L1740285, L1740287, L1740289 and L1741133. Samples were analyzed by one or more of the following: Clean Water Act (CWA, 2012) or Standard Methods for the Examination of Water and Wastewater (SM, 2014):

Laboratory	Parameter	Analytical Method	Validation Level
Eurofins	Mercury, total	CWA1631B (Hot aqua regia digestion)	10% Stage III/ 90% Stage IIB
Alpha	TOC	Lloyd Kahn	10% Stage III/ 90% Stage IIB
Eurofins/ Alpha	% Solids	SM2540	10% Stage III/ 90% Stage IIB

A Stage IIB data validation was completed on all SDGs. A Stage III data validation was performed on ten percent of samples. Data validation was completed using National Functional Guidelines for Inorganic Superfund Data Review (USEPA, 2014) and EPA New England Environmental Data Review Supplement for Regional Data Review Elements and Superfund Specific Guidance/Procedures (USEPA, 2013) where applicable. Data quality evaluations were completed using quality control (QC) limits specified in the draft Penobscot River Estuary Phase III Engineering Evaluation Quality Assurance Project Plan (QAPP) [Amec Foster Wheeler, 2016]. The project laboratory reported results using a combination of two detection limits including the reporting limit (RL) and the method detection limit (MDL). Results for compounds that are not detected in samples are reported as U qualified results at the RL. Positive detections between the MDL and RL are qualified as estimated (J) by the laboratory.

Data validation review and qualification actions are discussed in the following subsections. It should be noted that only instances that result in an impact to data quality are presented in this report. There may be QC elements outside of QAPP and/or method control limits not presented in this report since there is no impact to data quality. Samples included in this data evaluation are presented in Table 1.

Data qualifications were completed if necessary in accordance with the guidelines or the professional judgment of the project chemist. The following qualifiers as applied during data validation or reported by the laboratory are included in the final data set:

J = The reported concentration is considered an estimated value
U = The target compound was not detected above the method detection limit

Validation reason codes were applied to results associated with QC measurements outside project QC goals. The validation qualification actions and associated validation reason codes applied to sample results are summarized on Table 2. The following data validation reason codes were applied to one or more sample results:

HT = Holding time exceeded
LD = Lab Duplicate limit exceeded
MS-H = MS and/or MSD recovery high
MS-L = MS and/or MSD recovery low
MS-RPD = MS/MSD Relative Percent Difference (RPD) limit exceeded
FD = Field duplicate RPD limit exceeded
LCS-RPD = LCS/LCSD RPD limit exceeded

A complete summary of final sample results is provided in Table 3.

Data were evaluated based on the following parameters:

- * Data Completeness and Chain of Custody
Holding Times and Preservation
 - * Blanks
 - * Initial Calibration
 - * Continuing Calibration
Laboratory Control Sample (LCS)
Matrix Spike/Matrix Spike Duplicates (MS/MSD)
Laboratory Duplicates
Field Duplicates
 - * Detection Limits
 - * Sample Result Verification/Electronic Evaluation Verification (EDD)
 - * Ongoing Precision Recovery
- * = indicates that criteria were met and/or no impact to data quality for this parameter

With the exception of the following items discussed below, results were determined to be usable as reported by the laboratory.

2.0 Mercury – 1631

Laboratory Control Sample

SDG 1710637 – The LCS (F710506-BS1)/LCSD (F710506-BSD1) RPD (25%) associated with samples MM-T1-C1-A-17_SED_000-001CM, MM-T1-C1-A-17_SED_001-002CM, MM-T1-C1-A-17_SED_002-003CM, MM-T1-C1-A-17_SED_003-004CM, MM-T1-C1-A-17_SED_004-005CM, MM-T1-C1-A-17_SED_005-006CM, MM-T1-C1-A-17_SED_006-007CM, MM-T1-C1-A-17_SED_007-008CM, MM-T1-

C1-A-17_SED_008-009CM, MM-T1-C1-A-17_SED_009-010CM and MM-T1-C1-A-17_SED_010-011CM was above the QC limit of 24%. The mercury results for the above listed samples were qualified as estimated (J) due to the imprecision.

Matrix Spike

SDG 1710307 – Samples OR-T1-C5-A-17_SED_008-009CM, OR-T1-C5-A-17_SED_015-016CM, OR-T1-C5-A-17_SED_034-036CM and OR-T1-C5-A-17_SED_060-065CM were used for MS/MSD analysis. The MSD recoveries of mercury in sample OR-T1-C5-A-17_SED_060-065CM (0.5%) and the reanalysis (0.27%) were below the lower QC limit of 71%. The MS/MSD RPDs for sample OR-T1-C5-A-17_SED_060-065CM (198%) and the reanalysis (199%) were above the QC limit of 24%. The laboratory indicated that the MSD may not have been spiked. The laboratory re-prep and re-analyzed samples to ensure a project sample was not accidentally spiked. Results confirmed and original data reported. Based on professional judgment, the mercury result for sample OR-T1-C5-A-17_SED_060-065CM was qualified as estimated (J) due to the potential low bias and imprecision.

SDG 1710730 – Sample MM-T4-C6-17_SED_017-018CM was used for MS/MSD analysis. The MS recovery of mercury in sample MM-T4-C6-17_SED_017-018CM (70.8%) was below the lower QC limit of 71%. Based on professional judgment, the mercury result for sample MM-T4-C6-17_SED_017-018CM was qualified as estimated (J) due to the potential low bias.

SDG 1710916 – Sample MM-T5-C3-17_SED_006-007CM was used for MS/MSD analysis. The MS recovery of mercury in sample MM-T5-C3-17_SED_006-007CM (66%) was below the lower QC limit of 71%. Based on professional judgment, the mercury result for sample MM-T5-C3-17_SED_006-007CM was qualified as estimated (J) due to the potential low bias.

SDG 1711174 – Sample MM-T3-C1-17_SED_015-016CM_DUP was used for MS/MSD analysis. The MS recovery for mercury in sample MM-T3-C1-17_SED_015-016CM_DUP (70.5%) was below the lower QC limit of 71%. The mercury results for samples MM-T3-C1-17_SED_015-016CM_DUP and MM-T3-C1-17_SED_015-016CM were qualified as estimated (J) due to the potential low bias.

Field Duplicate

SDG 1710682 – Sample MM-T1-C4-17_SED_045-050CM_DUP was submitted as field duplicate of sample MM-T1-C4-17_SED_045-050CM. The RPD (74%) was above the QC limit of 50%. The mercury results for samples MM-T1-C4-17_SED_045-050CM and MM-T1-C4-17_SED_045-050CM_DUP were qualified as estimated (J) due to the imprecision.

SDG 1710685 – Sample OR-T1-C3-A-17_SED_018-019CM_DUP was submitted as field duplicate of sample OR-T1-C3-A-17_SED_018-019CM. The RPD (65%) was above the QC limit of 50%. The mercury results for samples OR-T1-C3-A-17_SED_018-019CM and OR-T1-C3-A-17_SED_018-019CM_DUP were qualified as estimated (J) due to the imprecision.

SDG 1711050 – Sample VE-MU4-GC-1-F-17_SED_03-05_DUP was submitted as field duplicate of sample VE-MU4-GC-1-F-17_SED_03-05. The RPD (94%) was above the QC limit of 50%. The mercury results for samples VE-MU4-GC-1-F-17_SED_03-05 and VE-MU4-GC-1-F-17_SED_03-05_DUP were qualified as estimated (J) due to the imprecision.

3.0 TOC- Lloyd Kahn

Holding Times and Preservation

SDGs L1737045, L1737046, L1737047, L1738093, L1738103, L1738104, L1738105 – All samples were analyzed with the method required holding time exceeded. All TOC results have been qualified as estimated (J) due to the hold time exceedance.

Laboratory Duplicate/ Replicate

SDG L1732774 – Sample burn replicate RPDs for samples MM-T3-C2-C-17_SED_026-028CM (45%), MM-T3-C2-C-17_SED_034-036CM (46%), MM-T3-C2-C-17_SED_045-050CM (48%), and MM-T3-C2-C-17_SED_055-060CM (63%) exceeded the QC limit of 30%. All TOC results for samples MM-T3-C2-C-17_SED_026-028CM, MM-T3-C2-C-17_SED_034-036CM, MM-T3-C2-C-17_SED_045-050CM and MM-T3-C2-C-17_SED_055-060CM were qualified as estimated (UJ/J) due to imprecision.

SDG L1733612 – Sample burn replicate RPDs for samples OR-T1-C4-C-17_SED_019-020CM (32%) and OR-T1-C4-C-17_SED_032-034CM (39%) exceeded the QC limit of 30%. All TOC results for samples OR-T1-C4-C-17_SED_019-020CM and OR-T1-C4-C-17_SED_032-034CM were qualified as estimated (J) due to imprecision.

SDG L1733618 – Sample MM-T1-C3-B-17_SED_022-024CM was selected by the laboratory for duplicate analysis. The RPD of sample MM-T1-C3-B-17_SED_022-024CM TOC Rep 1 (86%) was above the QC limit of 25%. The Rep 1 and average TOCs result for sample MM-T1-C3-B-17_SED_022-024CM were qualified as estimated (J) due to the imprecision.

SDG L1733618 – Sample burn replicate RPDs for samples MM-T1-C3-B-17_SED_012-013CM (71%), MM-T1-C3-B-17_SED_014-015CM (41%), MM-T1-C3-B-17_SED_019-020CM (34%), MM-T1-C3-B-17_SED_022-024CM (43%), MM-T1-C3-B-17_SED_034-036CM (32%), MM-T1-C3-B-17_SED_060-065CM (48%), and MM-T1-C3-B-17_SED_070-075CM (47%) exceeded the QC limit of 30%. All TOC results for samples MM-T1-C3-B-17_SED_012-013CM, MM-T1-C3-B-17_SED_014-015CM, MM-T1-C3-B-17_SED_019-020CM, MM-T1-C3-B-17_SED_022-024CM, MM-T1-C3-B-17_SED_034-036CM, MM-T1-C3-B-17_SED_060-065CM and MM-T1-C3-B-17_SED_070-075CM were qualified as estimated (J) due to imprecision.

SDG L1733619 – Sample burn replicate RPDs for samples MM-T2-C4-B-17_SED_022-024CM (76%) and MM-T2-C4-B-17_SED_065-070CM (48%) exceeded the QC limit of 30%. All TOC results for samples MM-T2-C4-B-17_SED_022-024CM and MM-T2-C4-B-17_SED_065-070CM were qualified as estimated (J) due to imprecision.

SDG L1733620 – Sample burn replicate RPDs for samples MM-T2-C5-A-17_SED_008-009CM (31%) and MM-T2-C5-A-17_SED_013-014CM (69%) exceeded the QC limit of 30%. All TOC results for samples MM-T2-C5-A-17_SED_008-009CM and MM-T2-C5-A-17_SED_013-014CM were qualified as estimated (J) due to imprecision.

SDG L1736454 – Sample burn replicate RPDs for samples OR-T1-C5-A-17_SED_001-002CM (38%) and OR-T1-C5-A-17_SED_075-080CM (51%) exceeded the QC limit of 30%. All TOC results for samples OR-T1-C5-A-17_SED_001-002CM and OR-T1-C5-A-17_SED_075-080CM were qualified as estimated (J) due to imprecision.

SDG L1736455 – Sample burn replicate RPD for sample OR-T2-C1-C-17_SED_018-019CM (41%) exceeds the QC limit of 30%. All TOC results for sample OR-T2-C1-C-17_SED_018-019CM were qualified as estimated (J) due to imprecision.

SDG L1737045 – All samples were selected for duplicate analysis. The RPD of samples MM-T3-C3-B2-17_SED_010-011CM Rep 2 (38%), MM-T3-C3-B2-17_SED_018-019CM Rep 1 (33%), MM-T3-C3-B2-17_SED_040-045CM Rep 2 (36%), and MM-T3-C3-B2-17_SED_075-080CM Rep 2 (27%) were above the QC limit of 25%. Samples MM-T3-C3-B2-17_SED_010-011CM Rep 2, MM-T3-C3-B2-17_SED_018-019CM Rep 1, MM-T3-C3-B2-17_SED_040-045CM Rep 2, and MM-T3-C3-B2-17_SED_075-080CM Rep 2 and the associated average TOC results were qualified as estimated (J) due to the imprecision.

SDG 1737046 – Almost all samples were selected for duplicate analysis. The RPD of sample OR-T1-C3-A-17_SED_060-065CM TOC Rep 2 (39%) was above the QC limit of 25%. The Rep 2 and average TOC results for sample OR-T1-C3-A-17_SED_060-065CM were qualified as estimated (J) due to the imprecision.

The RPD of sample OR-T1-C3-A-17_SED_030-032CM TOC Rep 1 (26%) and Rep 2 (28%) were above the QC limit of 25%. All TOC results for sample OR-T1-C3-A-17_SED_030-032CM were qualified as estimated (J) due to imprecision.

SDG L1739122 – Almost all samples were selected for duplicate analysis. The RPD of sample MM-T4-C7-17_SED_024-026CM TOC Rep 2 (31%) was above the QC limit of 25%. The Rep 2 and average TOC results for sample MM-T4-C7-17_SED_024-026CM were qualified as estimated (J) due to the imprecision.

The RPD of sample MM-T4-C7-17_SED_030-032CM TOC Rep 2 (35%) were above the QC limit of 25%. The Rep 2 and average TOC results for sample MM-T4-C7-17_SED_030-032CM were qualified as estimated (J) due to imprecision.

SDG L1739537 – Sample burn replicate RPD for sample ES-18-F-17_SED_03-05 (35%) exceeds the QC limit of 30%. All TOC results for sample ES-18-F-17_SED_03-05 were qualified as estimated (J) due to imprecision.

SDG L1739656 – Sample VE-MU4-GC-1-F-17_SED_03-05 was selected for duplicate analysis. The RPDs of sample VE-MU4-GC-1-F-17_SED_03-05 Rep 1 (45%) and Rep 2 (28%) were above the QC limit of 25%. All TOC results for sample VE-MU4-GC-1-F-17_SED_03-05 were qualified as estimated (J) due to the imprecision.

SDG L1740285 – Sample burn replicate RPD for samples MM-T3-C1-17_SED_007-008CM (37%) and MM-T3-C1-17_SED_017-018CM (31%) exceeds the QC limit of 30%. All TOC results for samples MM-T3-C1-17_SED_007-008CM and MM-T3-C1-17_SED_017-018CM were qualified as estimated (J) due to imprecision.

SDG L1740285 – Almost all samples were selected for duplicate analysis. The RPDs of samples MM-T3-C1-17_SED_007-008CM, MM-T3-C1-17_SED_010-011CM, MM-T3-C1-17_SED_012-013CM, MM-T3-C1-17_SED_014-015CM, MM-T3-C1-17_SED_016-017CM, MM-T3-C1-17_SED_017-018CM, MM-T3-C1-17_SED_022-024CM were elevated however the sample results were <5X the reporting limit so the RPD does not apply, Based on professional judgement the TOC results for these samples do not require qualification.

SDG L1741133 – Sample burn replicate RPD for sample MM-T1-C1-B-17_SED_05-07 (73%) exceeds the QC limit of 30%. All TOC results for sample MM-T1-C1-B-17_SED_05-07 were qualified as estimated (J) due to imprecision.

Matrix Spike

SDG L1732774 – Sample MM-T3-C2-C-17_SED_012-013CM was used for MS analysis. The MS recoveries for TOC Rep 1 (53%) and TOC Rep 2 (0%) were below the lower QC limit of 75%. The MS recoveries do not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample MM-T3-C2-C-17_SED_012-013CM do not require qualification.

SDG L1733612 – Sample OR-T1-C4-C-17_SED_008-009CM was used for MS analysis. The MS recovery for TOC Rep 2 (143%) was above the upper QC limit of 125%. The MS recovery does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample OR-T1-C4-C-17_SED_008-009CM do not require qualification.

SDG L1733619 – Sample MM-T2-C4-B-17_SED_007-008CM was used for MS analysis. The MS recoveries for TOC Rep 1 (325%) and Rep 2 (214%) were above the upper QC limit of 125%. Based on professional judgment, all TOC results for sample MM-T2-C4-B-17_SED_007-008CM were qualified as estimated (J) due to the potential high bias.

SDG L1733620 – Sample MM-T2-C5-A-17_SED_000-001CM and MM-T2-C5-A-17_SED_036-038CM were used for MS analysis. For sample MM-T2-C5-A-17_SED_000-001CM, the MS recovery for TOC Rep 1 (0%) was below the lower QC limit of 75% and Rep 2 (221%) was above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample MM-T2-C5-A-17_SED_000-001CM do not require qualification. For sample MM-T2-C5-A-17_SED_036-038CM, the MS recovery of TOC Rep 1 (152%) was above the upper QC limit of 125%. The Rep 1 and average TOC results for sample MM-T2-C5-A-17_SED_036-038CM were qualified as estimated (J) due to the potential high bias.

SDG L1733621 – Sample MM-T2-C6-A-17_SED_000-001CM was used for MS analysis. The MS recovery for TOC Rep 1 (50%) was below the lower QC limit of 75%. The MS recovery does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample MM-T2-C6-A-17_SED_000-001CM do not require qualification.

SDG L1736451 – Sample MM-T1-C2-B_SED_000-001CM and MM-T1-C2-B_SED_040-045CM were used for MS analysis. For sample MM-T1-C2-B_SED_000-001CM, the MS recovery for TOC Rep 2 (177%) was above the upper QC limit of 125%. The MS recovery does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample MM-T1-C2-B_SED_000-001CM do not require qualification. For sample MM-T1-C2-B_SED_040-045CM, the MS recovery of TOC Rep 2 (137%) was above the upper QC limit of 125%. The Rep 2 and average TOC results for sample MM-T1-C2-B_SED_040-045CM were qualified as estimated (J) due to the potential high bias.

SDG L1736453 – Sample OR-T1-C2-B-17_SED_000-001CM was used for MS analysis. The MS recovery for TOC Rep 2 (4%) was below the lower QC limit of 75%. The MS recovery does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample OR-T1-C2-B-17_SED_000-001CM do not require qualification.

SDG L1736454 – Samples OR-T1-C5-A-17_SED_000-001CM, OR-T1-C5-A-17_SED_017-018CM, OR-T1-C5-A-17_SED_020-022CM, and OR-T1-C5-A-17_SED_085-90CM were used for MS analysis. The MS recoveries of samples OR-T1-C5-A-17_SED_000-001CM, OR-T1-C5-A-17_SED_020-022CM and OR-T1-C5-A-17_SED_085-90CM do not apply because the sample concentrations were >4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

For sample OR-T1-C5-A-17_SED_017-018CM, the MS recovery for TOC Rep 1 (141%) and Rep 2 (211%) were above the upper QC limit of 125%. The MS recovery of Rep 2 does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC Rep 2 result for sample OR-T1-C5-A-17_SED_017-018CM does not need to be qualified. Sample OR-T1-C5-A-17_SED_017-018CM Rep 1 and the average TOC results were qualified as estimated (J) due to the potential high bias.

SDG L1736455 – Sample OR-T2-C1-C-17_SED_000-001CM was used for MS analysis. The MS recoveries for TOC Rep 1 (0%) and Rep 2 (0%) were below the lower QC limit of 75%. The MS recoveries do not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample OR-T2-C1-C-17_SED_000-001CM do not require qualification.

SDG L1736456 – Sample OR-T2-C4-A-17_SED_032-034CM was used for MS analysis. The MS recoveries for TOC Rep 1 (206%) and Rep 2 (276%) were above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentration was >4X the spike amount added. Based on professional judgement the TOC results for sample OR-T2-C4-A-17_SED_032-034CM do not require qualification.

SDG L1736458 – Samples OR-T3-C3-B-17_SED_000-001CM and OR-T3-C3-B-17_SED_006-007CM were used for MS analysis. For sample OR-T3-C3-B-17_SED_000-001CM the MS recoveries for TOC Rep 1 (235%) and Rep 2 (411%) were above the upper QC limit of 125%. For sample OR-T3-C3-B-17_SED_006-007CM the MS recovery for TOC Rep 1 (0%) was below the lower QC limit of 75%. The MS recoveries do not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

SDG L1737040 – Samples MM-C1-C-17_SED_017-018CM and MM-C1-C-17_SED_024-026CM were used for MS/MSD analysis. For sample MM-C1-C-17_SED_017-018CM the MS recovery for TOC Rep 1 (58%) was below the lower QC limit of 75%. For sample MM-C1-C-17_SED_024-026CM the MS recovery for TOC Rep 2 (178%) and the MSD recovery for Rep 2 (132%) were above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for samples these samples do not require qualification.

SDG L1737041 – Samples MM-T1-C1-A-17_SED_001-002CM and MM-T1-C1-A-17_SED_013-014CM were used for MS/MSD analysis. For samples MM-T1-C1-A-17_SED_001-002CM and MM-T1-C1-A-17_SED_013-014CM the MS recoveries for TOC Rep 1 (145% and 212%, respectively) were above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for samples MM-T1-C1-A-17_SED_001-002CM and MM-T1-C1-A-17_SED_013-014CM do not require qualification.

SDG L1737042 – Samples MM-T1-C4-17_SED_003-004CM and MM-T1-C4-17_SED_013-014CM were used for MS analysis. For sample MM-T1-C4-17_SED_003-004CM the MS recovery for TOC Rep 1 (11%) was below the lower QC limit of 75% and Rep 2 (126%) was above the upper QC limit of 125%. For sample MM-T1-C4-17_SED_013-014CM the MS recovery for TOC Rep 1 (0%) was below the lower QC limit of 75% and Rep 2 (267%) was above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

SDG L1737043 – Samples MM-T1-C5-17_SED_007-008CM and MM-T1-C5-17_SED_034-036CM were used for MS analysis. For sample MM-T1-C5-17_SED_007-008CM the recoveries for TOC Rep 1 (72%) and Rep 2 (0%) were below the lower QC limit of 75%. For sample MM-T1-C5-17_SED_034-036CM the recovery for TOC Rep 2 (45%) was below the lower QC limit of 75%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

SDG L1737044 – Sample MM-T1-C6-17_SED_045-050CM was used for MS analysis. The recovery of TOC Rep 1 (0%) was below the lower QC limit of 25% and TOC Rep 2 (130%) was above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for this sample do not require qualification.

SDG L1737045 – Sample MM-T3-C3-B2-17_SED_015-016CM was used for MS analysis. The recoveries of TOC Rep 1 (433%) and Rep 2 (460%) were above the upper QC limit of 125%. Based on professional judgement all TOC results for sample MM-T3-C3-B2-17_SED_015-016CM were qualified as estimated (J) due to the potential high bias.

SDG L1737046 – Sample OR-T1-C3-A-17_SED_010-011CM and OR-T1-C3-A17_SED_075-080CM were used for MS analysis. For sample OR-T1-C3-A-17_SED_010-011CM the recovery of TOC Rep 1 (48%) was below the lower QC limit of 75% and the recovery of TOC Rep 2 (146%) was above the upper QC limit of 125%. The MS recovery of Rep 1 does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the Rep 2 and average TOC results for sample OR-T1-C3-A-17_SED_010-011CM were qualified as estimated (J) due to the potential high bias. For sample OR-T1-C3-A-17_SED_075-080CM the MS recoveries of TOC Rep 1 (150%) and Rep 2 (140%) were above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for sample OR-T1-C3-A17_SED_075-080CM do not require qualification.

SDG L1738093 – Sample MM-T3-C6-17_SED_032-034CM was used for MS analysis. The recovery of TOC Rep 1 (73%) was below the lower QC limit of 75%. The MS recovery does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample MM-T3-C6-17_SED_032-034CM do not require qualification.

SDG L1738103 – Samples MM-T4-C1-17_SED_005-006CM and MM-T4-C1-17_SED_040-045CM were used for MS analysis. For sample MM-T4-C1-17_SED_005-006CM the recovery of TOC Rep 1 (162%) was above the upper QC limit of 125%. For sample MM-T4-C1-17_SED_040-045CM the recoveries of TOC Rep 1 (147%) and Rep 2 (143%) were above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

SDG L1738104 – Samples MM-T4-C5-17_SED_007-008CM, MM-T4-C5-17_SED_008-009CM, and MM-T4-C5-17_SED_036-038CM were used for MS analysis. For sample MM-T4-C5-17_SED_007-008CM the recoveries of TOC Rep 1 (0%) and Rep 2 (8%) were below the lower QC limit of 75%. For sample MM-T4-C5-17_SED_008-009CM the recovery of TOC Rep 1 (169%) was above the upper QC limit of 125% and TOC Rep 2 (72%) was below the lower QC limit of 75%. For sample MM-T4-C5-17_SED_036-038CM the recovery of TOC Rep 1 (128%) was above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

SDG L1738105 – Samples MM-T4-C6-17_SED_000-001CM and MM-T4-C6-17_SED_038-040CM were used for MS analysis. For sample MM-T4-C6-17_SED_000-001CM the recoveries of TOC Rep 1 (133%) and Rep 2 (129%) were above the upper QC limit of 125%. For sample MM-T4-C6-17_SED_038-040CM the recovery of TOC Rep 1 (69%) was below the lower QC limit of 75% and the recovery of Rep 2 (126%) was above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

SDG L1738106 – Samples MM-T5-C1-17_SED_000-001CM and MM-T5-C1-17_SED_020-022CM were used for MS analysis. For sample MM-T5-C1-17_SED_000-001CM the recoveries of TOC Rep 1 (174%) and Rep 2 (152%) were above the upper QC limit of 125%. For sample MM-T5-C1-17_SED_020-022CM the recovery of TOC Rep 2 (131%) was above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

SDG L1738128 – Samples MM-T5-C2-17_SED_014-015CM and MM-T5-C2-17_SED_038-040CM were used for MS analysis. For sample MM-T5-C2-17_SED_014-015CM the recovery of TOC Rep 1 (127%) was above the upper QC limit of 125%. The MS recovery does not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for sample MM-T5-C2-17_SED_014-015CM do not require qualification. For sample MM-T5-C2-17_SED_038-040CM the recovery of TOC Rep 2 (195%) was above the upper QC limit of 125%. Based on professional judgement the Rep 2 and average TOC results for sample MM-T5-C2-17_SED_038-040CM were qualified as estimated (J) due to the potential high bias.

SDG L1739120 – Samples MM-T3-C4-D-17_SED_022-024CM and MM-T3-C4-D-17_SED_075-080CM were used for MS analysis. For sample MM-T3-C4-D-17_SED_022-024CM the recovery of TOC Rep 1 (7%) was below the lower QC limit of 75% and the recovery of TOC Rep 2 (152%) was above the upper QC limit of 125%. For sample MM-T3-C4-D-17_SED_075-080CM the recovery of TOC Rep 1 (222%) was above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

SDG L1739121 – Samples MM-T3-C7-17_SED_000-001CM and MM-T3-C7-17_SED_045-050CM were used for MS analysis. For sample MM-T3-C7-17_SED_000-001CM the recovery of TOC Rep 1 (50%) was below the lower QC limit of 75% and the recovery of TOC Rep 2 (136%) was above the upper QC limit of 125%. For sample MM-T3-C7-17_SED_045-050CM the recovery of TOC Rep 1 (147%) was above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

SDG L1739122 – Sample MM-T4-C7-17_SED_000-001CM was used for MS analysis. The recovery of TOC Rep 1 (150%) was above the upper QC limit of 125%. The TOC Rep 1 and average TOC results for sample MM-T4-C7-17_SED_000-001CM were qualified as estimated (J) due to the potential high bias.

SDG L1739123 – Samples MM-T5-C3-17_SED_010-011CM and MM-T5-C3-17_SED_065-070CM were used for MS analysis. For sample MM-T5-C3-17_SED_010-011CM the recovery of TOC Rep 1 (131%) was above the upper QC limit of 125%. For sample MM-T5-C3-17_SED_065-070CM the recovery of TOC Rep 1 (127%) was above the upper QC limit of 125% and TOC Rep 2 (27%) was below the lower QC limit of 75%. The MS recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

SDG L1739127 – Sample OR-T3-C4-A-17_SED_020-022CM was used for MS/MSD analysis. The recovery of TOC Rep 1 (131%) was above the upper QC limit of 125%. The TOC Rep 1 and average TOC results for sample OR-T3-C4-A-17_SED_020-022CM were qualified as estimated (J) due to the potential high bias.

SDG L1739540 – Sample MM-T1-C2-D-17_SED_05-07 was used for MS/MSD analysis. The recovery of TOC Rep 1 (127%) was above the upper QC limit of 125%. The TOC Rep 1 and average TOC results for sample MM-T1-C2-D-17_SED_05-07 were qualified as estimated (J) due to the potential high bias.

SDG L1739573 – Sample MM-T4-C2-F-17_SED_01-03 was used for MS analysis. The recoveries of TOC Rep 1 (137%) and Rep 2 (163%) were above the upper QC limit of 125%. The TOC Rep 1 and average TOC results for sample MM-T4-C2-F-17_SED_01-03 were qualified as estimated (J) due to the potential high bias. The MS recovery of Rep 2 does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC Rep 2 result for sample MM-T4-C2-F-17_SED_01-03 does not require qualification.

SDG L1739579 – Sample OR-T1-C5-C-17_SED_00-01 was used for MS analysis. The recovery of TOC Rep 1 (184%) was above the upper QC limit of 125%. The MS recovery does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample OR-T1-C5-C-17_SED_00-01 do not require qualification.

SDG L1739580 – Sample OR-T2-C1-D-17_SED_05-07 was used for MS analysis. The recovery of TOC Rep 1 (46%) was below the lower QC limit of 25% and the recovery of Rep 2 (130%) was above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample OR-T2-C1-D-17_SED_05-07 do not require qualification.

SDG L1739593 – Sample OR-T2-C3-C-17_SED_07-10 was used for MS analysis. The recoveries of TOC Rep 1 (145%) and Rep 2 (138%) were above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample OR-T2-C3-C-17_SED_07-10 do not require qualification.

SDG L1739691 – Sample MM-T3-C4-C-17_SED_00-01 was used for MS analysis. The recoveries of TOC Rep 1 (128%) and Rep 2 (157%) were above the upper QC limit of 125%. The MS recoveries do not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample MM-T3-C4-C-17_SED_00-01 do not require qualification.

SDG L1740284 – Samples MM-T2-C7-A-17_SED_015-016CM and MM-T2-C7-A-17_SED_020-022CM were used for MS analysis. For sample MM-T2-C7-A-17_SED_015-016CM the recovery of TOC Rep 2 (127%) was above the upper QC limit of 125%. The TOC Rep 2 and average TOC results for sample MM-T2-C7-A-17_SED_015-016CM were qualified as estimated (J) due to the potential high bias. For sample MM-T2-C7-A-17_SED_020-022CM the recovery of TOC Rep 2 (139%) was above the upper QC limit of 125%. The MS recovery does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the TOC results for sample MM-T2-C7-A-17_SED_020-022CM do not require qualification.

SDG L1740285 – Sample MM-T3-C1-17_SED_000-001CM was used for MS analysis. The recoveries of TOC Rep 1 (160%) and Rep 2 (150%) were above the upper QC limit of 125%. The Rep 1 MS recovery does not apply because the sample concentration was > 4X the spike amount added. Based on professional judgement the Rep 1 TOC result for sample MM-T3-C1-17_SED_000-001CM does not need to be qualified. The TOC Rep 2 and average TOC results for sample MM-T3-C1-17_SED_000-001CM were qualified as estimated (J) due to the potential high bias.

SDG L1740289 – Samples OR-T3-C1-B-17_SED_024-026CM and OR-T3-C1-B-17_SED_036-038CM were used for MS analysis. For sample OR-T3-C1-B-17_SED_024-026CM the MS recovery of TOC Rep 1 (161%) was above the upper QC limit of 125%. For sample OR-T3-C1-B-17_SED_036-038CM the MS recovery of TOC Rep 1 (126%) was above the upper QC limit of 125%. The recoveries do not apply because the sample concentrations were > 4X the spike amount added. Based on professional judgement the TOC results for these samples do not require qualification.

Field Duplicate

Samples submitted to the laboratory as field duplicates were logged incorrectly by the lab and processed as laboratory duplicates. These sample results are not available in the project database since laboratory duplicates are not included in the electronic data deliverable. The samples were evaluated as laboratory duplicates and assessed based on the more stringent laboratory duplicate criteria and qualified as necessary.

4.0 Percent Solids – 2540G

Holding Times and Preservation

The percent solids results from samples in the following SDGs have been J qualified due to technical holding time exceedance:

- J 1709432, 1709552, 1709555, 1709558, 1709562, 1709563, 1709564, 1709565, 1709566, 1709567, 1709568, 1709569, 1709570, 1709571, 1709572, 1709574, 1710289, 1710294, 1710307, 1710310, 1710313, 1710315, 1710633, 1710634, 1710637, 1710639, 1710641, 1710682, 1710684, 1710685, 1710728, 1710729, 1710730, 1710731, 1710732, 1710733, 1710907, 1710910, 1710913, 1710916, 1710917, 1710918, 1711046, 1711047, 1711050, 1711056, 1711057, 1711058, 1711059, 1711060, 1711061, 1711062, 1711063, 1711064, 1711065, 1711066, 1711067, 1711068, 1711069, 1711070, 1711071, 1711073, 1711077, 1711083, 1711084, 1711085, 1711151, 1711156, 1711171, 1711173, 1711174, 1711328, 1712044, 1712045, and 1712047. (J-HT)

Laboratory Duplicate

SDG 1709570 – Sample MM-T2-C4-B-17_SED_004-005CM was selected by the laboratory for duplicate analysis. The RPD (57%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample MM-T2-C4-B-17_SED_004-005CM was qualified estimated (J) due to the imprecision.

SDG 1710731 – Sample MM-T4-C5-17_SED_005-006CM was selected by the laboratory for duplicate analysis. The RPD (15.6%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample MM-T4-C5-17_SED_005-006CM was qualified estimated (J) due to the imprecision.

SDG L1733618 – Sample MM-T1-C3-B-17_SED_000-001CM was selected by the laboratory for duplicate analysis. The RPD (36%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample MM-T1-C3-B-17_SED_000-001CM was qualified estimated (J) due to the imprecision.

SDG L1733621 – Sample MM-T2-C6-A-17_SED_000-001CM was selected by the laboratory for duplicate analysis. The RPD (13%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample MM-T2-C6-A-17_SED_000-001CM was qualified estimated (J) due to the imprecision.

SDG L1736453 – Sample OR-T1-C2-B-17_SED_000-001CM was selected by the laboratory for duplicate analysis. The RPD (15%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample OR-T1-C2-B-17_SED_000-001CM was qualified estimated (J) due to the imprecision.

SDG L1736455 – Sample OR-T2-C1-C-17_SED_000-001CM was selected by the laboratory for duplicate analysis. The RPD (12%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample OR-T2-C1-C-17_SED_000-001CM was qualified estimated (J) due to the imprecision.

SDG L1736456 – Sample OR-T2-C4-A-17_SED_000-001CM was selected by the laboratory for duplicate analysis. The RPD (25%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample OR-T2-C4-A-17_SED_000-001CM was qualified estimated (J) due to the imprecision.

SDG L1736458 – Sample OR-T3-C3-B-17_SED_020-022CM was selected by the laboratory for duplicate analysis. The RPD (11%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample OR-T3-C3-B-17_SED_020-022CM was qualified estimated (J) due to the imprecision.

SDG L1737045 – Sample MM-T3-C3-B2-17_SED_000-001CM was selected by the laboratory for duplicate analysis. The RPD (14%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample MM-T3-C3-B2-17_SED_000-001CM was qualified estimated (J) due to the imprecision.

SDG L1738093 – Sample MM-T3-C6-17_SED_000-001CM was selected by the laboratory for duplicate analysis. The RPD (32%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample MM-T3-C6-17_SED_000-001CM was qualified estimated (J) due to the imprecision.

SDG L1738128 – Sample MM-T5-C2-17_SED_001-002CM was selected by the laboratory for duplicate analysis. The RPD (11%) exceeds the QC limit of 10%. Based on professional judgment, the percent solids result for sample MM-T5-C2-17_SED_001-002CM was qualified estimated (J) due to the imprecision.

References:

Amec Foster Wheeler, 2016. “Draft Penobscot River Estuary Phase III – Engineering Study Quality Assurance Project Plan”, Penobscot River, Maine, July 2016.

Eurofins, 2017. “AMEC Sediment Lab Homogenization and Subsampling Procedure.” Work Instruction EFSR-P-SP-WI15953; August 8, 2017.

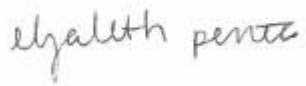
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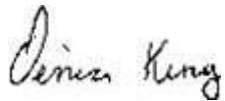
U.S. Environmental Protection Agency (USEPA), 2014. "National Functional Guidelines for Inorganic Superfund Data Review"; Office of Superfund Remediation and Technology Innovation; EPA-540-R-013-001; August 2014.

U.S. Environmental Protection Agency (USEPA), 2013. "EPA New England Environmental Data Review Supplement for Regional Data Review Elements and Superfund Specific Guidance/Procedures"; Quality Assurance Unit Staff; Office of Environmental Measurement and Evaluation; April 22, 2013.

Data Validator: Elizabeth Penta January 22, 2018



Senior Reviewer: Denise King January 23, 2018



**TABLE 1
DATA VALIDATION SUMMARY**

2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES

PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709432, 1709552, 1709555, 1709558, 1709562, 1709563, 1709564, 1709565, 1709566, 1709567, 1709568, 1709569, 1709570, 1709571, 1709572, 1709574, 1710289, 1710294, 1710307, 1710310, 1710313, 1710315, 1710633, 1710634, 1710637, 1710639, 1710641, 1710682, 1710684, 1710685, 1710728, 1710729, 1710730, 1710731, 1710732, 1710733, 1710907, 1710910, 1710913, 1710916, 1710917, 1710918, 1711046, 1711047, 1711050, 1711056, 1711057, 1711058, 1711059, 1711060, 1711061, 1711062, 1711063, 1711064, 1711065, 1711066, 1711067, 1711068, 1711069, 1711070, 1711071, 1711073, 1711077, 1711083, 1711084, 1711085, 1711151, 1711156, 1711171, 1711173, 1711174, 1711328, 1712044, 1712045, 1712047, L1732774, L1733612, L1733618, L1733619, L1733620, L1733621, L1736451, L1736453, L1736454, L1736455, L1736456, L1736458, L1737040, L1737041, L1737042, L1737043, L1737044, L1737045, L1737046, L1737047, L1738093, L1738103, L1738104, L1738105, L1738106, L1738128, L1739120, L1739121, L1739122, L1739123, L1739124, L1739127, L1739536, L1739537, L1739540, L1739541, L1739542, L1739572, L1739573, L1739577, L1739578, L1739579, L1739580, L1739581, L1739593, L1739594, L1739595, L1739596, L1739597, L1739598, L1739599, L1739601, L1739602, L1739653, L1739656, L1739691, L1740283, L1740284, L1740285, L1740287, L1740289 and L1741133

SDG	Media	Location	Field Sample ID	Sample Date	QC Code	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
						Analysis Method	% Solids		
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_000-001CM	9/12/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_001-002CM	9/12/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_002-003CM	9/12/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_003-004CM	9/12/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_004-005CM	9/12/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_005-006CM	9/12/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_006-007CM	9/12/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_007-008CM	9/12/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_008-009CM	9/12/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_009-010CM	9/12/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_010-011CM	9/12/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_011-012CM	9/13/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_012-013CM	9/13/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_013-014CM	9/13/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_014-015CM	9/13/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_015-016CM	9/13/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_016-017CM	9/13/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_017-018CM	9/13/2017	FS		1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_018-019CM	9/13/2017	FS		1	1	

Created by: BCG 1/15/2018

Checked by: EP 1/22/2018

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_019-020CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_020-022CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_022-024CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_024-026CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_026-028CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_028-030CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_030-032CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_032-034CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_034-036CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_036-038CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_038-040CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_040-045CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_045-050CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_050-055CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_055-060CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_060-065CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_065-070CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_070-075CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_075-080CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_080-085CM	9/13/2017	FS	1	1	
1709432	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_085-090CM	9/13/2017	FS	1	1	
1709552	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_040-045CM	9/14/2017	FS	1	1	
1709552	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_045-050CM	9/14/2017	FS	1	1	
1709552	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_050-055CM	9/14/2017	FS	1	1	
1709552	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_055-060CM	9/14/2017	FS	1	1	
1709552	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_060-065CM	9/14/2017	FS	1	1	
1709552	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_065-070CM	9/14/2017	FS	1	1	
1709552	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_070-075CM	9/14/2017	FS	1	1	
1709552	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_075-080CM	9/14/2017	FS	1	1	

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DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709552	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_080-085CM	9/14/2017	FS	1	1	
1709552	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_085-090CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_015-016CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_016-017CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_017-018CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_018-019CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_019-020CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_020-022CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_022-024CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_024-026CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_026-028CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_028-030CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_030-032CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_032-034CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_034-036CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_036-038CM	9/14/2017	FS	1	1	
1709555	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_038-040CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_000-001CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_001-002CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_002-003CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_003-004CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_004-005CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_005-006CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_006-007CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_007-008CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_008-009CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_009-010CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_010-011CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_011-012CM	9/14/2017	FS	1	1	

Created by: BCG 1/15/2018

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_012-013CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_013-014CM	9/14/2017	FS	1	1	
1709558	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_014-015CM	9/14/2017	FS	1	1	
1709562	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_040-045CM	9/18/2017	FS	1	1	
1709562	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_045-050CM	9/18/2017	FS	1	1	
1709562	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_050-055CM	9/18/2017	FS	1	1	
1709562	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_055-060CM	9/18/2017	FS	1	1	
1709562	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_060-065CM	9/18/2017	FS	1	1	
1709562	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_065-070CM	9/18/2017	FS	1	1	
1709562	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_070-075CM	9/18/2017	FS	1	1	
1709562	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_075-080CM	9/18/2017	FS	1	1	
1709562	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_080-085CM	9/18/2017	FS	1	1	
1709562	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_085-090CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_015-016CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_016-017CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_017-018CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_018-019CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_019-020CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_020-022CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_022-024CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_024-026CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_026-028CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_028-030CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_030-032CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_032-034CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_034-036CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_036-038CM	9/18/2017	FS	1	1	
1709563	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_038-040CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_000-001CM	9/18/2017	FS	1	1	

Created by: BCG 1/15/2018

Checked by: EP 1/22/2018

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_001-002CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_002-003CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_003-004CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_004-005CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_005-006CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_006-007CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_007-008CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_008-009CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_009-010CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_010-011CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_011-012CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_012-013CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_013-014CM	9/18/2017	FS	1	1	
1709564	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_014-015CM	9/18/2017	FS	1	1	
1709565	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_040-045CM	9/15/2017	FS	1	1	
1709565	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_045-050CM	9/15/2017	FS	1	1	
1709565	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_050-055CM	9/15/2017	FS	1	1	
1709565	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_055-060CM	9/15/2017	FS	1	1	
1709565	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_060-065CM	9/15/2017	FS	1	1	
1709565	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_065-070CM	9/15/2017	FS	1	1	
1709565	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_070-075CM	9/15/2017	FS	1	1	
1709565	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_075-080CM	9/15/2017	FS	1	1	
1709565	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_080-085CM	9/15/2017	FS	1	1	
1709565	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_085-090CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_015-016CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_016-017CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_017-018CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_018-019CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_019-020CM	9/15/2017	FS	1	1	

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_020-022CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_022-024CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_024-026CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_026-028CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_028-030CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_030-032CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_032-034CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_034-036CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_036-038CM	9/15/2017	FS	1	1	
1709566	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_038-040CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_000-001CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_001-002CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_002-003CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_003-004CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_004-005CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_005-006CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_006-007CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_007-008CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_008-009CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_009-010CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_010-011CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_011-012CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_012-013CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_013-014CM	9/15/2017	FS	1	1	
1709567	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_014-015CM	9/15/2017	FS	1	1	
1709568	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_040-045CM	9/15/2017	FS	1	1	
1709568	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_045-050CM	9/15/2017	FS	1	1	
1709568	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_050-055CM	9/15/2017	FS	1	1	
1709568	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_055-060CM	9/15/2017	FS	1	1	

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709568	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_060-065CM	9/15/2017	FS	1	1	
1709568	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_065-070CM	9/15/2017	FS	1	1	
1709568	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_070-075CM	9/15/2017	FS	1	1	
1709568	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_075-080CM	9/15/2017	FS	1	1	
1709568	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_080-085CM	9/15/2017	FS	1	1	
1709568	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_085-090CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_015-016CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_016-017CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_017-018CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_018-019CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_019-020CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_020-022CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_022-024CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_024-026CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_026-028CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_028-030CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_030-032CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_032-034CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_034-036CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_036-038CM	9/15/2017	FS	1	1	
1709569	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_038-040CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_000-001CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_001-002CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_002-003CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_003-004CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_004-005CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_005-006CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_006-007CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_007-008CM	9/15/2017	FS	1	1	

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TABLE 1
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_008-009CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_009-010CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_010-011CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_011-012CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_012-013CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_013-014CM	9/15/2017	FS	1	1	
1709570	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_014-015CM	9/15/2017	FS	1	1	
1709571	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_040-045CM	9/14/2017	FS	1	1	
1709571	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_045-050CM	9/14/2017	FS	1	1	
1709571	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_050-055CM	9/14/2017	FS	1	1	
1709571	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_055-060CM	9/14/2017	FS	1	1	
1709571	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_060-065CM	9/14/2017	FS	1	1	
1709571	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_065-070CM	9/14/2017	FS	1	1	
1709571	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_070-075CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_015-016CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_016-017CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_017-018CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_018-019CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_019-020CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_020-022CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_022-024CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_024-026CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_026-028CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_028-030CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_030-032CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_032-034CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_034-036CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_036-038CM	9/14/2017	FS	1	1	
1709572	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_038-040CM	9/14/2017	FS	1	1	

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_000-001CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_001-002CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_002-003CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_003-004CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_004-005CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_005-006CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_006-007CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_007-008CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_008-009CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_009-010CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_010-011CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_011-012CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_012-013CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_013-014CM	9/13/2017	FS	1	1	
1709574	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_014-015CM	9/14/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_000-001CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_001-002CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_002-003CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_003-004CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_004-005CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_005-006CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_006-007CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_007-008CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_008-009CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_009-010CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_010-011CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_011-012CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_012-013CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_013-014CM	10/3/2017	FS	1	1	

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_014-015CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_015-016CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_016-017CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_017-018CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_018-019CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_019-020CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_020-022CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_022-024CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_024-026CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_026-028CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_028-030CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_030-032CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_032-034CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_034-036CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_036-038CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_038-040CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_040-045CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_045-050CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_050-055CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_055-060CM	10/3/2017	FS	1	1	
1710289	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_060-065CM	10/3/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_000-001CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_001-002CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_002-003CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_003-004CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_004-005CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_005-006CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_006-007CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_007-008CM	9/28/2017	FS	1	1	

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_008-009CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_009-010CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_010-011CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_011-012CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_012-013CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_013-014CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_014-015CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_015-016CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_016-017CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_017-018CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_018-019CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_019-020CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_020-022CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_022-024CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_024-026CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_026-028CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_028-030CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_030-032CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_032-034CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_034-036CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_036-038CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_038-040CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_040-045CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_045-050CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_050-055CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_055-060CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_060-065CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_065-070CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_070-075CM	9/28/2017	FS	1	1	

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DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_075-080CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_080-085CM	9/28/2017	FS	1	1	
1710294	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_085-090CM	9/28/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_000-001CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_001-002CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_002-003CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_003-004CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_004-005CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_005-006CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_006-007CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_007-008CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_008-009CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_009-010CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_010-011CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_011-012CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_012-013CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_013-014CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_014-015CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_015-016CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_016-017CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_017-018CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_018-019CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_019-020CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_020-022CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_022-024CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_024-026CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_026-028CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_028-030CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_030-032CM	9/29/2017	FS	1	1	

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DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_032-034CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_034-036CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_036-038CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_038-040CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_040-045CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_045-050CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_050-055CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_055-060CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_060-065CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_065-070CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_070-075CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_075-080CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_080-085CM	9/29/2017	FS	1	1	
1710307	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_085-090CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_000-001CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_001-002CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_002-003CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_003-004CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_004-005CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_005-006CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_006-007CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_007-008CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_008-009CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_009-010CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_010-011CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_011-012CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_012-013CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_013-014CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_014-015CM	9/29/2017	FS	1	1	

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DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_015-016CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_016-017CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_017-018CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_018-019CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_019-020CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_020-022CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_022-024CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_024-026CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_026-028CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_028-030CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_030-032CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_032-034CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_034-036CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_036-038CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_038-040CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_040-045CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_045-050CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_050-055CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_055-060CM	9/29/2017	FS	1	1	
1710310	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_060-065CM	9/29/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_000-001CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_001-002CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_002-003CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_003-004CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_004-005CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_005-006CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_006-007CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_007-008CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_008-009CM	10/3/2017	FS	1	1	

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_009-010CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_010-011CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_011-012CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_012-013CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_013-014CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_014-015CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_015-016CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_016-017CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_017-018CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_018-019CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_019-020CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_020-022CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_022-024CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_024-026CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_026-028CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_028-030CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_030-032CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_032-034CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_034-036CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_036-038CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_038-040CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_040-045CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_045-050CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_050-055CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_055-060CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_060-065CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_065-070CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_070-075CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_075-080CM	10/3/2017	FS	1	1	

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_080-085CM	10/3/2017	FS	1	1	
1710313	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_085-090CM	10/3/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_000-001CM	9/29/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_001-002CM	9/29/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_002-003CM	9/29/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_003-004CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_004-005CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_005-006CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_006-007CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_007-008CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_008-009CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_009-010CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_010-011CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_011-012CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_012-013CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_013-014CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_014-015CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_015-016CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_016-017CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_017-018CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_018-019CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_019-020CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_020-022CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_022-024CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_024-026CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_026-028CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_028-030CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_030-032CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_032-034CM	10/2/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_034-036CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_036-038CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_038-040CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_040-045CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_045-050CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_050-055CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_055-060CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_060-065CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_065-070CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_070-075CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_075-080CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_080-085CM	10/2/2017	FS	1	1	
1710315	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_085-090CM	10/2/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_000-001CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_001-002CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_002-003CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_003-004CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_004-005CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_005-006CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_006-007CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_007-008CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_008-009CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_009-010CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_010-011CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_011-012CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_012-013CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_013-014CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_014-015CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_015-016CM	10/9/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_016-017CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_017-018CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_018-019CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_019-020CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_020-022CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_022-024CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_024-026CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_026-028CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_028-030CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_030-032CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_032-034CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_034-036CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_036-038CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_038-040CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_040-045CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_045-050CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_050-055CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_055-060CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_060-065CM	10/9/2017	FS	1	1	
1710633	SED	MM-T1-C6	MM-T1-C6-A-17_SED_065-070CM	10/9/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_000-001CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_001-002CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_002-003CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_003-004CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_004-005CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_005-006CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_006-007CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_007-008CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_008-009CM	10/6/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1710634	SED	MM-C1-C	MM-C1-C-17_SED_009-010CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_010-011CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_011-012CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_012-013CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_013-014CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_014-015CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_015-016CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_016-017CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_017-018CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_018-019CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_019-020CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_020-022CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_022-024CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_024-026CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_026-028CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_028-030CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_030-032CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_032-034CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_034-036CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_036-038CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_038-040CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_040-045CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_045-050CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_050-055CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_055-060CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_060-065CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_065-070CM	10/6/2017	FS	1	1	
1710634	SED	MM-C1-C	MM-C1-C-17_SED_070-075CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_000-001CM	10/6/2017	FS	1	1	

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_001-002CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_002-003CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_003-004CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_004-005CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_005-006CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_006-007CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_007-008CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_008-009CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_009-010CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_010-011CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_011-012CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_012-013CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_013-014CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_014-015CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_015-016CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_016-017CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_017-018CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_018-019CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_019-020CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_020-022CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_022-024CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_024-026CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_026-028CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_028-030CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_030-032CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_032-034CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_034-036CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_036-038CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_038-040CM	10/6/2017	FS	1	1	

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TABLE 1
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_040-045CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_045-050CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_050-055CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_055-060CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_060-065CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_065-070CM	10/6/2017	FS	1	1	
1710637	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_070-075CM	10/6/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_000-001CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_001-002CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_002-003CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_003-004CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_004-005CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_005-006CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_006-007CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_007-008CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_008-009CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_009-010CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_010-011CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_011-012CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_012-013CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_013-014CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_014-015CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_015-016CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_016-017CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_017-018CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_018-019CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_019-020CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_020-022CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_022-024CM	10/3/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_024-026CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_026-028CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_028-030CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_030-032CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_032-034CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_034-036CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_036-038CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_038-040CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_040-045CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_045-050CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_050-055CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_055-060CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_060-065CM	10/3/2017	FS	1	1	
1710639	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_065-070CM	10/3/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_000-001CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_001-002CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_002-003CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_003-004CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_004-005CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_005-006CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_006-007CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_007-008CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_008-009CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_009-010CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_010-011CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_011-012CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_012-013CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_013-014CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_014-015CM	10/9/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_015-016CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_016-017CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_017-018CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_018-019CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_019-020CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_020-022CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_022-024CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_024-026CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_026-028CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_028-030CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_030-032CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_032-034CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_034-036CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_036-038CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_038-040CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_040-045CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_045-050CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_050-055CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_055-060CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_060-065CM	10/9/2017	FS	1	1	
1710641	SED	MM-T1-C5	MM-T1-C5-A-17_SED_065-070CM	10/9/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_000-001CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_000-001CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_001-002CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_001-002CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_002-003CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_002-003CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_003-004CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_003-004CM_DUP	10/6/2017	FD	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_004-005CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_005-006CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_005-006CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_006-007CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_006-007CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_007-008CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_007-008CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_008-009CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_008-009CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_009-010CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_009-010CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_010-011CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_010-011CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_011-012CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_011-012CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_012-013CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_012-013CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_013-014CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_013-014CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_014-015CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_014-015CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_015-016CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_015-016CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_016-017CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_016-017CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_017-018CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_017-018CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_018-019CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_018-019CM_DUP	10/6/2017	FD	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_019-020CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_019-020CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_020-022CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_020-022CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_022-024CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_022-024CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_024-026CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_024-026CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_026-028CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_026-028CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_028-030CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_028-030CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_030-032CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_030-032CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_032-034CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_032-034CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_034-036CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_034-036CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_036-038CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_036-038CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_038-040CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_038-040CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_040-045CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_040-045CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_045-050CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_045-050CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_050-055CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_050-055CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_055-060CM	10/6/2017	FS	1	1	

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TABLE 1
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_055-060CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_060-065CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_060-065CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_065-070CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_065-070CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_070-075CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_070-075CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_075-080CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_075-080CM_DUP	10/6/2017	FD	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_080-085CM	10/6/2017	FS	1	1	
1710682	SED	MM-T1-C4	MM-T1-C4-17_SED_080-085CM_DUP	10/6/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_000-001CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_000-001CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_001-002CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_001-002CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_002-003CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_002-003CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_003-004CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_003-004CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_004-005CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_004-005CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_005-006CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_005-006CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_006-007CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_006-007CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_007-008CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_007-008CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_008-009CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_008-009CM_DUP	10/4/2017	FD	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_009-010CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_009-010CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_010-011CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_010-011CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_011-012CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_011-012CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_012-013CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_012-013CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_013-014CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_013-014CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_014-015CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_014-015CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_015-016CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_015-016CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_016-017CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_016-017CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_017-018CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_017-018CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_018-019CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_018-019CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_019-020CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_019-020CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_020-022CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_020-022CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_022-024CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_022-024CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_024-026CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_024-026CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_026-028CM	10/4/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_026-028CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_028-030CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_028-030CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_030-032CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_030-032CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_032-034CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_032-034CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_034-036CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_034-036CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_036-038CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_036-038CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_038-040CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_038-040CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_040-045CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_040-045CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_045-050CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_045-050CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_050-055CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_050-055CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_055-060CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_055-060CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_060-065CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_060-065CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_065-070CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_065-070CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_070-075CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_070-075CM_DUP	10/4/2017	FD	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_075-080CM	10/4/2017	FS	1	1	
1710684	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_075-080CM_DUP	10/4/2017	FD	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_000-001CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_000-001CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_001-002CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_001-002CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_002-003CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_003-004CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_003-004CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_004-005CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_004-005CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_005-006CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_005-006CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_006-007CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_006-007CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_007-008CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_008-009CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_008-009CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_009-010CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_009-010CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_010-011CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_010-011CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_011-012CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_011-012CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_012-013CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_012-013CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_013-014CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_013-014CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_014-015CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_014-015CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_015-016CM	10/4/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_015-016CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_016-017CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_016-017CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_017-018CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_017-018CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_018-019CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_018-019CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_019-020CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_019-020CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_020-022CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_020-022CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_022-024CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_022-024CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_024-026CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_024-026CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_026-028CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_026-028CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_028-030CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_028-030CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_030-032CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_030-032CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_032-034CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_032-034CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_034-036CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_034-036CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_036-038CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_036-038CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_038-040CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_038-040CM_DUP	10/4/2017	FD	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_040-045CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_040-045CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_045-050CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_045-050CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_050-055CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_050-055CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_055-060CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_055-060CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_060-065CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_060-065CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_065-070CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_065-070CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_070-075CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_070-075CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_075-080CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_075-080CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_080-085CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_080-085CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_085-090CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_085-090CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_090-095CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_090-095CM_DUP	10/4/2017	FD	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_095-101CM	10/4/2017	FS	1	1	
1710685	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_095-101CM_DUP	10/4/2017	FD	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_000-001CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_001-002CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_002-003CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_003-004CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_004-005CM	10/10/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_005-006CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_006-007CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_007-008CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_008-009CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_009-010CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_010-011CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_011-012CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_012-013CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_013-014CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_014-015CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_015-016CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_016-017CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_017-018CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_018-019CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_019-020CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_020-022CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_022-024CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_024-026CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_026-028CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_028-030CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_030-032CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_032-034CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_034-036CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_036-038CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_038-040CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_040-045CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_045-050CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_050-055CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_055-060CM	10/10/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_060-065CM	10/10/2017	FS	1	1	
1710728	SED	MM-T3-C6	MM-T3-C6-17_SED_065-070CM	10/10/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_000-001CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_001-002CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_002-003CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_003-004CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_004-005CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_005-006CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_006-007CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_007-008CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_008-009CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_009-010CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_010-011CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_011-012CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_012-013CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_013-014CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_014-015CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_015-016CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_016-017CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_017-018CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_018-019CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_019-020CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_020-022CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_022-024CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_024-026CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_026-028CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_028-030CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_030-032CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_032-034CM	10/12/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_034-036CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_036-038CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_038-040CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_040-045CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_045-050CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_050-055CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_055-060CM	10/12/2017	FS	1	1	
1710729	SED	MM-T5-C2	MM-T5-C2-17_SED_060-065CM	10/12/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_000-001CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_001-002CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_002-003CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_003-004CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_004-005CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_005-006CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_006-007CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_007-008CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_008-009CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_009-010CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_010-011CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_011-012CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_012-013CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_013-014CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_014-015CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_015-016CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_016-017CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_017-018CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_018-019CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_019-020CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_020-022CM	10/11/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_022-024CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_024-026CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_026-028CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_028-030CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_030-032CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_032-034CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_034-036CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_036-038CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_038-040CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_040-045CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_045-050CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_050-055CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_055-060CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_060-065CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_065-070CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_070-075CM	10/11/2017	FS	1	1	
1710730	SED	MM-T4-C6	MM-T4-C6-17_SED_075-080CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_000-001CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_001-002CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_002-003CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_003-004CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_004-005CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_005-006CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_006-007CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_007-008CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_008-009CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_009-010CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_010-011CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_011-012CM	10/11/2017	FS	1	1	

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_012-013CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_013-014CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_014-015CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_015-016CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_016-017CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_017-018CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_018-019CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_019-020CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_020-022CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_022-024CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_024-026CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_026-028CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_028-030CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_030-032CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_032-034CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_034-036CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_036-038CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_038-040CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_040-045CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_045-050CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_050-055CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_055-060CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_060-065CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_065-070CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_070-075CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_075-080CM	10/11/2017	FS	1	1	
1710731	SED	MM-T4-C5	MM-T4-C5-17_SED_080-085CM	10/11/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_000-001CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_001-002CM	10/10/2017	FS	1	1	

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_002-003CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_003-004CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_004-005CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_005-006CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_006-007CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_007-008CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_008-009CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_009-010CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_010-011CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_011-012CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_012-013CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_013-014CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_014-015CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_015-016CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_016-017CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_017-018CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_018-019CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_019-020CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_020-022CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_022-024CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_024-026CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_026-028CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_028-030CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_030-032CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_032-034CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_034-036CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_036-038CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_038-040CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_040-045CM	10/10/2017	FS	1	1	

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_045-050CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_050-055CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_055-060CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_060-065CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_065-070CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_070-075CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_075-080CM	10/10/2017	FS	1	1	
1710732	SED	MM-T4-C1	MM-T4-C1-17_SED_080-085CM	10/10/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_000-001CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_001-002CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_002-003CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_003-004CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_004-005CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_005-006CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_006-007CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_007-008CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_008-009CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_009-010CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_010-011CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_011-012CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_012-013CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_013-014CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_014-015CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_015-016CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_016-017CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_017-018CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_018-019CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_019-020CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_020-022CM	10/13/2017	FS	1	1	

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_022-024CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_024-026CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_026-028CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_028-030CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_030-032CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_032-034CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_034-036CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_036-038CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_038-040CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_040-045CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_045-050CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_050-055CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_055-060CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_060-065CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_065-070CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_070-075CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_075-080CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_080-085CM	10/13/2017	FS	1	1	
1710733	SED	MM-T5-C1	MM-T5-C1-17_SED_085-090CM	10/13/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_000-001CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_000-001CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_001-002CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_001-002CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_002-003CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_002-003CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_003-004CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_003-004CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_004-005CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_004-005CM_DUP	10/16/2017	FD	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_005-006CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_005-006CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_006-007CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_006-007CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_007-008CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_007-008CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_008-009CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_008-009CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_009-010CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_009-010CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_010-011CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_010-011CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_011-012CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_011-012CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_012-013CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_012-013CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_013-014CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_013-014CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_014-015CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_014-015CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_015-016CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_015-016CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_016-017CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_016-017CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_017-018CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_017-018CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_018-019CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_018-019CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_019-020CM	10/16/2017	FS	1	1	

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_019-020CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_020-022CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_020-022CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_024-026CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_024-026CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_026-028CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_026-028CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_028-030CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_028-030CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_030-032CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_030-032CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_032-034CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_032-034CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_034-036CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_034-036CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_036-038CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_036-038CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_038-040CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_038-040CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_040-045CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_040-045CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_045-050CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_045-050CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_050-055CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_050-055CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_055-060CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_055-060CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_060-065CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_060-065CM_DUP	10/16/2017	FD	1	1	

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TABLE 1
DATA VALIDATION SUMMARY
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_065-070CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_065-070CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_070-075CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_070-075CM_DUP	10/16/2017	FD	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_075-080CM	10/16/2017	FS	1	1	
1710907	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_075-080CM_DUP	10/16/2017	FD	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_000-001CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_001-002CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_002-003CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_003-004CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_004-005CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_005-006CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_006-007CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_007-008CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_008-009CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_009-010CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_010-011CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_011-012CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_012-013CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_013-014CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_014-015CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_015-016CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_016-017CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_017-018CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_018-019CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_019-020CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_020-022CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_022-024CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_024-026CM	10/16/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_026-028CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_028-030CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_030-032CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_032-034CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_034-036CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_036-038CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_038-040CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_040-045CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_045-050CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_050-055CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_055-060CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_060-065CM	10/16/2017	FS	1	1	
1710910	SED	MM-T3-C7	MM-T3-C7-17_SED_065-070CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_000-001CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_000-001CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_001-002CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_001-002CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_002-003CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_002-003CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_003-004CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_003-004CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_004-005CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_004-005CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_005-006CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_005-006CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_006-007CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_006-007CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_007-008CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_007-008CM_DUP	10/16/2017	FD	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_008-009CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_008-009CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_009-010CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_009-010CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_010-011CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_010-011CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_011-012CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_011-012CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_012-013CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_012-013CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_013-014CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_013-014CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_014-015CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_014-015CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_015-016CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_015-016CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_016-017CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_016-017CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_017-018CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_017-018CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_018-019CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_018-019CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_019-020CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_019-020CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_020-022CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_020-022CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_022-024CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_022-024CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_024-026CM	10/16/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_024-026CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_026-028CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_026-028CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_028-030CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_028-030CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_030-032CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_030-032CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_032-034CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_032-034CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_034-036CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_034-036CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_036-038CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_036-038CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_038-040CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_038-040CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_040-045CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_040-045CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_050-055CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_050-055CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_060-065CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_060-065CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_065-070CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_065-070CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_070-075CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_070-075CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_075-080CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_075-080CM_DUP	10/16/2017	FD	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_080-085CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_080-085CM_DUP	10/16/2017	FD	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_085-090CM	10/16/2017	FS	1	1	
1710913	SED	MM-T4-C7	MM-T4-C7-17_SED_085-090CM_DUP	10/16/2017	FD	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_000-001CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_001-002CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_002-003CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_003-004CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_004-005CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_005-006CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_006-007CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_007-008CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_008-009CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_009-010CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_010-011CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_011-012CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_012-013CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_013-014CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_014-015CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_015-016CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_016-017CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_017-018CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_018-019CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_019-020CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_020-022CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_022-024CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_024-026CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_026-028CM	10/13/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_028-030CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_030-032CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_032-034CM	10/16/2017	FS	1	1	

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TABLE 1
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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_034-036CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_036-038CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_038-040CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_040-045CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_045-050CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_050-055CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_055-060CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_060-065CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_065-070CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_070-075CM	10/16/2017	FS	1	1	
1710916	SED	MM-T5-C3	MM-T5-C3-17_SED_075-080CM	10/16/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_000-001CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_001-002CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_002-003CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_003-004CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_004-005CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_005-006CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_006-007CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_007-008CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_008-009CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_009-010CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_010-011CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_011-012CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_012-013CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_013-014CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_014-015CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_015-016CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_016-017CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_017-018CM	10/17/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_018-019CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_019-020CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_020-022CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_022-024CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_024-026CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_026-028CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_028-030CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_030-032CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_032-034CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_034-036CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_036-038CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_038-040CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_040-045CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_045-050CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_055-060CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_060-065CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_065-070CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_070-075CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_075-080CM	10/17/2017	FS	1	1	
1710917	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_080-085CM	10/17/2017	FS	1	1	
1710918	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_00-01	10/16/2017	FS	1	1	
1710918	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_01-03	10/16/2017	FS	1	1	
1710918	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_03-05	10/16/2017	FS	1	1	
1710918	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_05-07	10/16/2017	FS	1	1	
1710918	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_07-10	10/16/2017	FS	1	1	
1710918	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_10-15	10/16/2017	FS	1	1	
1711046	SED	PBR-20-G	PBR-20-G-17_SED_00-01	10/23/2017	FS	1	1	
1711046	SED	PBR-20-G	PBR-20-G-17_SED_01-03	10/23/2017	FS	1	1	
1711046	SED	PBR-20-G	PBR-20-G-17_SED_03-05	10/23/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1711047	SED	UPB-MU11-GC-1-E	UPB-MU11-GC-1-E-17_SED_00-01	10/23/2017	FS	1	1	
1711047	SED	UPB-MU11-GC-1-E	UPB-MU11-GC-1-E-17_SED_01-03	10/23/2017	FS	1	1	
1711047	SED	UPB-MU11-GC-1-E	UPB-MU11-GC-1-E-17_SED_03-05	10/23/2017	FS	1	1	
1711047	SED	UPB-MU11-GC-1-E	UPB-MU11-GC-1-E-17_SED_05-07	10/23/2017	FS	1	1	
1711047	SED	UPB-MU11-GC-1-E	UPB-MU11-GC-1-E-17_SED_07-10	10/23/2017	FS	1	1	
1711047	SED	UPB-MU11-GC-1-E	UPB-MU11-GC-1-E-17_SED_07-10_DUP	10/23/2017	FS	1	1	
1711050	SED	VE-MU4-GC-1-F	VE-MU4-GC-1-F-17_SED_00-01	10/19/2017	FS	1	1	
1711050	SED	VE-MU4-GC-1-F	VE-MU4-GC-1-F-17_SED_01-03	10/19/2017	FS	1	1	
1711050	SED	VE-MU4-GC-1-F	VE-MU4-GC-1-F-17_SED_03-05	10/19/2017	FS	1	1	
1711050	SED	VE-MU4-GC-1-F	VE-MU4-GC-1-F-17_SED_03-05_DUP	10/19/2017	FD	1	1	
1711056	SED	OR-T3-C5-E	OR-T3-C5-E-17_SED_00-01	10/24/2017	FS	1	1	
1711056	SED	OR-T3-C5-E	OR-T3-C5-E-17_SED_01-03	10/24/2017	FS	1	1	
1711056	SED	OR-T3-C5-E	OR-T3-C5-E-17_SED_03-05	10/24/2017	FS	1	1	
1711056	SED	OR-T3-C5-E	OR-T3-C5-E-17_SED_05-07	10/24/2017	FS	1	1	
1711056	SED	OR-T3-C5-E	OR-T3-C5-E-17_SED_07-10	10/24/2017	FS	1	1	
1711057	SED	OR-T3-C4-F	OR-T3-C4-F-17_SED_00-01	10/23/2017	FS	1	1	
1711057	SED	OR-T3-C4-F	OR-T3-C4-F-17_SED_01-03	10/23/2017	FS	1	1	
1711057	SED	OR-T3-C4-F	OR-T3-C4-F-17_SED_03-05	10/23/2017	FS	1	1	
1711057	SED	OR-T3-C4-F	OR-T3-C4-F-17_SED_03-05_DUP	10/23/2017	FD	1	1	
1711057	SED	OR-T3-C4-F	OR-T3-C4-F-17_SED_05-07	10/23/2017	FS	1	1	
1711057	SED	OR-T3-C4-F	OR-T3-C4-F-17_SED_07-10	10/23/2017	FS	1	1	
1711058	SED	OR-T3-C2-F	OR-T3-C2-F-17_SED_00-01	10/23/2017	FS	1	1	
1711058	SED	OR-T3-C2-F	OR-T3-C2-F-17_SED_01-03	10/23/2017	FS	1	1	
1711058	SED	OR-T3-C2-F	OR-T3-C2-F-17_SED_03-05	10/23/2017	FS	1	1	
1711058	SED	OR-T3-C2-F	OR-T3-C2-F-17_SED_03-05_DUP	10/23/2017	FD	1	1	
1711058	SED	OR-T3-C2-F	OR-T3-C2-F-17_SED_05-07	10/23/2017	FS	1	1	
1711059	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_00-01	10/24/2017	FS	1	1	
1711059	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_01-03	10/24/2017	FS	1	1	
1711059	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_03-05	10/24/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1711059	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_05-07	10/24/2017	FS	1	1	
1711059	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_07-10	10/24/2017	FS	1	1	
1711059	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_10-15	10/24/2017	FS	1	1	
1711059	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_15-20	10/24/2017	FS	1	1	
1711059	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_15-20_DUP	10/24/2017	FD	1	1	
1711060	SED	OR-T2-C5-E	OR-T2-C5-E-17_SED_00-01	10/24/2017	FS	1	1	
1711060	SED	OR-T2-C5-E	OR-T2-C5-E-17_SED_01-03	10/24/2017	FS	1	1	
1711060	SED	OR-T2-C5-E	OR-T2-C5-E-17_SED_03-05	10/24/2017	FS	1	1	
1711060	SED	OR-T2-C5-E	OR-T2-C5-E-17_SED_05-07	10/24/2017	FS	1	1	
1711060	SED	OR-T2-C5-E	OR-T2-C5-E-17_SED_07-10	10/24/2017	FS	1	1	
1711061	SED	OR-T2-C4-C	OR-T2-C4-C-17_SED_00-01	10/23/2017	FS	1	1	
1711061	SED	OR-T2-C4-C	OR-T2-C4-C-17_SED_01-03	10/23/2017	FS	1	1	
1711061	SED	OR-T2-C4-C	OR-T2-C4-C-17_SED_03-05	10/23/2017	FS	1	1	
1711061	SED	OR-T2-C4-C	OR-T2-C4-C-17_SED_05-07	10/23/2017	FS	1	1	
1711061	SED	OR-T2-C4-C	OR-T2-C4-C-17_SED_07-10	10/23/2017	FS	1	1	
1711062	SED	PBR-18-I	PBR-18-I-17_SED_00-01	10/20/2017	FS	1	1	
1711062	SED	PBR-18-I	PBR-18-I-17_SED_01-03	10/20/2017	FS	1	1	
1711062	SED	PBR-18-I	PBR-18-I-17_SED_03-05	10/20/2017	FS	1	1	
1711062	SED	PBR-18-I	PBR-18-I-17_SED_05-07	10/20/2017	FS	1	1	
1711063	SED	OR-T2-C3-C	OR-T2-C3-C-17_SED_00-01	10/20/2017	FS	1	1	
1711063	SED	OR-T2-C3-C	OR-T2-C3-C-17_SED_01-03	10/20/2017	FS	1	1	
1711063	SED	OR-T2-C3-C	OR-T2-C3-C-17_SED_03-05	10/20/2017	FS	1	1	
1711063	SED	OR-T2-C3-C	OR-T2-C3-C-17_SED_05-07	10/20/2017	FS	1	1	
1711063	SED	OR-T2-C3-C	OR-T2-C3-C-17_SED_07-10	10/20/2017	FS	1	1	
1711063	SED	OR-T2-C3-C	OR-T2-C3-C-17_SED_07-10_DUP	10/20/2017	FD	1	1	
1711064	SED	OR-T2-C2-E	OR-T2-C2-E-17_SED_00-01	10/20/2017	FS	1	1	
1711064	SED	OR-T2-C2-E	OR-T2-C2-E-17_SED_01-03	10/20/2017	FS	1	1	
1711064	SED	OR-T2-C2-E	OR-T2-C2-E-17_SED_03-05	10/20/2017	FS	1	1	
1711064	SED	OR-T2-C2-E	OR-T2-C2-E-17_SED_05-07	10/20/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1711064	SED	OR-T2-C2-E	OR-T2-C2-E-17_SED_07-10	10/20/2017	FS	1	1	
1711065	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_00-01	10/24/2017	FS	1	1	
1711065	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_01-03	10/24/2017	FS	1	1	
1711065	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_03-05	10/24/2017	FS	1	1	
1711065	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_05-07	10/24/2017	FS	1	1	
1711065	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_05-07_DUP	10/24/2017	FD	1	1	
1711065	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_07-10	10/24/2017	FS	1	1	
1711065	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_10-15	10/24/2017	FS	1	1	
1711065	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_15-20	10/24/2017	FS	1	1	
1711066	SED	OR-T1-C5-C	OR-T1-C5-C-17_SED_00-01	10/23/2017	FS	1	1	
1711066	SED	OR-T1-C5-C	OR-T1-C5-C-17_SED_01-03	10/23/2017	FS	1	1	
1711066	SED	OR-T1-C5-C	OR-T1-C5-C-17_SED_01-03_DUP	10/23/2017	FD	1	1	
1711066	SED	OR-T1-C5-C	OR-T1-C5-C-17_SED_03-05	10/23/2017	FS	1	1	
1711066	SED	OR-T1-C5-C	OR-T1-C5-C-17_SED_05-07	10/23/2017	FS	1	1	
1711066	SED	OR-T1-C5-C	OR-T1-C5-C-17_SED_07-10	10/23/2017	FS	1	1	
1711067	SED	MM-T4-C2-F	MM-T4-C2-F-17_SED_00-01	10/24/2017	FS	1	1	
1711067	SED	MM-T4-C2-F	MM-T4-C2-F-17_SED_01-03	10/24/2017	FS	1	1	
1711067	SED	MM-T4-C2-F	MM-T4-C2-F-17_SED_01-03_DUP	10/24/2017	FD	1	1	
1711067	SED	MM-T4-C2-F	MM-T4-C2-F-17_SED_03-05	10/24/2017	FS	1	1	
1711067	SED	MM-T4-C2-F	MM-T4-C2-F-17_SED_05-07	10/24/2017	FS	1	1	
1711067	SED	MM-T4-C2-F	MM-T4-C2-F-17_SED_07-10	10/24/2017	FS	1	1	
1711068	SED	OR-T1-C3-C	OR-T1-C3-C-17_SED_00-01	10/19/2017	FS	1	1	
1711068	SED	OR-T1-C3-C	OR-T1-C3-C-17_SED_01-03	10/19/2017	FS	1	1	
1711068	SED	OR-T1-C3-C	OR-T1-C3-C-17_SED_03-05	10/19/2017	FS	1	1	
1711068	SED	OR-T1-C3-C	OR-T1-C3-C-17_SED_05-07	10/19/2017	FS	1	1	
1711069	SED	OR-T1-C2-C	OR-T1-C2-C-17_SED_00-01	10/19/2017	FS	1	1	
1711069	SED	OR-T1-C2-C	OR-T1-C2-C-17_SED_01-03	10/19/2017	FS	1	1	
1711069	SED	OR-T1-C2-C	OR-T1-C2-C-17_SED_03-05	10/19/2017	FS	1	1	
1711069	SED	OR-T1-C2-C	OR-T1-C2-C-17_SED_05-07	10/19/2017	FS	1	1	

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TABLE 1
DATA VALIDATION SUMMARY
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1711069	SED	OR-T1-C2-C	OR-T1-C2-C-17_SED_07-10	10/19/2017	FS	1	1	
1711070	SED	MM-T3-C4-C	MM-T3-C4-C-17_SED_00-01	10/24/2017	FS	1	1	
1711070	SED	MM-T3-C4-C	MM-T3-C4-C-17_SED_01-03	10/24/2017	FS	1	1	
1711070	SED	MM-T3-C4-C	MM-T3-C4-C-17_SED_03-05	10/24/2017	FS	1	1	
1711070	SED	MM-T3-C4-C	MM-T3-C4-C-17_SED_05-07	10/24/2017	FS	1	1	
1711070	SED	MM-T3-C4-C	MM-T3-C4-C-17_SED_07-10	10/24/2017	FS	1	1	
1711071	SED	MM-T1-C2-D	MM-T1-C2-D-17_SED_00-01	10/20/2017	FS	1	1	
1711071	SED	MM-T1-C2-D	MM-T1-C2-D-17_SED_01-03	10/20/2017	FS	1	1	
1711071	SED	MM-T1-C2-D	MM-T1-C2-D-17_SED_03-05	10/20/2017	FS	1	1	
1711071	SED	MM-T1-C2-D	MM-T1-C2-D-17_SED_05-07	10/20/2017	FS	1	1	
1711071	SED	MM-T1-C2-D	MM-T1-C2-D-17_SED_05-07_DUP	10/20/2017	FD	1	1	
1711071	SED	MM-T1-C2-D	MM-T1-C2-D-17_SED_07-10	10/20/2017	FS	1	1	
1711073	SED	ES-01-F	ES-01-F-17_SED_00-01	10/20/2017	FS	1	1	
1711073	SED	ES-01-F	ES-01-F-17_SED_01-03	10/20/2017	FS	1	1	
1711073	SED	ES-01-F	ES-01-F-17_SED_01-03_DUP	10/20/2017	FD	1	1	
1711073	SED	ES-01-F	ES-01-F-17_SED_03-05	10/20/2017	FS	1	1	
1711073	SED	ES-01-F	ES-01-F-17_SED_05-07	10/20/2017	FS	1	1	
1711077	SED	ES-18-F	ES-18-F-17_SED_00-01	10/23/2017	FS	1	1	
1711077	SED	ES-18-F	ES-18-F-17_SED_01-03	10/23/2017	FS	1	1	
1711077	SED	ES-18-F	ES-18-F-17_SED_03-05	10/23/2017	FS	1	1	
1711077	SED	ES-18-F	ES-18-F-17_SED_05-07	10/23/2017	FS	1	1	
1711083	SED	MM-T3-C2-F	MM-T3-C2-F-17_SED_00-01	10/20/2017	FS	1	1	
1711083	SED	MM-T3-C2-F	MM-T3-C2-F-17_SED_01-03	10/20/2017	FS	1	1	
1711083	SED	MM-T3-C2-F	MM-T3-C2-F-17_SED_03-05	10/20/2017	FS	1	1	
1711083	SED	MM-T3-C2-F	MM-T3-C2-F-17_SED_05-07	10/20/2017	FS	1	1	
1711084	SED	MM-T3-C3-C	MM-T3-C3-C-17_SED_00-01	10/19/2017	FS	1	1	
1711084	SED	MM-T3-C3-C	MM-T3-C3-C-17_SED_01-03	10/19/2017	FS	1	1	
1711084	SED	MM-T3-C3-C	MM-T3-C3-C-17_SED_03-05	10/19/2017	FS	1	1	
1711085	SED	MM-T2-C8-B	MM-T2-C8-B-17_SED_00-01	10/24/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1711085	SED	MM-T2-C8-B	MM-T2-C8-B-17_SED_01-03	10/24/2017	FS	1	1	
1711085	SED	MM-T2-C8-B	MM-T2-C8-B-17_SED_03-05	10/24/2017	FS	1	1	
1711085	SED	MM-T2-C8-B	MM-T2-C8-B-17_SED_05-07	10/24/2017	FS	1	1	
1711085	SED	MM-T2-C8-B	MM-T2-C8-B-17_SED_07-10	10/24/2017	FS	1	1	
1711151	SED	PBR-28	PBR-28-17_SED_00-01	11/1/2017	FS	1	1	
1711151	SED	PBR-28	PBR-28-17_SED_01-03	11/1/2017	FS	1	1	
1711151	SED	PBR-28	PBR-28-17_SED_03-05	11/1/2017	FS	1	1	
1711151	SED	PBR-28	PBR-28-17_SED_05-07	11/1/2017	FS	1	1	
1711151	SED	PBR-28	PBR-28-17_SED_05-07_DUP	11/1/2017	FD	1	1	
1711151	SED	PBR-28	PBR-28-17_SED_07-10	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_000-001CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_001-002CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_002-003CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_003-004CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_004-005CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_005-006CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_006-007CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_007-008CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_008-009CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_009-010CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_010-011CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_011-012CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_012-013CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_013-014CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_014-015CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_015-016CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_016-017CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_017-018CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_018-019CM	11/1/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_019-020CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_020-022CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_022-024CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_024-026CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_026-028CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_028-030CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_030-032CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_032-034CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_034-036CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_036-038CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_038-040CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_040-045CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_045-050CM	11/1/2017	FS	1	1	
1711156	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_050-055CM	11/1/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_000-001CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_001-002CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_002-003CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_003-004CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_004-005CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_005-006CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_006-007CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_007-008CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_008-009CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_009-010CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_010-011CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_011-012CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_012-013CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_013-014CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_014-015CM	10/31/2017	FS	1	1	

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_015-016CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_016-017CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_017-018CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_018-019CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_019-020CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_020-022CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_022-024CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_024-026CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_026-028CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_028-030CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_030-032CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_032-034CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_034-036CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_036-038CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_038-040CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_040-045CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_045-050CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_050-055CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_055-060CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_060-065CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_065-070CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_070-075CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_075-080CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_080-085CM	10/31/2017	FS	1	1	
1711171	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_085-090CM	10/31/2017	FS	1	1	
1711173	SED	OR-T1-C1-D	OR-T1-C1-D-17_SED_00-01	11/1/2017	FS	1	1	
1711173	SED	OR-T1-C1-D	OR-T1-C1-D-17_SED_01-03	11/1/2017	FS	1	1	
1711173	SED	OR-T1-C1-D	OR-T1-C1-D-17_SED_03-05	11/1/2017	FS	1	1	
1711173	SED	OR-T1-C1-D	OR-T1-C1-D-17_SED_05-07	11/1/2017	FS	1	1	

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SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1711173	SED	OR-T1-C1-D	OR-T1-C1-D-17_SED_07-10	11/1/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_000-001CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_000-001CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_001-002CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_001-002CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_002-003CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_003-004CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_003-004CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_004-005CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_004-005CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_005-006CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_005-006CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_006-007CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_006-007CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_007-008CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_007-008CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_008-009CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_008-009CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_009-010CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_009-010CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_010-011CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_010-011CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_011-012CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_011-012CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_012-013CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_012-013CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_013-014CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_013-014CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_014-015CM	10/31/2017	FS	1	1	

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_014-015CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_015-016CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_015-016CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_016-017CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_016-017CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_017-018CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_017-018CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_018-019CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_018-019CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_019-020CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_019-020CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_020-022CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_020-022CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_022-024CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_022-024CM_DUP	10/31/2017	FD	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_024-026CM	10/31/2017	FS	1	1	
1711174	SED	MM-T3-C1	MM-T3-C1-17_SED_024-026CM_DUP	10/31/2017	FD	1	1	
1711328	SED	MM-T1-C1-B	MM-T1-C1-B-17_SED_00-01	11/1/2017	FS	1	1	
1711328	SED	MM-T1-C1-B	MM-T1-C1-B-17_SED_01-03	11/1/2017	FS	1	1	
1711328	SED	MM-T1-C1-B	MM-T1-C1-B-17_SED_03-05	11/1/2017	FS	1	1	
1711328	SED	MM-T1-C1-B	MM-T1-C1-B-17_SED_03-05-Dup	11/1/2017	FD	1	1	
1711328	SED	MM-T1-C1-B	MM-T1-C1-B-17_SED_05-07	11/1/2017	FS	1	1	
1711328	SED	MM-T1-C1-B	MM-T1-C1-B-17_SED_07-10	11/1/2017	FS	1	1	
1712044	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_022-024CM	10/16/2017	FS	1	1	
1712044	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_022-024CM_DUP	10/16/2017	FD	1	1	
1712045	SED	MM-T4-C7	MM-T4-C7-17_SED_045-050CM	10/16/2017	FS	1	1	
1712045	SED	MM-T4-C7	MM-T4-C7-17_SED_045-050CM_DUP	10/16/2017	FD	1	1	
1712045	SED	MM-T4-C7	MM-T4-C7-17_SED_055-060CM	10/16/2017	FS	1	1	
1712045	SED	MM-T4-C7	MM-T4-C7-17_SED_055-060CM_DUP	10/16/2017	FD	1	1	

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TABLE 1
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
1712047	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_050-055CM	10/17/2017	FS	1	1	
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_000-001CM	9/12/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_001-002CM	9/12/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_002-003CM	9/12/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_003-004CM	9/12/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_004-005CM	9/12/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_005-006CM	9/12/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_006-007CM	9/12/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_007-008CM	9/12/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_008-009CM	9/12/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_009-010CM	9/12/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_010-011CM	9/12/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_011-012CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_012-013CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_013-014CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_014-015CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_015-016CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_016-017CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_017-018CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_018-019CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_019-020CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_020-022CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_022-024CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_024-026CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_026-028CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_028-030CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_030-032CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_032-034CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_034-036CM	9/13/2017	FS	1		3

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TABLE 1
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_036-038CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_038-040CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_040-045CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_045-050CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_050-055CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_055-060CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_060-065CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_065-070CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_070-075CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_075-080CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_080-085CM	9/13/2017	FS	1		3
L1732774	SED	MM-T3-C2-C	MM-T3-C2-C-17_SED_085-090CM	9/13/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_000-001CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_001-002CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_002-003CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_003-004CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_004-005CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_005-006CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_006-007CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_007-008CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_008-009CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_009-010CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_010-011CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_011-012CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_012-013CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_013-014CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_014-015CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_015-016CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_016-017CM	9/14/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_017-018CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_018-019CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_019-020CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_020-022CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_022-024CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_024-026CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_026-028CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_028-030CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_030-032CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_032-034CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_034-036CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_036-038CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_038-040CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_040-045CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_045-050CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_050-055CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_055-060CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_060-065CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_065-070CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_070-075CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_075-080CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_080-085CM	9/14/2017	FS	1		3
L1733612	SED	OR-T1-C4-C	OR-T1-C4-C-17_SED_085-090CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_000-001CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_001-002CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_002-003CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_003-004CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_004-005CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_005-006CM	9/13/2017	FS	1		3

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TABLE 1
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_006-007CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_007-008CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_008-009CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_009-010CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_010-011CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_011-012CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_012-013CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_013-014CM	9/13/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_014-015CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_015-016CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_016-017CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_017-018CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_018-019CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_019-020CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_020-022CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_022-024CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_024-026CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_026-028CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_028-030CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_030-032CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_032-034CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_034-036CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_036-038CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_038-040CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_040-045CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_045-050CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_050-055CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_055-060CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_060-065CM	9/14/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_065-070CM	9/14/2017	FS	1		3
L1733618	SED	MM-T1-C3-B	MM-T1-C3-B-17_SED_070-075CM	9/14/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_000-001CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_001-002CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_002-003CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_003-004CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_004-005CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_005-006CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_006-007CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_007-008CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_008-009CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_009-010CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_010-011CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_011-012CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_012-013CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_013-014CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_014-015CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_015-016CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_016-017CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_017-018CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_018-019CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_019-020CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_020-022CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_022-024CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_024-026CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_026-028CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_028-030CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_030-032CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_032-034CM	9/15/2017	FS	1		3

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DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_034-036CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_036-038CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_038-040CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_040-045CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_045-050CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_050-055CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_055-060CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_060-065CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_065-070CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_070-075CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_075-080CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_080-085CM	9/15/2017	FS	1		3
L1733619	SED	MM-T2-C4-B	MM-T2-C4-B-17_SED_085-090CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_000-001CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_001-002CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_002-003CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_003-004CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_004-005CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_005-006CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_006-007CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_007-008CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_008-009CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_009-010CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_010-011CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_011-012CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_012-013CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_013-014CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_014-015CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_015-016CM	9/15/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_016-017CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_017-018CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_018-019CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_019-020CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_020-022CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_022-024CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_024-026CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_026-028CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_028-030CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_030-032CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_032-034CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_034-036CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_036-038CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_038-040CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_040-045CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_045-050CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_050-055CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_055-060CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_060-065CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_065-070CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_070-075CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_075-080CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_080-085CM	9/15/2017	FS	1		3
L1733620	SED	MM-T2-C5-A	MM-T2-C5-A-17_SED_085-090CM	9/15/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_000-001CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_001-002CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_002-003CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_003-004CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_004-005CM	9/18/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_005-006CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_006-007CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_007-008CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_008-009CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_009-010CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_010-011CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_011-012CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_012-013CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_013-014CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_014-015CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_015-016CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_016-017CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_017-018CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_018-019CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_019-020CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_020-022CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_022-024CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_024-026CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_026-028CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_028-030CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_030-032CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_032-034CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_034-036CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_036-038CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_038-040CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_040-045CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_045-050CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_050-055CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_055-060CM	9/18/2017	FS	1		3

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_060-065CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_065-070CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_070-075CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_075-080CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_080-085CM	9/18/2017	FS	1		3
L1733621	SED	MM-T2-C6-A	MM-T2-C6-A-17_SED_085-090CM	9/18/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_000-001CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_001-002CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_002-003CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_003-004CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_004-005CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_005-006CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_006-007CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_007-008CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_008-009CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_009-010CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_010-011CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_011-012CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_012-013CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_013-014CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_014-015CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_015-016CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_016-017CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_017-018CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_018-019CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_019-020CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_020-022CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_022-024CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_024-026CM	10/3/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_026-028CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_028-030CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_030-032CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_032-034CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_034-036CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_036-038CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_038-040CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_040-045CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_045-050CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_050-055CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_055-060CM	10/3/2017	FS	1		3
L1736451	SED	MM-T1-C2-B	MM-T1-C2-B-17_SED_060-065CM	10/3/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_000-001CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_001-002CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_002-003CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_003-004CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_004-005CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_005-006CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_006-007CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_007-008CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_008-009CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_009-010CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_010-011CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_011-012CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_012-013CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_013-014CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_014-015CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_015-016CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_016-017CM	9/28/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_017-018CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_018-019CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_019-020CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_020-022CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_022-024CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_024-026CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_026-028CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_028-030CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_030-032CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_032-034CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_034-036CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_036-038CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_038-040CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_040-045CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_045-050CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_050-055CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_055-060CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_060-065CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_065-070CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_070-075CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_075-080CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_080-085CM	9/28/2017	FS	1		3
L1736453	SED	OR-T1-C2-B	OR-T1-C2-B-17_SED_085-090CM	9/28/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_000-001CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_001-002CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_002-003CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_003-004CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_004-005CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_005-006CM	9/29/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_006-007CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_007-008CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_008-009CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_009-010CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_010-011CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_011-012CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_012-013CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_013-014CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_014-015CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_015-016CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_016-017CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_017-018CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_018-019CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_019-020CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_020-022CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_022-024CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_024-026CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_026-028CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_028-030CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_030-032CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_032-034CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_034-036CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_036-038CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_038-040CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_040-045CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_045-050CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_050-055CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_055-060CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_060-065CM	9/29/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_065-070CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_070-075CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_075-080CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_080-085CM	9/29/2017	FS	1		3
L1736454	SED	OR-T1-C5-A	OR-T1-C5-A-17_SED_085-090CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_000-001CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_001-002CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_002-003CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_003-004CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_004-005CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_005-006CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_006-007CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_007-008CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_008-009CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_009-010CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_010-011CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_011-012CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_012-013CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_013-014CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_014-015CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_015-016CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_016-017CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_017-018CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_018-019CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_019-020CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_020-022CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_022-024CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_024-026CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_026-028CM	9/29/2017	FS	1		3

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_028-030CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_030-032CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_032-034CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_034-036CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_036-038CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_038-040CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_040-045CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_045-050CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_050-055CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_055-060CM	9/29/2017	FS	1		3
L1736455	SED	OR-T2-C1-C	OR-T2-C1-C-17_SED_060-065CM	9/29/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_000-001CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_001-002CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_002-003CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_003-004CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_004-005CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_005-006CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_006-007CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_007-008CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_008-009CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_009-010CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_010-011CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_011-012CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_012-013CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_013-014CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_014-015CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_015-016CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_016-017CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_017-018CM	10/3/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_018-019CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_019-020CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_020-022CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_022-024CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_024-026CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_026-028CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_028-030CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_030-032CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_032-034CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_034-036CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_036-038CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_038-040CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_040-045CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_045-050CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_050-055CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_055-060CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_060-065CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_065-070CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_070-075CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_075-080CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_080-085CM	10/3/2017	FS	1		3
L1736456	SED	OR-T2-C4-A	OR-T2-C4-A-17_SED_085-090CM	10/3/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_000-001CM	9/29/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_001-002CM	9/29/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_002-003CM	9/29/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_003-004CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_004-005CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_005-006CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_006-007CM	10/2/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_007-008CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_008-009CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_009-010CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_010-011CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_011-012CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_012-013CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_013-014CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_014-015CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_015-016CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_016-017CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_017-018CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_018-019CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_019-020CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_020-022CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_022-024CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_024-026CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_026-028CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_028-030CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_030-032CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_032-034CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_034-036CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_036-038CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_038-040CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_040-045CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_045-050CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_050-055CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_055-060CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_060-065CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_065-070CM	10/2/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_070-075CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_075-080CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_080-085CM	10/2/2017	FS	1		3
L1736458	SED	OR-T3-C3-B	OR-T3-C3-B-17_SED_085-090CM	10/2/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_000-001CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_001-002CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_002-003CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_003-004CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_004-005CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_005-006CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_006-007CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_007-008CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_008-009CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_009-010CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_010-011CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_011-012CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_012-013CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_013-014CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_014-015CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_015-016CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_016-017CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_017-018CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_018-019CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_019-020CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_020-022CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_022-024CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_024-026CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_026-028CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_028-030CM	10/6/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_030-032CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_032-034CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_034-036CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_036-038CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_038-040CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_040-045CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_045-050CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_050-055CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_055-060CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_060-065CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_065-070CM	10/6/2017	FS	1		3
L1737040	SED	MM-C1-C	MM-C1-C-17_SED_070-075CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_000-001CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_001-002CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_002-003CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_003-004CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_004-005CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_005-006CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_006-007CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_007-008CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_008-009CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_009-010CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_010-011CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_011-012CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_012-013CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_013-014CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_014-015CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_015-016CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_016-017CM	10/6/2017	FS	1		3

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TABLE 1
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_017-018CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_018-019CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_019-020CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_020-022CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_022-024CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_024-026CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_026-028CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_028-030CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_030-032CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_032-034CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_034-036CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_036-038CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_038-040CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_040-045CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_045-050CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_050-055CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_055-060CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_060-065CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_065-070CM	10/6/2017	FS	1		3
L1737041	SED	MM-T1-C1-A	MM-T1-C1-A-17_SED_070-075CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_000-001CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_001-002CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_002-003CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_003-004CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_004-005CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_005-006CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_006-007CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_007-008CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_008-009CM	10/6/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_009-010CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_010-011CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_011-012CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_012-013CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_013-014CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_014-015CM	10/6/2017	FS			3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_015-016CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_016-017CM	10/6/2017	FS			3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_017-018CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_018-019CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_019-020CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_020-022CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_022-024CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_024-026CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_026-028CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_028-030CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_030-032CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_032-034CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_034-036CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_036-038CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_038-040CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_040-045CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_045-050CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_050-055CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_055-060CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_060-065CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_065-070CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_070-075CM	10/6/2017	FS	1		3
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_075-080CM	10/6/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1737042	SED	MM-T1-C4	MM-T1-C4-17_SED_080-085CM	10/6/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_000-001CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_001-002CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_002-003CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_003-004CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_004-005CM	10/9/2017	FS			3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_005-006CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_006-007CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_007-008CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_008-009CM	10/9/2017	FS			3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_009-010CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_010-011CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_011-012CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_012-013CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_013-014CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_014-015CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_015-016CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_016-017CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_017-018CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_018-019CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_019-020CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_020-022CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_022-024CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_024-026CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_026-028CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_028-030CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_030-032CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_032-034CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_034-036CM	10/9/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_036-038CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_038-040CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_040-045CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_045-050CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_050-055CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_055-060CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_060-065CM	10/9/2017	FS	1		3
L1737043	SED	MM-T1-C5	MM-T1-C5-A-17_SED_065-070CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_000-001CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_001-002CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_002-003CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_003-004CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_004-005CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_005-006CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_006-007CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_007-008CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_008-009CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_009-010CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_010-011CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_011-012CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_012-013CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_013-014CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_014-015CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_015-016CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_016-017CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_017-018CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_018-019CM	10/9/2017	FS			3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_019-020CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_020-022CM	10/9/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_022-024CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_024-026CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_026-028CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_028-030CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_030-032CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_032-034CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_034-036CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_036-038CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_038-040CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_040-045CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_045-050CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_050-055CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_055-060CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_060-065CM	10/9/2017	FS	1		3
L1737044	SED	MM-T1-C6	MM-T1-C6-A-17_SED_065-070CM	10/9/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_000-001CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_001-002CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_002-003CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_003-004CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_004-005CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_005-006CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_006-007CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_007-008CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_008-009CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_009-010CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_010-011CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_011-012CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_012-013CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_013-014CM	10/4/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_014-015CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_015-016CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_016-017CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_017-018CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_018-019CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_019-020CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_020-022CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_022-024CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_024-026CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_026-028CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_028-030CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_030-032CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_032-034CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_034-036CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_036-038CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_038-040CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_040-045CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_045-050CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_050-055CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_055-060CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_060-065CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_065-070CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_070-075CM	10/4/2017	FS	1		3
L1737045	SED	MM-T3-C3-B2	MM-T3-C3-B2-17_SED_075-080CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_000-001CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_001-002CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_002-003CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_003-004CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_004-005CM	10/4/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_005-006CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_006-007CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_007-008CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_008-009CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_009-010CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_010-011CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_011-012CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_012-013CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_013-014CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_014-015CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_015-016CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_016-017CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_017-018CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_018-019CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_019-020CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_020-022CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_022-024CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_024-026CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_026-028CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_028-030CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_030-032CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_032-034CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_034-036CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_036-038CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_038-040CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_040-045CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_045-050CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_050-055CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_055-060CM	10/4/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_060-065CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_065-070CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_070-075CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_075-080CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_080-085CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_085-090CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_090-095CM	10/4/2017	FS	1		3
L1737046	SED	OR-T1-C3-A	OR-T1-C3-A-17_SED_095-101CM	10/4/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_000-001CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_001-002CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_002-003CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_003-004CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_004-005CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_005-006CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_006-007CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_007-008CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_008-009CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_009-010CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_010-011CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_011-012CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_012-013CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_013-014CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_014-015CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_015-016CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_016-017CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_017-018CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_018-019CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_019-020CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_020-022CM	10/3/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_022-024CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_024-026CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_026-028CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_028-030CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_030-032CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_032-034CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_034-036CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_036-038CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_038-040CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_040-045CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_045-050CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_050-055CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_055-060CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_060-065CM	10/3/2017	FS	1		3
L1737047	SED	OR-T2-C3-B	OR-T2-C3-B-17_SED_065-070CM	10/3/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_000-001CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_001-002CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_002-003CM	10/10/2017	FS			3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_003-004CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_004-005CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_005-006CM	10/10/2017	FS			3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_006-007CM	10/10/2017	FS			3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_007-008CM	10/10/2017	FS			3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_008-009CM	10/10/2017	FS			3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_010-011CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_011-012CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_012-013CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_013-014CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_014-015CM	10/10/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_015-016CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_016-017CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_017-018CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_018-019CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_019-020CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_020-022CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_022-024CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_024-026CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_026-028CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_028-030CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_030-032CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_032-034CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_034-036CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_036-038CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_038-040CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_040-045CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_045-050CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_050-055CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_055-060CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_060-065CM	10/10/2017	FS	1		3
L1738093	SED	MM-T3-C6	MM-T3-C6-17_SED_065-070CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_000-001CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_001-002CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_002-003CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_003-004CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_004-005CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_005-006CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_006-007CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_007-008CM	10/10/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_008-009CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_009-010CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_010-011CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_011-012CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_012-013CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_013-014CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_014-015CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_015-016CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_016-017CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_017-018CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_018-019CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_019-020CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_020-022CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_022-024CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_024-026CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_026-028CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_028-030CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_030-032CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_032-034CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_034-036CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_036-038CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_038-040CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_040-045CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_045-050CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_050-055CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_055-060CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_060-065CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_065-070CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_070-075CM	10/10/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_075-080CM	10/10/2017	FS	1		3
L1738103	SED	MM-T4-C1	MM-T4-C1-17_SED_080-085CM	10/10/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_000-001CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_001-002CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_002-003CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_003-004CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_004-005CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_005-006CM	10/11/2017	FS			3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_006-007CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_007-008CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_008-009CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_009-010CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_010-011CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_011-012CM	10/11/2017	FS			3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_012-013CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_013-014CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_014-015CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_015-016CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_016-017CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_017-018CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_018-019CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_019-020CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_020-022CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_022-024CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_024-026CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_026-028CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_028-030CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_030-032CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_032-034CM	10/11/2017	FS	1		3

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TABLE 1
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_034-036CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_036-038CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_038-040CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_040-045CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_045-050CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_050-055CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_055-060CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_060-065CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_065-070CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_070-075CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_075-080CM	10/11/2017	FS	1		3
L1738104	SED	MM-T4-C5	MM-T4-C5-17_SED_080-085CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_000-001CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_001-002CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_002-003CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_003-004CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_004-005CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_005-006CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_006-007CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_007-008CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_008-009CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_009-010CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_010-011CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_011-012CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_012-013CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_013-014CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_014-015CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_015-016CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_016-017CM	10/11/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_017-018CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_018-019CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_019-020CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_020-022CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_022-024CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_024-026CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_026-028CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_028-030CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_030-032CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_032-034CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_034-036CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_036-038CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_038-040CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_040-045CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_045-050CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_050-055CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_055-060CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_060-065CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_065-070CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_070-075CM	10/11/2017	FS	1		3
L1738105	SED	MM-T4-C6	MM-T4-C6-17_SED_075-080CM	10/11/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_000-001CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_001-002CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_002-003CM	10/13/2017	FS			3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_003-004CM	10/13/2017	FS			3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_004-005CM	10/13/2017	FS			3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_005-006CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_006-007CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_007-008CM	10/13/2017	FS	1		3

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TABLE 1
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_008-009CM	10/13/2017	FS			3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_009-010CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_010-011CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_011-012CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_012-013CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_013-014CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_014-015CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_015-016CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_016-017CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_017-018CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_018-019CM	10/13/2017	FS			3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_020-022CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_022-024CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_024-026CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_026-028CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_028-030CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_030-032CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_032-034CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_034-036CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_036-038CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_038-040CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_040-045CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_045-050CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_050-055CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_055-060CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_060-065CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_065-070CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_070-075CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_075-080CM	10/13/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_080-085CM	10/13/2017	FS	1		3
L1738106	SED	MM-T5-C1	MM-T5-C1-17_SED_085-090CM	10/13/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_000-001CM	10/12/2017	FS			3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_001-002CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_002-003CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_003-004CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_004-005CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_005-006CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_006-007CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_007-008CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_008-009CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_009-010CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_010-011CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_011-012CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_012-013CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_013-014CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_014-015CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_015-016CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_016-017CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_017-018CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_018-019CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_019-020CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_020-022CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_022-024CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_024-026CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_026-028CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_028-030CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_030-032CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_032-034CM	10/12/2017	FS	1		3

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_034-036CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_036-038CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_038-040CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_040-045CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_045-050CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_050-055CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_055-060CM	10/12/2017	FS	1		3
L1738128	SED	MM-T5-C2	MM-T5-C2-17_SED_060-065CM	10/12/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_000-001CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_001-002CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_002-003CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_003-004CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_004-005CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_005-006CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_006-007CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_007-008CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_008-009CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_009-010CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_010-011CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_011-012CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_012-013CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_013-014CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_014-015CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_015-016CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_016-017CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_017-018CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_018-019CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_019-020CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_020-022CM	10/16/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_022-024CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_024-026CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_026-028CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_028-030CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_030-032CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_032-034CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_034-036CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_036-038CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_038-040CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_040-045CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_045-050CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_050-055CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_055-060CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_060-065CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_065-070CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_070-075CM	10/16/2017	FS	1		3
L1739120	SED	MM-T3-C4-D	MM-T3-C4-D-17_SED_075-080CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_000-001CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_001-002CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_002-003CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_003-004CM	10/16/2017	FS			3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_004-005CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_005-006CM	10/16/2017	FS			3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_006-007CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_008-009CM	10/16/2017	FS			3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_009-010CM	10/16/2017	FS			3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_010-011CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_011-012CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_012-013CM	10/16/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_013-014CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_014-015CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_015-016CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_016-017CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_017-018CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_018-019CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_019-020CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_020-022CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_022-024CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_024-026CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_026-028CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_028-030CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_030-032CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_032-034CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_034-036CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_036-038CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_038-040CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_040-045CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_045-050CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_050-055CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_055-060CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_060-065CM	10/16/2017	FS	1		3
L1739121	SED	MM-T3-C7	MM-T3-C7-17_SED_065-070CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_000-001CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_001-002CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_002-003CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_003-004CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_004-005CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_005-006CM	10/16/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_006-007CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_007-008CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_008-009CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_009-010CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_010-011CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_011-012CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_012-013CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_013-014CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_014-015CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_015-016CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_016-017CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_017-018CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_018-019CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_019-020CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_020-022CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_022-024CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_024-026CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_026-028CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_028-030CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_030-032CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_032-034CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_034-036CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_036-038CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_038-040CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_040-045CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_045-050CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_050-055CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_055-060CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_060-065CM	10/16/2017	FS	1		3

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TABLE 1
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_065-070CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_070-075CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_075-080CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_080-085CM	10/16/2017	FS	1		3
L1739122	SED	MM-T4-C7	MM-T4-C7-17_SED_085-090CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_000-001CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_001-002CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_002-003CM	10/13/2017	FS			3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_003-004CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_004-005CM	10/13/2017	FS			3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_005-006CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_006-007CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_007-008CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_008-009CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_009-010CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_010-011CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_011-012CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_012-013CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_013-014CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_014-015CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_015-016CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_016-017CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_017-018CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_018-019CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_019-020CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_020-022CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_022-024CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_024-026CM	10/13/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_026-028CM	10/13/2017	FS	1		3

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_028-030CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_030-032CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_032-034CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_034-036CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_036-038CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_038-040CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_040-045CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_045-050CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_050-055CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_055-060CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_060-065CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_065-070CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_070-075CM	10/16/2017	FS	1		3
L1739123	SED	MM-T5-C3	MM-T5-C3-17_SED_075-080CM	10/16/2017	FS	1		3
L1739124	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_00-01	10/16/2017	FS	1		3
L1739124	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_01-03	10/16/2017	FS	1		3
L1739124	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_03-05	10/16/2017	FS	1		3
L1739124	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_05-07	10/16/2017	FS	1		3
L1739124	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_07-10	10/16/2017	FS	1		3
L1739124	SED	VN-MU3-GC-1-G	VN-MU3-GC-1-G-17_SED_10-15	10/16/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_000-001CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_001-002CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_002-003CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_003-004CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_004-005CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_005-006CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_006-007CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_007-008CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_008-009CM	10/17/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_009-010CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_010-011CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_011-012CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_012-013CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_013-014CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_014-015CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_015-016CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_016-017CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_017-018CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_018-019CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_019-020CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_020-022CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_022-024CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_024-026CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_026-028CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_028-030CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_030-032CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_032-034CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_034-036CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_036-038CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_038-040CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_040-045CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_045-050CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_050-055CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_055-060CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_060-065CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_065-070CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_070-075CM	10/17/2017	FS	1		3
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_075-080CM	10/17/2017	FS	1		3

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739127	SED	OR-T3-C4-A	OR-T3-C4-A-17_SED_080-085CM	10/17/2017	FS	1		3
L1739536	SED	ES-01-F	ES-01-F-17_SED_00-01	10/20/2017	FS	1		3
L1739536	SED	ES-01-F	ES-01-F-17_SED_01-03	10/20/2017	FS	1		3
L1739536	SED	ES-01-F	ES-01-F-17_SED_03-05	10/20/2017	FS	1		3
L1739536	SED	ES-01-F	ES-01-F-17_SED_05-07	10/20/2017	FS	1		3
L1739537	SED	ES-18-F	ES-18-F-17_SED_00-01	10/23/2017	FS	1		3
L1739537	SED	ES-18-F	ES-18-F-17_SED_01-03	10/23/2017	FS	1		3
L1739537	SED	ES-18-F	ES-18-F-17_SED_03-05	10/23/2017	FS	1		3
L1739537	SED	ES-18-F	ES-18-F-17_SED_05-07	10/23/2017	FS	1		3
L1739540	SED	MM-T1-C2-D	MM-T1-C2-D-17_SED_00-01	10/20/2017	FS	1		3
L1739540	SED	MM-T1-C2-D	MM-T1-C2-D-17_SED_01-03	10/20/2017	FS	1		3
L1739540	SED	MM-T1-C2-D	MM-T1-C2-D-17_SED_03-05	10/20/2017	FS	1		3
L1739540	SED	MM-T1-C2-D	MM-T1-C2-D-17_SED_05-07	10/20/2017	FS	1		3
L1739540	SED	MM-T1-C2-D	MM-T1-C2-D-17_SED_07-10	10/20/2017	FS	1		3
L1739541	SED	MM-T2-C8-B	MM-T2-C8-B-17_SED_00-01	10/24/2017	FS	1		3
L1739541	SED	MM-T2-C8-B	MM-T2-C8-B-17_SED_01-03	10/24/2017	FS	1		3
L1739541	SED	MM-T2-C8-B	MM-T2-C8-B-17_SED_03-05	10/24/2017	FS	1		3
L1739541	SED	MM-T2-C8-B	MM-T2-C8-B-17_SED_05-07	10/24/2017	FS	1		3
L1739541	SED	MM-T2-C8-B	MM-T2-C8-B-17_SED_07-10	10/24/2017	FS	1		3
L1739542	SED	MM-T3-C2-F	MM-T3-C2-F-17_SED_00-01	10/20/2017	FS	1		3
L1739542	SED	MM-T3-C2-F	MM-T3-C2-F-17_SED_01-03	10/20/2017	FS	1		3
L1739542	SED	MM-T3-C2-F	MM-T3-C2-F-17_SED_03-05	10/20/2017	FS	1		3
L1739542	SED	MM-T3-C2-F	MM-T3-C2-F-17_SED_05-07	10/20/2017	FS	1		3
L1739572	SED	MM-T3-C3-C	MM-T3-C3-C-17_SED_00-01	10/19/2017	FS	1		3
L1739572	SED	MM-T3-C3-C	MM-T3-C3-C-17_SED_01-03	10/19/2017	FS	1		3
L1739572	SED	MM-T3-C3-C	MM-T3-C3-C-17_SED_03-05	10/19/2017	FS	1		3
L1739573	SED	MM-T4-C2-F	MM-T4-C2-F-17_SED_00-01	10/24/2017	FS	1		3
L1739573	SED	MM-T4-C2-F	MM-T4-C2-F-17_SED_01-03	10/24/2017	FS	1		3
L1739573	SED	MM-T4-C2-F	MM-T4-C2-F-17_SED_03-05	10/24/2017	FS	1		3

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739573	SED	MM-T4-C2-F	MM-T4-C2-F-17_SED_05-07	10/24/2017	FS	1		3
L1739573	SED	MM-T4-C2-F	MM-T4-C2-F-17_SED_07-10	10/24/2017	FS	1		3
L1739577	SED	OR-T1-C2-C	OR-T1-C2-C-17_SED_00-01	10/19/2017	FS	1		3
L1739577	SED	OR-T1-C2-C	OR-T1-C2-C-17_SED_01-03	10/19/2017	FS	1		3
L1739577	SED	OR-T1-C2-C	OR-T1-C2-C-17_SED_03-05	10/19/2017	FS	1		3
L1739577	SED	OR-T1-C2-C	OR-T1-C2-C-17_SED_05-07	10/19/2017	FS	1		3
L1739577	SED	OR-T1-C2-C	OR-T1-C2-C-17_SED_07-10	10/19/2017	FS	1		3
L1739578	SED	OR-T1-C3-C	OR-T1-C3-C-17_SED_00-01	10/19/2017	FS	1		3
L1739578	SED	OR-T1-C3-C	OR-T1-C3-C-17_SED_01-03	10/19/2017	FS	1		3
L1739578	SED	OR-T1-C3-C	OR-T1-C3-C-17_SED_03-05	10/19/2017	FS	1		3
L1739578	SED	OR-T1-C3-C	OR-T1-C3-C-17_SED_05-07	10/19/2017	FS	1		3
L1739579	SED	OR-T1-C5-C	OR-T1-C5-C-17_SED_00-01	10/23/2017	FS	1		3
L1739579	SED	OR-T1-C5-C	OR-T1-C5-C-17_SED_01-03	10/23/2017	FS	1		3
L1739579	SED	OR-T1-C5-C	OR-T1-C5-C-17_SED_03-05	10/23/2017	FS	1		3
L1739579	SED	OR-T1-C5-C	OR-T1-C5-C-17_SED_05-07	10/23/2017	FS	1		3
L1739579	SED	OR-T1-C5-C	OR-T1-C5-C-17_SED_07-10	10/23/2017	FS	1		3
L1739580	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_00-01	10/24/2017	FS	1		3
L1739580	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_01-03	10/24/2017	FS	1		3
L1739580	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_03-05	10/24/2017	FS	1		3
L1739580	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_05-07	10/24/2017	FS	1		3
L1739580	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_07-10	10/24/2017	FS	1		3
L1739580	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_10-15	10/24/2017	FS	1		3
L1739580	SED	OR-T2-C1-D	OR-T2-C1-D-17_SED_15-20	10/24/2017	FS	1		3
L1739581	SED	OR-T2-C2-E	OR-T2-C2-E-17_SED_00-01	10/20/2017	FS	1		3
L1739581	SED	OR-T2-C2-E	OR-T2-C2-E-17_SED_01-03	10/20/2017	FS	1		3
L1739581	SED	OR-T2-C2-E	OR-T2-C2-E-17_SED_03-05	10/20/2017	FS	1		3
L1739581	SED	OR-T2-C2-E	OR-T2-C2-E-17_SED_05-07	10/20/2017	FS	1		3
L1739581	SED	OR-T2-C2-E	OR-T2-C2-E-17_SED_07-10	10/20/2017	FS	1		3
L1739593	SED	OR-T2-C3-C	OR-T2-C3-C-17_SED_00-01	10/20/2017	FS	1		3

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739593	SED	OR-T2-C3-C	OR-T2-C3-C-17_SED_01-03	10/20/2017	FS	1		3
L1739593	SED	OR-T2-C3-C	OR-T2-C3-C-17_SED_03-05	10/20/2017	FS	1		3
L1739593	SED	OR-T2-C3-C	OR-T2-C3-C-17_SED_05-07	10/20/2017	FS	1		3
L1739593	SED	OR-T2-C3-C	OR-T2-C3-C-17_SED_07-10	10/20/2017	FS	1		3
L1739594	SED	OR-T2-C4-C	OR-T2-C4-C-17_SED_00-01	10/23/2017	FS	1		3
L1739594	SED	OR-T2-C4-C	OR-T2-C4-C-17_SED_01-03	10/23/2017	FS	1		3
L1739594	SED	OR-T2-C4-C	OR-T2-C4-C-17_SED_03-05	10/23/2017	FS	1		3
L1739594	SED	OR-T2-C4-C	OR-T2-C4-C-17_SED_05-07	10/23/2017	FS	1		3
L1739594	SED	OR-T2-C4-C	OR-T2-C4-C-17_SED_07-10	10/23/2017	FS	1		3
L1739595	SED	OR-T2-C5-E	OR-T2-C5-E-17_SED_00-01	10/24/2017	FS	1		3
L1739595	SED	OR-T2-C5-E	OR-T2-C5-E-17_SED_01-03	10/24/2017	FS	1		3
L1739595	SED	OR-T2-C5-E	OR-T2-C5-E-17_SED_03-05	10/24/2017	FS	1		3
L1739595	SED	OR-T2-C5-E	OR-T2-C5-E-17_SED_05-07	10/24/2017	FS	1		3
L1739595	SED	OR-T2-C5-E	OR-T2-C5-E-17_SED_07-10	10/24/2017	FS	1		3
L1739596	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_00-01	10/24/2017	FS	1		3
L1739596	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_01-03	10/24/2017	FS	1		3
L1739596	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_03-05	10/24/2017	FS	1		3
L1739596	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_05-07	10/24/2017	FS	1		3
L1739596	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_07-10	10/24/2017	FS	1		3
L1739596	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_10-15	10/24/2017	FS	1		3
L1739596	SED	OR-T3-C1-F	OR-T3-C1-F-17_SED_15-20	10/24/2017	FS	1		3
L1739597	SED	OR-T3-C2-F	OR-T3-C2-F-17_SED_00-01	10/23/2017	FS	1		3
L1739597	SED	OR-T3-C2-F	OR-T3-C2-F-17_SED_01-03	10/23/2017	FS	1		3
L1739597	SED	OR-T3-C2-F	OR-T3-C2-F-17_SED_03-05	10/23/2017	FS	1		3
L1739597	SED	OR-T3-C2-F	OR-T3-C2-F-17_SED_05-07	10/23/2017	FS	1		3
L1739598	SED	OR-T3-C4-F	OR-T3-C4-F-17_SED_00-01	10/23/2017	FS	1		3
L1739598	SED	OR-T3-C4-F	OR-T3-C4-F-17_SED_01-03	10/23/2017	FS	1		3
L1739598	SED	OR-T3-C4-F	OR-T3-C4-F-17_SED_03-05	10/23/2017	FS	1		3
L1739598	SED	OR-T3-C4-F	OR-T3-C4-F-17_SED_05-07	10/23/2017	FS	1		3

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1739598	SED	OR-T3-C4-F	OR-T3-C4-F-17_SED_07-10	10/23/2017	FS	1		3
L1739599	SED	OR-T3-C5-E	OR-T3-C5-E-17_SED_00-01	10/24/2017	FS	1		3
L1739599	SED	OR-T3-C5-E	OR-T3-C5-E-17_SED_01-03	10/24/2017	FS	1		3
L1739599	SED	OR-T3-C5-E	OR-T3-C5-E-17_SED_03-05	10/24/2017	FS	1		3
L1739599	SED	OR-T3-C5-E	OR-T3-C5-E-17_SED_05-07	10/24/2017	FS	1		3
L1739599	SED	OR-T3-C5-E	OR-T3-C5-E-17_SED_07-10	10/24/2017	FS	1		3
L1739601	SED	PBR-18-I	PBR-18-I-17_SED_00-01	10/20/2017	FS	1		3
L1739601	SED	PBR-18-I	PBR-18-I-17_SED_01-03	10/20/2017	FS	1		3
L1739601	SED	PBR-18-I	PBR-18-I-17_SED_03-05	10/20/2017	FS	1		3
L1739601	SED	PBR-18-I	PBR-18-I-17_SED_05-07	10/20/2017	FS	1		3
L1739602	SED	PBR-20-G	PBR-20-G-17_SED_00-01	10/23/2017	FS	1		3
L1739602	SED	PBR-20-G	PBR-20-G-17_SED_01-03	10/23/2017	FS	1		3
L1739602	SED	PBR-20-G	PBR-20-G-17_SED_03-05	10/23/2017	FS	1		3
L1739653	SED	UPB-MU11-GC-1-E	UPB-MU11-GC-1-E-17_SED_00-01	10/23/2017	FS	1		3
L1739653	SED	UPB-MU11-GC-1-E	UPB-MU11-GC-1-E-17_SED_01-03	10/23/2017	FS	1		3
L1739653	SED	UPB-MU11-GC-1-E	UPB-MU11-GC-1-E-17_SED_03-05	10/23/2017	FS	1		3
L1739653	SED	UPB-MU11-GC-1-E	UPB-MU11-GC-1-E-17_SED_05-07	10/23/2017	FS	1		3
L1739653	SED	UPB-MU11-GC-1-E	UPB-MU11-GC-1-E-17_SED_07-10	10/23/2017	FS	1		3
L1739656	SED	VE-MU4-GC-1-F	VE-MU4-GC-1-F-17_SED_00-01	10/19/2017	FS	1		3
L1739656	SED	VE-MU4-GC-1-F	VE-MU4-GC-1-F-17_SED_01-03	10/19/2017	FS	1		3
L1739656	SED	VE-MU4-GC-1-F	VE-MU4-GC-1-F-17_SED_03-05	10/19/2017	FS	1		3
L1739691	SED	MM-T3-C4-C	MM-T3-C4-C-17_SED_00-01	10/24/2017	FS	1		3
L1739691	SED	MM-T3-C4-C	MM-T3-C4-C-17_SED_01-03	10/24/2017	FS	1		3
L1739691	SED	MM-T3-C4-C	MM-T3-C4-C-17_SED_03-05	10/24/2017	FS	1		3
L1739691	SED	MM-T3-C4-C	MM-T3-C4-C-17_SED_05-07	10/24/2017	FS	1		3
L1739691	SED	MM-T3-C4-C	MM-T3-C4-C-17_SED_07-10	10/24/2017	FS	1		3
L1740283	SED	PBR-28	PBR-28-17_SED_00-01	11/1/2017	FS	1		3
L1740283	SED	PBR-28	PBR-28-17_SED_01-03	11/1/2017	FS	1		3
L1740283	SED	PBR-28	PBR-28-17_SED_03-05	11/1/2017	FS	1		3

Created by: BCG 1/15/2018

Checked by: EP 1/22/2018

TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1740283	SED	PBR-28	PBR-28-17_SED_05-07	11/1/2017	FS	1		3
L1740283	SED	PBR-28	PBR-28-17_SED_07-10	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_000-001CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_001-002CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_002-003CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_003-004CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_004-005CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_005-006CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_006-007CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_007-008CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_008-009CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_009-010CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_010-011CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_011-012CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_012-013CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_013-014CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_014-015CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_015-016CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_016-017CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_017-018CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_018-019CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_019-020CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_020-022CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_022-024CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_024-026CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_026-028CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_028-030CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_030-032CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_032-034CM	11/1/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_034-036CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_036-038CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_038-040CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_040-045CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_045-050CM	11/1/2017	FS	1		3
L1740284	SED	MM-T2-C7-A	MM-T2-C7-A-17_SED_050-055CM	11/1/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_000-001CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_001-002CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_002-003CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_003-004CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_004-005CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_005-006CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_006-007CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_007-008CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_008-009CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_009-010CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_010-011CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_011-012CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_012-013CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_013-014CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_014-015CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_015-016CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_016-017CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_017-018CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_018-019CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_019-020CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_020-022CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_022-024CM	10/31/2017	FS	1		3
L1740285	SED	MM-T3-C1	MM-T3-C1-17_SED_024-026CM	10/31/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1740287	SED	OR-T1-C1-D	OR-T1-C1-D-17_SED_00-01	11/1/2017	FS	1		3
L1740287	SED	OR-T1-C1-D	OR-T1-C1-D-17_SED_01-03	11/1/2017	FS	1		3
L1740287	SED	OR-T1-C1-D	OR-T1-C1-D-17_SED_03-05	11/1/2017	FS	1		3
L1740287	SED	OR-T1-C1-D	OR-T1-C1-D-17_SED_05-07	11/1/2017	FS	1		3
L1740287	SED	OR-T1-C1-D	OR-T1-C1-D-17_SED_07-10	11/1/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_000-001CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_001-002CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_002-003CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_003-004CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_004-005CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_005-006CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_006-007CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_007-008CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_008-009CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_009-010CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_010-011CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_011-012CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_012-013CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_013-014CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_014-015CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_015-016CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_016-017CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_017-018CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_018-019CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_019-020CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_020-022CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_022-024CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_024-026CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_026-028CM	10/31/2017	FS	1		3

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TABLE 1
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Media	Location	Field Sample ID	Sample Date	Method Class		Mercury EPA 1631	TOC Lloyd-Kahn
					Analysis Method	% Solids		
					QC Code			
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_028-030CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_030-032CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_032-034CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_034-036CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_036-038CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_038-040CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_040-045CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_045-050CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_050-055CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_055-060CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_060-065CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_065-070CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_070-075CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_075-080CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_080-085CM	10/31/2017	FS	1		3
L1740289	SED	OR-T3-C1-B	OR-T3-C1-B-17_SED_085-090CM	10/31/2017	FS	1		3
L1741133	SED	MM-T1-C1-B	MM-T1-C1-B-17_SED_00-01	11/1/2017	FS	1		3
L1741133	SED	MM-T1-C1-B	MM-T1-C1-B-17_SED_01-03	11/1/2017	FS	1		3
L1741133	SED	MM-T1-C1-B	MM-T1-C1-B-17_SED_03-05	11/1/2017	FS	1		3
L1741133	SED	MM-T1-C1-B	MM-T1-C1-B-17_SED_05-07	11/1/2017	FS	1		3
L1741133	SED	MM-T1-C1-B	MM-T1-C1-B-17_SED_07-10	11/1/2017	FS	1		3

Notes:

Count = # of analytes

FD = Field Duplicate

FS = Field Sample

SDG = Sample Delivery Group

SED = Sediment

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709432, 1709552, 1709555, 1709558, 1709562, 1709563, 1709564, 1709565, 1709566, 1709567, 1709568, 1709569, 1709570, 1709571, 1709572, 1709574, 1710289, 1710294, 1710307, 1710310, 1710313, 1710315, 1710633, 1710634, 1710637, 1710639, 1710641, 1710682, 1710684, 1710685, 1710728, 1710729, 1710730, 1710731, 1710732, 1710733, 1710907, 1710910, 1710913, 1710916, 1710917, 1710918, 1711046, 1711047, 1711050, 1711056, 1711057, 1711058, 1711059, 1711060, 1711061, 1711062, 1711063, 1711064, 1711065, 1711066, 1711067, 1711068, 1711069, 1711070, 1711071, 1711073, 1711077, 1711083, 1711084, 1711085, 1711151, 1711156, 1711171, 1711173, 1711174, 1711328, 1712044, 1712045, 1712047, L1732774, L1733612, L1733618, L1733619, L1733620, L1733621, L1736451, L1736453, L1736454, L1736455, L1736456, L1736458, L1737040, L1737041, L1737042, L1737043, L1737044, L1737045, L1737046, L1737047, L1738093, L1738103, L1738104, L1738105, L1738106, L1738128, L1739120, L1739121, L1739122, L1739123, L1739124, L1739127, L1739536, L1739537, L1739540, L1739541, L1739542, L1739572, L1739573, L1739577, L1739578, L1739579, L1739580, L1739581, L1739593, L1739594, L1739595, L1739596, L1739597, L1739598, L1739599, L1739601, L1739602, L1739653, L1739656, L1739691, L1740283, L1740284, L1740285, L1740287, L1740289 and L1741133

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709432	% Solids	1709432-01	MM-T3-C2-C-17_SED_000-001CM	Percent Solids	51.1	O-04	51.1	J	HT	% BY WT.
1709432	% Solids	1709432-02	MM-T3-C2-C-17_SED_001-002CM	Percent Solids	58.3	O-04	58.3	J	HT	% BY WT.
1709432	% Solids	1709432-03	MM-T3-C2-C-17_SED_002-003CM	Percent Solids	54.3	O-04	54.3	J	HT	% BY WT.
1709432	% Solids	1709432-04	MM-T3-C2-C-17_SED_003-004CM	Percent Solids	50	O-04	50	J	HT	% BY WT.
1709432	% Solids	1709432-05	MM-T3-C2-C-17_SED_004-005CM	Percent Solids	42.8	O-04	42.8	J	HT	% BY WT.
1709432	% Solids	1709432-06	MM-T3-C2-C-17_SED_005-006CM	Percent Solids	41.3	O-04	41.3	J	HT	% BY WT.
1709432	% Solids	1709432-07	MM-T3-C2-C-17_SED_006-007CM	Percent Solids	43	O-04	43	J	HT	% BY WT.
1709432	% Solids	1709432-08	MM-T3-C2-C-17_SED_007-008CM	Percent Solids	45.3	O-04	45.3	J	HT	% BY WT.
1709432	% Solids	1709432-09	MM-T3-C2-C-17_SED_008-009CM	Percent Solids	49	O-04	49	J	HT	% BY WT.
1709432	% Solids	1709432-10	MM-T3-C2-C-17_SED_009-010CM	Percent Solids	46.1	O-04	46.1	J	HT	% BY WT.
1709432	% Solids	1709432-11	MM-T3-C2-C-17_SED_010-011CM	Percent Solids	49.7	O-04	49.7	J	HT	% BY WT.
1709432	% Solids	1709432-12	MM-T3-C2-C-17_SED_011-012CM	Percent Solids	42.5	O-04	42.5	J	HT	% BY WT.
1709432	% Solids	1709432-13	MM-T3-C2-C-17_SED_012-013CM	Percent Solids	40.8	O-04	40.8	J	HT	% BY WT.
1709432	% Solids	1709432-14	MM-T3-C2-C-17_SED_013-014CM	Percent Solids	50.8	O-04	50.8	J	HT	% BY WT.
1709432	% Solids	1709432-15	MM-T3-C2-C-17_SED_014-015CM	Percent Solids	58.4	O-04	58.4	J	HT	% BY WT.
1709432	% Solids	1709432-16	MM-T3-C2-C-17_SED_015-016CM	Percent Solids	59.3	O-04	59.3	J	HT	% BY WT.
1709432	% Solids	1709432-17	MM-T3-C2-C-17_SED_016-017CM	Percent Solids	41.6	O-04	41.6	J	HT	% BY WT.
1709432	% Solids	1709432-18	MM-T3-C2-C-17_SED_017-018CM	Percent Solids	57	O-04	57	J	HT	% BY WT.
1709432	% Solids	1709432-19	MM-T3-C2-C-17_SED_018-019CM	Percent Solids	83	O-04	83	J	HT	% BY WT.
1709432	% Solids	1709432-20	MM-T3-C2-C-17_SED_019-020CM	Percent Solids	81.9	O-04	81.9	J	HT	% BY WT.
1709432	% Solids	1709432-21	MM-T3-C2-C-17_SED_020-022CM	Percent Solids	82.5	O-04	82.5	J	HT	% BY WT.
1709432	% Solids	1709432-22	MM-T3-C2-C-17_SED_022-024CM	Percent Solids	82.2	O-04	82.2	J	HT	% BY WT.
1709432	% Solids	1709432-23	MM-T3-C2-C-17_SED_024-026CM	Percent Solids	81.7	O-04	81.7	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709432	% Solids	1709432-24	MM-T3-C2-C-17_SED_026-028CM	Percent Solids	82.4	O-04	82.4	J	HT	% BY WT.
1709432	% Solids	1709432-25	MM-T3-C2-C-17_SED_028-030CM	Percent Solids	78.3	O-04	78.3	J	HT	% BY WT.
1709432	% Solids	1709432-26	MM-T3-C2-C-17_SED_030-032CM	Percent Solids	79.8	O-04	79.8	J	HT	% BY WT.
1709432	% Solids	1709432-27	MM-T3-C2-C-17_SED_032-034CM	Percent Solids	81.9	O-04	81.9	J	HT	% BY WT.
1709432	% Solids	1709432-28	MM-T3-C2-C-17_SED_034-036CM	Percent Solids	81.8	O-04	81.8	J	HT	% BY WT.
1709432	% Solids	1709432-29	MM-T3-C2-C-17_SED_036-038CM	Percent Solids	81.5	O-04	81.5	J	HT	% BY WT.
1709432	% Solids	1709432-30	MM-T3-C2-C-17_SED_038-040CM	Percent Solids	82.6	O-04	82.6	J	HT	% BY WT.
1709432	% Solids	1709432-31	MM-T3-C2-C-17_SED_040-045CM	Percent Solids	82.5	O-04	82.5	J	HT	% BY WT.
1709432	% Solids	1709432-32	MM-T3-C2-C-17_SED_045-050CM	Percent Solids	81.9	O-04	81.9	J	HT	% BY WT.
1709432	% Solids	1709432-33	MM-T3-C2-C-17_SED_050-055CM	Percent Solids	83.6	O-04	83.6	J	HT	% BY WT.
1709432	% Solids	1709432-34	MM-T3-C2-C-17_SED_055-060CM	Percent Solids	82.3	O-04	82.3	J	HT	% BY WT.
1709432	% Solids	1709432-35	MM-T3-C2-C-17_SED_060-065CM	Percent Solids	81.8	O-04	81.8	J	HT	% BY WT.
1709432	% Solids	1709432-36	MM-T3-C2-C-17_SED_065-070CM	Percent Solids	82.8	O-04	82.8	J	HT	% BY WT.
1709432	% Solids	1709432-37	MM-T3-C2-C-17_SED_070-075CM	Percent Solids	82.3	O-04	82.3	J	HT	% BY WT.
1709432	% Solids	1709432-38	MM-T3-C2-C-17_SED_075-080CM	Percent Solids	82.6	O-04	82.6	J	HT	% BY WT.
1709432	% Solids	1709432-39	MM-T3-C2-C-17_SED_080-085CM	Percent Solids	81.5	O-04	81.5	J	HT	% BY WT.
1709432	% Solids	1709432-40	MM-T3-C2-C-17_SED_085-090CM	Percent Solids	83.2	O-04	83.2	J	HT	% BY WT.
1709552	% Solids	1709552-01	OR-T1-C4-C-17_SED_040-045CM	Percent Solids	59.8	O-04	59.8	J	HT	% BY WT.
1709552	% Solids	1709552-02	OR-T1-C4-C-17_SED_045-050CM	Percent Solids	60.8	O-04	60.8	J	HT	% BY WT.
1709552	% Solids	1709552-03	OR-T1-C4-C-17_SED_050-055CM	Percent Solids	56.2	O-04	56.2	J	HT	% BY WT.
1709552	% Solids	1709552-04	OR-T1-C4-C-17_SED_055-060CM	Percent Solids	56.4	O-04	56.4	J	HT	% BY WT.
1709552	% Solids	1709552-05	OR-T1-C4-C-17_SED_060-065CM	Percent Solids	56.6	O-04	56.6	J	HT	% BY WT.
1709552	% Solids	1709552-06	OR-T1-C4-C-17_SED_065-070CM	Percent Solids	56.1	O-04	56.1	J	HT	% BY WT.
1709552	% Solids	1709552-07	OR-T1-C4-C-17_SED_070-075CM	Percent Solids	55.6	O-04	55.6	J	HT	% BY WT.
1709552	% Solids	1709552-08	OR-T1-C4-C-17_SED_075-080CM	Percent Solids	55.7	O-04	55.7	J	HT	% BY WT.
1709552	% Solids	1709552-09	OR-T1-C4-C-17_SED_080-085CM	Percent Solids	57	O-04	57	J	HT	% BY WT.
1709552	% Solids	1709552-10	OR-T1-C4-C-17_SED_085-090CM	Percent Solids	55.8	O-04	55.8	J	HT	% BY WT.
1709555	% Solids	1709555-01	OR-T1-C4-C-17_SED_015-016CM	Percent Solids	62.4	O-04	62.4	J	HT	% BY WT.
1709555	% Solids	1709555-02	OR-T1-C4-C-17_SED_016-017CM	Percent Solids	64.5	O-04	64.5	J	HT	% BY WT.
1709555	% Solids	1709555-03	OR-T1-C4-C-17_SED_017-018CM	Percent Solids	62.5	O-04	62.5	J	HT	% BY WT.
1709555	% Solids	1709555-04	OR-T1-C4-C-17_SED_018-019CM	Percent Solids	61.6	O-04	61.6	J	HT	% BY WT.
1709555	% Solids	1709555-05	OR-T1-C4-C-17_SED_019-020CM	Percent Solids	61	O-04	61	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709555	% Solids	1709555-06	OR-T1-C4-C-17_SED_020-022CM	Percent Solids	59.4	O-04	59.4	J	HT	% BY WT.
1709555	% Solids	1709555-07	OR-T1-C4-C-17_SED_022-024CM	Percent Solids	59.8	O-04	59.8	J	HT	% BY WT.
1709555	% Solids	1709555-08	OR-T1-C4-C-17_SED_024-026CM	Percent Solids	62.4	O-04	62.4	J	HT	% BY WT.
1709555	% Solids	1709555-09	OR-T1-C4-C-17_SED_026-028CM	Percent Solids	60.5	O-04	60.5	J	HT	% BY WT.
1709555	% Solids	1709555-10	OR-T1-C4-C-17_SED_028-030CM	Percent Solids	54.7	O-04	54.7	J	HT	% BY WT.
1709555	% Solids	1709555-11	OR-T1-C4-C-17_SED_030-032CM	Percent Solids	53.2	O-04	53.2	J	HT	% BY WT.
1709555	% Solids	1709555-12	OR-T1-C4-C-17_SED_032-034CM	Percent Solids	55.6	O-04	55.6	J	HT	% BY WT.
1709555	% Solids	1709555-13	OR-T1-C4-C-17_SED_034-036CM	Percent Solids	56.1	O-04	56.1	J	HT	% BY WT.
1709555	% Solids	1709555-14	OR-T1-C4-C-17_SED_036-038CM	Percent Solids	57.8	O-04	57.8	J	HT	% BY WT.
1709555	% Solids	1709555-15	OR-T1-C4-C-17_SED_038-040CM	Percent Solids	59.4	O-04	59.4	J	HT	% BY WT.
1709558	% Solids	1709558-01	OR-T1-C4-C-17_SED_000-001CM	Percent Solids	50.8	O-04	50.8	J	HT	% BY WT.
1709558	% Solids	1709558-02	OR-T1-C4-C-17_SED_001-002CM	Percent Solids	50.2	O-04	50.2	J	HT	% BY WT.
1709558	% Solids	1709558-03	OR-T1-C4-C-17_SED_002-003CM	Percent Solids	49.6	O-04	49.6	J	HT	% BY WT.
1709558	% Solids	1709558-04	OR-T1-C4-C-17_SED_003-004CM	Percent Solids	49.4	O-04	49.4	J	HT	% BY WT.
1709558	% Solids	1709558-05	OR-T1-C4-C-17_SED_004-005CM	Percent Solids	50.4	O-04	50.4	J	HT	% BY WT.
1709558	% Solids	1709558-06	OR-T1-C4-C-17_SED_005-006CM	Percent Solids	54.5	O-04	54.5	J	HT	% BY WT.
1709558	% Solids	1709558-07	OR-T1-C4-C-17_SED_006-007CM	Percent Solids	56.3	O-04	56.3	J	HT	% BY WT.
1709558	% Solids	1709558-08	OR-T1-C4-C-17_SED_007-008CM	Percent Solids	56.3	O-04	56.3	J	HT	% BY WT.
1709558	% Solids	1709558-09	OR-T1-C4-C-17_SED_008-009CM	Percent Solids	59.5	[1]	59.5	J	HT	% BY WT.
1709558	% Solids	1709558-10	OR-T1-C4-C-17_SED_009-010CM	Percent Solids	59.5	[2]	59.5	J	HT	% BY WT.
1709558	% Solids	1709558-11	OR-T1-C4-C-17_SED_010-011CM	Percent Solids	58	[3]	58	J	HT	% BY WT.
1709558	% Solids	1709558-12	OR-T1-C4-C-17_SED_011-012CM	Percent Solids	59.2	[4]	59.2	J	HT	% BY WT.
1709558	% Solids	1709558-13	OR-T1-C4-C-17_SED_012-013CM	Percent Solids	58.6	[5]	58.6	J	HT	% BY WT.
1709558	% Solids	1709558-14	OR-T1-C4-C-17_SED_013-014CM	Percent Solids	58.5	[6]	58.5	J	HT	% BY WT.
1709558	% Solids	1709558-15	OR-T1-C4-C-17_SED_014-015CM	Percent Solids	63.2	[7]	63.2	J	HT	% BY WT.
1709562	% Solids	1709562-01	MM-T2-C6-A-17_SED_040-045CM	Percent Solids	45	[1]	45	J	HT	% BY WT.
1709562	% Solids	1709562-02	MM-T2-C6-A-17_SED_045-050CM	Percent Solids	48.8	[2]	48.8	J	HT	% BY WT.
1709562	% Solids	1709562-03	MM-T2-C6-A-17_SED_050-055CM	Percent Solids	54.8	[3]	54.8	J	HT	% BY WT.
1709562	% Solids	1709562-04	MM-T2-C6-A-17_SED_055-060CM	Percent Solids	45	[4]	45	J	HT	% BY WT.
1709562	% Solids	1709562-05	MM-T2-C6-A-17_SED_060-065CM	Percent Solids	42.2	[5]	42.2	J	HT	% BY WT.
1709562	% Solids	1709562-06	MM-T2-C6-A-17_SED_065-070CM	Percent Solids	43.6	[6]	43.6	J	HT	% BY WT.
1709562	% Solids	1709562-07	MM-T2-C6-A-17_SED_070-075CM	Percent Solids	49	[7]	49	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709562	% Solids	1709562-08	MM-T2-C6-A-17_SED_075-080CM	Percent Solids	46.1	O-04	46.1	J	HT	% BY WT.
1709562	% Solids	1709562-09	MM-T2-C6-A-17_SED_080-085CM	Percent Solids	54.2	O-04	54.2	J	HT	% BY WT.
1709562	% Solids	1709562-10	MM-T2-C6-A-17_SED_085-090CM	Percent Solids	63	O-04	63	J	HT	% BY WT.
1709563	% Solids	1709563-01	MM-T2-C6-A-17_SED_015-016CM	Percent Solids	40.1	O-04	40.1	J	HT	% BY WT.
1709563	% Solids	1709563-02	MM-T2-C6-A-17_SED_016-017CM	Percent Solids	39.6	O-04	39.6	J	HT	% BY WT.
1709563	% Solids	1709563-03	MM-T2-C6-A-17_SED_017-018CM	Percent Solids	41.6	O-04	41.6	J	HT	% BY WT.
1709563	% Solids	1709563-04	MM-T2-C6-A-17_SED_018-019CM	Percent Solids	42.6	O-04	42.6	J	HT	% BY WT.
1709563	% Solids	1709563-05	MM-T2-C6-A-17_SED_019-020CM	Percent Solids	39.7	O-04	39.7	J	HT	% BY WT.
1709563	% Solids	1709563-06	MM-T2-C6-A-17_SED_020-022CM	Percent Solids	43.1	O-04	43.1	J	HT	% BY WT.
1709563	% Solids	1709563-07	MM-T2-C6-A-17_SED_022-024CM	Percent Solids	47.9	O-04	47.9	J	HT	% BY WT.
1709563	% Solids	1709563-08	MM-T2-C6-A-17_SED_024-026CM	Percent Solids	42.9	O-04	42.9	J	HT	% BY WT.
1709563	% Solids	1709563-09	MM-T2-C6-A-17_SED_026-028CM	Percent Solids	46.2	O-04	46.2	J	HT	% BY WT.
1709563	% Solids	1709563-10	MM-T2-C6-A-17_SED_028-030CM	Percent Solids	45.6	O-04	45.6	J	HT	% BY WT.
1709563	% Solids	1709563-11	MM-T2-C6-A-17_SED_030-032CM	Percent Solids	43.2	O-04	43.2	J	HT	% BY WT.
1709563	% Solids	1709563-12	MM-T2-C6-A-17_SED_032-034CM	Percent Solids	41.8	O-04	41.8	J	HT	% BY WT.
1709563	% Solids	1709563-13	MM-T2-C6-A-17_SED_034-036CM	Percent Solids	44.2	O-04	44.2	J	HT	% BY WT.
1709563	% Solids	1709563-14	MM-T2-C6-A-17_SED_036-038CM	Percent Solids	43.2	O-04	43.2	J	HT	% BY WT.
1709563	% Solids	1709563-15	MM-T2-C6-A-17_SED_038-040CM	Percent Solids	38.2	O-04	38.2	J	HT	% BY WT.
1709564	% Solids	1709564-01	MM-T2-C6-A-17_SED_000-001CM	Percent Solids	37.2	O-04	37.2	J	HT	% BY WT.
1709564	% Solids	1709564-02	MM-T2-C6-A-17_SED_001-002CM	Percent Solids	43.8	O-04	43.8	J	HT	% BY WT.
1709564	% Solids	1709564-03	MM-T2-C6-A-17_SED_002-003CM	Percent Solids	39.8	O-04	39.8	J	HT	% BY WT.
1709564	% Solids	1709564-04	MM-T2-C6-A-17_SED_003-004CM	Percent Solids	38	O-04	38	J	HT	% BY WT.
1709564	% Solids	1709564-05	MM-T2-C6-A-17_SED_004-005CM	Percent Solids	40.5	O-04	40.5	J	HT	% BY WT.
1709564	% Solids	1709564-06	MM-T2-C6-A-17_SED_005-006CM	Percent Solids	37.8	O-04	37.8	J	HT	% BY WT.
1709564	% Solids	1709564-07	MM-T2-C6-A-17_SED_006-007CM	Percent Solids	39.8	O-04	39.8	J	HT	% BY WT.
1709564	% Solids	1709564-08	MM-T2-C6-A-17_SED_007-008CM	Percent Solids	42.1	O-04	42.1	J	HT	% BY WT.
1709564	% Solids	1709564-09	MM-T2-C6-A-17_SED_008-009CM	Percent Solids	38.5	O-04	38.5	J	HT	% BY WT.
1709564	% Solids	1709564-10	MM-T2-C6-A-17_SED_009-010CM	Percent Solids	41.3	O-04	41.3	J	HT	% BY WT.
1709564	% Solids	1709564-11	MM-T2-C6-A-17_SED_010-011CM	Percent Solids	40.3	O-04	40.3	J	HT	% BY WT.
1709564	% Solids	1709564-12	MM-T2-C6-A-17_SED_011-012CM	Percent Solids	40.6	O-04	40.6	J	HT	% BY WT.
1709564	% Solids	1709564-13	MM-T2-C6-A-17_SED_012-013CM	Percent Solids	42.6	O-04	42.6	J	HT	% BY WT.
1709564	% Solids	1709564-14	MM-T2-C6-A-17_SED_013-014CM	Percent Solids	42.6	O-04	42.6	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709564	% Solids	1709564-15	MM-T2-C6-A-17_SED_014-015CM	Percent Solids	44.1	O-04	44.1	J	HT	% BY WT.
1709565	% Solids	1709565-01	MM-T2-C5-A-17_SED_040-045CM	Percent Solids	63.6	O-04	63.6	J	HT	% BY WT.
1709565	% Solids	1709565-02	MM-T2-C5-A-17_SED_045-050CM	Percent Solids	63.1	O-04	63.1	J	HT	% BY WT.
1709565	% Solids	1709565-03	MM-T2-C5-A-17_SED_050-055CM	Percent Solids	67.5	O-04	67.5	J	HT	% BY WT.
1709565	% Solids	1709565-04	MM-T2-C5-A-17_SED_055-060CM	Percent Solids	66	O-04	66	J	HT	% BY WT.
1709565	% Solids	1709565-05	MM-T2-C5-A-17_SED_060-065CM	Percent Solids	64.8	O-04	64.8	J	HT	% BY WT.
1709565	% Solids	1709565-06	MM-T2-C5-A-17_SED_065-070CM	Percent Solids	67.1	O-04	67.1	J	HT	% BY WT.
1709565	% Solids	1709565-07	MM-T2-C5-A-17_SED_070-075CM	Percent Solids	63	O-04	63	J	HT	% BY WT.
1709565	% Solids	1709565-08	MM-T2-C5-A-17_SED_075-080CM	Percent Solids	58.4	O-04	58.4	J	HT	% BY WT.
1709565	% Solids	1709565-09	MM-T2-C5-A-17_SED_080-085CM	Percent Solids	55.8	O-04	55.8	J	HT	% BY WT.
1709565	% Solids	1709565-10	MM-T2-C5-A-17_SED_085-090CM	Percent Solids	59	O-04	59	J	HT	% BY WT.
1709566	% Solids	1709566-01	MM-T2-C5-A-17_SED_015-016CM	Percent Solids	63.8	O-04	63.8	J	HT	% BY WT.
1709566	% Solids	1709566-02	MM-T2-C5-A-17_SED_016-017CM	Percent Solids	60.3	O-04	60.3	J	HT	% BY WT.
1709566	% Solids	1709566-03	MM-T2-C5-A-17_SED_017-018CM	Percent Solids	62.9	O-04	62.9	J	HT	% BY WT.
1709566	% Solids	1709566-04	MM-T2-C5-A-17_SED_018-019CM	Percent Solids	64.1	O-04	64.1	J	HT	% BY WT.
1709566	% Solids	1709566-05	MM-T2-C5-A-17_SED_019-020CM	Percent Solids	67.4	[1]	67.4	J	HT	% BY WT.
1709566	% Solids	1709566-06	MM-T2-C5-A-17_SED_020-022CM	Percent Solids	67.8	[2]	67.8	J	HT	% BY WT.
1709566	% Solids	1709566-07	MM-T2-C5-A-17_SED_022-024CM	Percent Solids	65.9	[3]	65.9	J	HT	% BY WT.
1709566	% Solids	1709566-08	MM-T2-C5-A-17_SED_024-026CM	Percent Solids	62.8	[4]	62.8	J	HT	% BY WT.
1709566	% Solids	1709566-09	MM-T2-C5-A-17_SED_026-028CM	Percent Solids	64.9	[5]	64.9	J	HT	% BY WT.
1709566	% Solids	1709566-10	MM-T2-C5-A-17_SED_028-030CM	Percent Solids	63.6	[6]	63.6	J	HT	% BY WT.
1709566	% Solids	1709566-11	MM-T2-C5-A-17_SED_030-032CM	Percent Solids	67.1	[7]	67.1	J	HT	% BY WT.
1709566	% Solids	1709566-12	MM-T2-C5-A-17_SED_032-034CM	Percent Solids	63	[8]	63	J	HT	% BY WT.
1709566	% Solids	1709566-13	MM-T2-C5-A-17_SED_034-036CM	Percent Solids	65.8	[9]	65.8	J	HT	% BY WT.
1709566	% Solids	1709566-14	MM-T2-C5-A-17_SED_036-038CM	Percent Solids	64.7	[10]	64.7	J	HT	% BY WT.
1709566	% Solids	1709566-15	MM-T2-C5-A-17_SED_038-040CM	Percent Solids	64.6	[11]	64.6	J	HT	% BY WT.
1709567	% Solids	1709567-01	MM-T2-C5-A-17_SED_000-001CM	Percent Solids	36.1	O-04	36.1	J	HT	% BY WT.
1709567	% Solids	1709567-02	MM-T2-C5-A-17_SED_001-002CM	Percent Solids	33.4	O-04	33.4	J	HT	% BY WT.
1709567	% Solids	1709567-03	MM-T2-C5-A-17_SED_002-003CM	Percent Solids	35.8	O-04	35.8	J	HT	% BY WT.
1709567	% Solids	1709567-04	MM-T2-C5-A-17_SED_003-004CM	Percent Solids	39.6	O-04	39.6	J	HT	% BY WT.
1709567	% Solids	1709567-05	MM-T2-C5-A-17_SED_004-005CM	Percent Solids	44	O-04	44	J	HT	% BY WT.
1709567	% Solids	1709567-06	MM-T2-C5-A-17_SED_005-006CM	Percent Solids	45.2	O-04	45.2	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709567	% Solids	1709567-07	MM-T2-C5-A-17_SED_006-007CM	Percent Solids	46.1	O-04	46.1	J	HT	% BY WT.
1709567	% Solids	1709567-08	MM-T2-C5-A-17_SED_007-008CM	Percent Solids	51.4	O-04	51.4	J	HT	% BY WT.
1709567	% Solids	1709567-09	MM-T2-C5-A-17_SED_008-009CM	Percent Solids	41.3	O-04	41.3	J	HT	% BY WT.
1709567	% Solids	1709567-10	MM-T2-C5-A-17_SED_009-010CM	Percent Solids	53.6	O-04	53.6	J	HT	% BY WT.
1709567	% Solids	1709567-11	MM-T2-C5-A-17_SED_010-011CM	Percent Solids	59.3	O-04	59.3	J	HT	% BY WT.
1709567	% Solids	1709567-12	MM-T2-C5-A-17_SED_011-012CM	Percent Solids	53.1	O-04	53.1	J	HT	% BY WT.
1709567	% Solids	1709567-13	MM-T2-C5-A-17_SED_012-013CM	Percent Solids	55.5	O-04	55.5	J	HT	% BY WT.
1709567	% Solids	1709567-14	MM-T2-C5-A-17_SED_013-014CM	Percent Solids	56	O-04	56	J	HT	% BY WT.
1709567	% Solids	1709567-15	MM-T2-C5-A-17_SED_014-015CM	Percent Solids	56.5	O-04	56.5	J	HT	% BY WT.
1709568	% Solids	1709568-01	MM-T2-C4-B-17_SED_040-045CM	Percent Solids	84.5	[1]	84.5	J	HT	% BY WT.
1709568	% Solids	1709568-02	MM-T2-C4-B-17_SED_045-050CM	Percent Solids	81.5	[2]	81.5	J	HT	% BY WT.
1709568	% Solids	1709568-03	MM-T2-C4-B-17_SED_050-055CM	Percent Solids	83.7	[3]	83.7	J	HT	% BY WT.
1709568	% Solids	1709568-04	MM-T2-C4-B-17_SED_055-060CM	Percent Solids	82.5	[4]	82.5	J	HT	% BY WT.
1709568	% Solids	1709568-05	MM-T2-C4-B-17_SED_060-065CM	Percent Solids	80.6	[5]	80.6	J	HT	% BY WT.
1709568	% Solids	1709568-06	MM-T2-C4-B-17_SED_065-070CM	Percent Solids	81.9	[6]	81.9	J	HT	% BY WT.
1709568	% Solids	1709568-07	MM-T2-C4-B-17_SED_070-075CM	Percent Solids	80.1	[7]	80.1	J	HT	% BY WT.
1709568	% Solids	1709568-08	MM-T2-C4-B-17_SED_075-080CM	Percent Solids	81.5	[8]	81.5	J	HT	% BY WT.
1709568	% Solids	1709568-09	MM-T2-C4-B-17_SED_080-085CM	Percent Solids	81.1	[9]	81.1	J	HT	% BY WT.
1709568	% Solids	1709568-10	MM-T2-C4-B-17_SED_085-090CM	Percent Solids	80.9	[10]	80.9	J	HT	% BY WT.
1709569	% Solids	1709569-01	MM-T2-C4-B-17_SED_015-016CM	Percent Solids	74.4	[11]	74.4	J	HT	% BY WT.
1709569	% Solids	1709569-02	MM-T2-C4-B-17_SED_016-017CM	Percent Solids	76.4	[12]	76.4	J	HT	% BY WT.
1709569	% Solids	1709569-03	MM-T2-C4-B-17_SED_017-018CM	Percent Solids	75.6	[13]	75.6	J	HT	% BY WT.
1709569	% Solids	1709569-04	MM-T2-C4-B-17_SED_018-019CM	Percent Solids	73.1	[14]	73.1	J	HT	% BY WT.
1709569	% Solids	1709569-05	MM-T2-C4-B-17_SED_019-020CM	Percent Solids	74.1	[15]	74.1	J	HT	% BY WT.
1709569	% Solids	1709569-06	MM-T2-C4-B-17_SED_020-022CM	Percent Solids	71.4	[16]	71.4	J	HT	% BY WT.
1709569	% Solids	1709569-07	MM-T2-C4-B-17_SED_022-024CM	Percent Solids	84.7	[17]	84.7	J	HT	% BY WT.
1709569	% Solids	1709569-08	MM-T2-C4-B-17_SED_024-026CM	Percent Solids	85.6	[18]	85.6	J	HT	% BY WT.
1709569	% Solids	1709569-09	MM-T2-C4-B-17_SED_026-028CM	Percent Solids	87.1	[19]	87.1	J	HT	% BY WT.
1709569	% Solids	1709569-10	MM-T2-C4-B-17_SED_028-030CM	Percent Solids	85.4	[20]	85.4	J	HT	% BY WT.
1709569	% Solids	1709569-11	MM-T2-C4-B-17_SED_030-032CM	Percent Solids	85.1	[21]	85.1	J	HT	% BY WT.
1709569	% Solids	1709569-12	MM-T2-C4-B-17_SED_032-034CM	Percent Solids	82.5	[22]	82.5	J	HT	% BY WT.
1709569	% Solids	1709569-13	MM-T2-C4-B-17_SED_034-036CM	Percent Solids	83.5	[23]	83.5	J	HT	% BY WT.

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1709569	% Solids	1709569-14	MM-T2-C4-B-17_SED_036-038CM	Percent Solids	82.8	[24]	82.8	J	HT	% BY WT.
1709569	% Solids	1709569-15	MM-T2-C4-B-17_SED_038-040CM	Percent Solids	84.2	[25]	84.2	J	HT	% BY WT.
1709570	% Solids	1709570-01	MM-T2-C4-B-17_SED_000-001CM	Percent Solids	40	[26]	40	J	HT	% BY WT.
1709570	% Solids	1709570-02	MM-T2-C4-B-17_SED_001-002CM	Percent Solids	47.2	[27]	47.2	J	HT	% BY WT.
1709570	% Solids	1709570-03	MM-T2-C4-B-17_SED_002-003CM	Percent Solids	43.8	[28]	43.8	J	HT	% BY WT.
1709570	% Solids	1709570-04	MM-T2-C4-B-17_SED_003-004CM	Percent Solids	45	[29]	45	J	HT	% BY WT.
1709570	% Solids	1709570-05	MM-T2-C4-B-17_SED_004-005CM	Percent Solids	48.6	O-04	48.6	J	HT,LD	% BY WT.
1709570	% Solids	1709570-06	MM-T2-C4-B-17_SED_005-006CM	Percent Solids	50.1	O-04	50.1	J	HT	% BY WT.
1709570	% Solids	1709570-07	MM-T2-C4-B-17_SED_006-007CM	Percent Solids	54.9	O-04	54.9	J	HT	% BY WT.
1709570	% Solids	1709570-08	MM-T2-C4-B-17_SED_007-008CM	Percent Solids	56.7	O-04	56.7	J	HT	% BY WT.
1709570	% Solids	1709570-09	MM-T2-C4-B-17_SED_008-009CM	Percent Solids	56.9	O-04	56.9	J	HT	% BY WT.
1709570	% Solids	1709570-10	MM-T2-C4-B-17_SED_009-010CM	Percent Solids	60	O-04	60	J	HT	% BY WT.
1709570	% Solids	1709570-11	MM-T2-C4-B-17_SED_010-011CM	Percent Solids	60.6	O-04	60.6	J	HT	% BY WT.
1709570	% Solids	1709570-12	MM-T2-C4-B-17_SED_011-012CM	Percent Solids	63.8	O-04	63.8	J	HT	% BY WT.
1709570	% Solids	1709570-13	MM-T2-C4-B-17_SED_012-013CM	Percent Solids	64.7	O-04	64.7	J	HT	% BY WT.
1709570	% Solids	1709570-14	MM-T2-C4-B-17_SED_013-014CM	Percent Solids	66.9	O-04	66.9	J	HT	% BY WT.
1709570	% Solids	1709570-15	MM-T2-C4-B-17_SED_014-015CM	Percent Solids	68.8	O-04	68.8	J	HT	% BY WT.
1709571	% Solids	1709571-01	MM-T1-C3-B-17_SED_040-045CM	Percent Solids	92.3	O-04	92.3	J	HT	% BY WT.
1709571	% Solids	1709571-02	MM-T1-C3-B-17_SED_045-050CM	Percent Solids	93.2	O-04	93.2	J	HT	% BY WT.
1709571	% Solids	1709571-03	MM-T1-C3-B-17_SED_050-055CM	Percent Solids	92	O-04	92	J	HT	% BY WT.
1709571	% Solids	1709571-04	MM-T1-C3-B-17_SED_055-060CM	Percent Solids	91.5	O-04	91.5	J	HT	% BY WT.
1709571	% Solids	1709571-05	MM-T1-C3-B-17_SED_060-065CM	Percent Solids	91.9	O-04	91.9	J	HT	% BY WT.
1709571	% Solids	1709571-06	MM-T1-C3-B-17_SED_065-070CM	Percent Solids	90.7	O-04	90.7	J	HT	% BY WT.
1709571	% Solids	1709571-07	MM-T1-C3-B-17_SED_070-075CM	Percent Solids	92.8	O-04	92.8	J	HT	% BY WT.
1709572	% Solids	1709572-01	MM-T1-C3-B-17_SED_015-016CM	Percent Solids	89.1	O-04	89.1	J	HT	% BY WT.
1709572	% Solids	1709572-02	MM-T1-C3-B-17_SED_016-017CM	Percent Solids	93.4	O-04	93.4	J	HT	% BY WT.
1709572	% Solids	1709572-03	MM-T1-C3-B-17_SED_017-018CM	Percent Solids	86.9	O-04	86.9	J	HT	% BY WT.
1709572	% Solids	1709572-04	MM-T1-C3-B-17_SED_018-019CM	Percent Solids	90.4	O-04	90.4	J	HT	% BY WT.
1709572	% Solids	1709572-05	MM-T1-C3-B-17_SED_019-020CM	Percent Solids	91.8	O-04	91.8	J	HT	% BY WT.
1709572	% Solids	1709572-06	MM-T1-C3-B-17_SED_020-022CM	Percent Solids	93.6	O-04	93.6	J	HT	% BY WT.
1709572	% Solids	1709572-07	MM-T1-C3-B-17_SED_022-024CM	Percent Solids	88	O-04	88	J	HT	% BY WT.
1709572	% Solids	1709572-08	MM-T1-C3-B-17_SED_024-026CM	Percent Solids	90.5	O-04	90.5	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1709572	% Solids	1709572-09	MM-T1-C3-B-17_SED_026-028CM	Percent Solids	89.8	O-04	89.8	J	HT	% BY WT.
1709572	% Solids	1709572-10	MM-T1-C3-B-17_SED_028-030CM	Percent Solids	88.4	O-04	88.4	J	HT	% BY WT.
1709572	% Solids	1709572-11	MM-T1-C3-B-17_SED_030-032CM	Percent Solids	94.4	O-04	94.4	J	HT	% BY WT.
1709572	% Solids	1709572-12	MM-T1-C3-B-17_SED_032-034CM	Percent Solids	92.1	O-04	92.1	J	HT	% BY WT.
1709572	% Solids	1709572-13	MM-T1-C3-B-17_SED_034-036CM	Percent Solids	93.3	O-04	93.3	J	HT	% BY WT.
1709572	% Solids	1709572-14	MM-T1-C3-B-17_SED_036-038CM	Percent Solids	93.6	O-04	93.6	J	HT	% BY WT.
1709572	% Solids	1709572-15	MM-T1-C3-B-17_SED_038-040CM	Percent Solids	91	O-04	91	J	HT	% BY WT.
1709574	% Solids	1709574-01	MM-T1-C3-B-17_SED_000-001CM	Percent Solids	40.4	O-04	40.4	J	HT	% BY WT.
1709574	% Solids	1709574-02	MM-T1-C3-B-17_SED_001-002CM	Percent Solids	42.3	O-04	42.3	J	HT	% BY WT.
1709574	% Solids	1709574-03	MM-T1-C3-B-17_SED_002-003CM	Percent Solids	42.7	O-04	42.7	J	HT	% BY WT.
1709574	% Solids	1709574-04	MM-T1-C3-B-17_SED_003-004CM	Percent Solids	45.6	O-04	45.6	J	HT	% BY WT.
1709574	% Solids	1709574-05	MM-T1-C3-B-17_SED_004-005CM	Percent Solids	63.7	O-04	63.7	J	HT	% BY WT.
1709574	% Solids	1709574-06	MM-T1-C3-B-17_SED_005-006CM	Percent Solids	53.5	O-04	53.5	J	HT	% BY WT.
1709574	% Solids	1709574-07	MM-T1-C3-B-17_SED_006-007CM	Percent Solids	53.6	O-04	53.6	J	HT	% BY WT.
1709574	% Solids	1709574-08	MM-T1-C3-B-17_SED_007-008CM	Percent Solids	58.7	O-04	58.7	J	HT	% BY WT.
1709574	% Solids	1709574-09	MM-T1-C3-B-17_SED_008-009CM	Percent Solids	73.1	O-04	73.1	J	HT	% BY WT.
1709574	% Solids	1709574-10	MM-T1-C3-B-17_SED_009-010CM	Percent Solids	72.5	O-04	72.5	J	HT	% BY WT.
1709574	% Solids	1709574-11	MM-T1-C3-B-17_SED_010-011CM	Percent Solids	82.8	O-04	82.8	J	HT	% BY WT.
1709574	% Solids	1709574-12	MM-T1-C3-B-17_SED_011-012CM	Percent Solids	78.8	O-04	78.8	J	HT	% BY WT.
1709574	% Solids	1709574-13	MM-T1-C3-B-17_SED_012-013CM	Percent Solids	86.1	O-04	86.1	J	HT	% BY WT.
1709574	% Solids	1709574-14	MM-T1-C3-B-17_SED_013-014CM	Percent Solids	90.1	O-04	90.1	J	HT	% BY WT.
1709574	% Solids	1709574-15	MM-T1-C3-B-17_SED_014-015CM	Percent Solids	88.5	O-04	88.5	J	HT	% BY WT.
1710289	% Solids	1710289-01	MM-T1-C2-B-17_SED_000-001CM	Percent Solids	34.7	[1]	34.7	J	HT	% BY WT.
1710289	% Solids	1710289-02	MM-T1-C2-B-17_SED_001-002CM	Percent Solids	30.5	[2]	30.5	J	HT	% BY WT.
1710289	% Solids	1710289-03	MM-T1-C2-B-17_SED_002-003CM	Percent Solids	29.6	[3]	29.6	J	HT	% BY WT.
1710289	% Solids	1710289-04	MM-T1-C2-B-17_SED_003-004CM	Percent Solids	35.5	[4]	35.5	J	HT	% BY WT.
1710289	% Solids	1710289-05	MM-T1-C2-B-17_SED_004-005CM	Percent Solids	34.6	[5]	34.6	J	HT	% BY WT.
1710289	% Solids	1710289-06	MM-T1-C2-B-17_SED_005-006CM	Percent Solids	37.1	[6]	37.1	J	HT	% BY WT.
1710289	% Solids	1710289-07	MM-T1-C2-B-17_SED_006-007CM	Percent Solids	36.5	[7]	36.5	J	HT	% BY WT.
1710289	% Solids	1710289-08	MM-T1-C2-B-17_SED_007-008CM	Percent Solids	37.4	[8]	37.4	J	HT	% BY WT.
1710289	% Solids	1710289-09	MM-T1-C2-B-17_SED_008-009CM	Percent Solids	37.7	[9]	37.7	J	HT	% BY WT.
1710289	% Solids	1710289-10	MM-T1-C2-B-17_SED_009-010CM	Percent Solids	36.3	[10]	36.3	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710289	% Solids	1710289-11	MM-T1-C2-B-17_SED_010-011CM	Percent Solids	34.4	[11]	34.4	J	HT	% BY WT.
1710289	% Solids	1710289-12	MM-T1-C2-B-17_SED_011-012CM	Percent Solids	36	[12]	36	J	HT	% BY WT.
1710289	% Solids	1710289-13	MM-T1-C2-B-17_SED_012-013CM	Percent Solids	34.3	[13]	34.3	J	HT	% BY WT.
1710289	% Solids	1710289-14	MM-T1-C2-B-17_SED_013-014CM	Percent Solids	37.6	[14]	37.6	J	HT	% BY WT.
1710289	% Solids	1710289-15	MM-T1-C2-B-17_SED_014-015CM	Percent Solids	36.9	[15]	36.9	J	HT	% BY WT.
1710289	% Solids	1710289-16	MM-T1-C2-B-17_SED_015-016CM	Percent Solids	38.1	[16]	38.1	J	HT	% BY WT.
1710289	% Solids	1710289-17	MM-T1-C2-B-17_SED_016-017CM	Percent Solids	38.6	[17]	38.6	J	HT	% BY WT.
1710289	% Solids	1710289-18	MM-T1-C2-B-17_SED_017-018CM	Percent Solids	37.3	[18]	37.3	J	HT	% BY WT.
1710289	% Solids	1710289-19	MM-T1-C2-B-17_SED_018-019CM	Percent Solids	36.3	[19]	36.3	J	HT	% BY WT.
1710289	% Solids	1710289-20	MM-T1-C2-B-17_SED_019-020CM	Percent Solids	36.7	[20]	36.7	J	HT	% BY WT.
1710289	% Solids	1710289-21	MM-T1-C2-B-17_SED_020-022CM	Percent Solids	39.2	[21]	39.2	J	HT	% BY WT.
1710289	% Solids	1710289-22	MM-T1-C2-B-17_SED_022-024CM	Percent Solids	39.8	[22]	39.8	J	HT	% BY WT.
1710289	% Solids	1710289-23	MM-T1-C2-B-17_SED_024-026CM	Percent Solids	42.8	[23]	42.8	J	HT	% BY WT.
1710289	% Solids	1710289-24	MM-T1-C2-B-17_SED_026-028CM	Percent Solids	45.9	[24]	45.9	J	HT	% BY WT.
1710289	% Solids	1710289-25	MM-T1-C2-B-17_SED_028-030CM	Percent Solids	45.6	[25]	45.6	J	HT	% BY WT.
1710289	% Solids	1710289-26	MM-T1-C2-B-17_SED_030-032CM	Percent Solids	45.8	[26]	45.8	J	HT	% BY WT.
1710289	% Solids	1710289-27	MM-T1-C2-B-17_SED_032-034CM	Percent Solids	47	[27]	47	J	HT	% BY WT.
1710289	% Solids	1710289-28	MM-T1-C2-B-17_SED_034-036CM	Percent Solids	47.3	[28]	47.3	J	HT	% BY WT.
1710289	% Solids	1710289-29	MM-T1-C2-B-17_SED_036-038CM	Percent Solids	58	[29]	58	J	HT	% BY WT.
1710289	% Solids	1710289-30	MM-T1-C2-B-17_SED_038-040CM	Percent Solids	56.7	[30]	56.7	J	HT	% BY WT.
1710289	% Solids	1710289-31	MM-T1-C2-B-17_SED_040-045CM	Percent Solids	60.9	[31]	60.9	J	HT	% BY WT.
1710289	% Solids	1710289-32	MM-T1-C2-B-17_SED_045-050CM	Percent Solids	61.3	[32]	61.3	J	HT	% BY WT.
1710289	% Solids	1710289-33	MM-T1-C2-B-17_SED_050-055CM	Percent Solids	59.7	[33]	59.7	J	HT	% BY WT.
1710289	% Solids	1710289-34	MM-T1-C2-B-17_SED_055-060CM	Percent Solids	62.7	[34]	62.7	J	HT	% BY WT.
1710289	% Solids	1710289-35	MM-T1-C2-B-17_SED_060-065CM	Percent Solids	61.7	[35]	61.7	J	HT	% BY WT.
1710294	% Solids	1710294-01	OR-T1-C2-B-17_SED_000-001CM	Percent Solids	40.1	[1]	40.1	J	HT	% BY WT.
1710294	% Solids	1710294-02	OR-T1-C2-B-17_SED_001-002CM	Percent Solids	40.9	[2]	40.9	J	HT	% BY WT.
1710294	% Solids	1710294-03	OR-T1-C2-B-17_SED_002-003CM	Percent Solids	39.7	[3]	39.7	J	HT	% BY WT.
1710294	% Solids	1710294-04	OR-T1-C2-B-17_SED_003-004CM	Percent Solids	40.2	[4]	40.2	J	HT	% BY WT.
1710294	% Solids	1710294-05	OR-T1-C2-B-17_SED_004-005CM	Percent Solids	46.6	[5]	46.6	J	HT	% BY WT.
1710294	% Solids	1710294-06	OR-T1-C2-B-17_SED_005-006CM	Percent Solids	43.1	[6]	43.1	J	HT	% BY WT.
1710294	% Solids	1710294-07	OR-T1-C2-B-17_SED_006-007CM	Percent Solids	41.8	[7]	41.8	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710294	% Solids	1710294-08	OR-T1-C2-B-17_SED_007-008CM	Percent Solids	41.9	[8]	41.9	J	HT	% BY WT.
1710294	% Solids	1710294-09	OR-T1-C2-B-17_SED_008-009CM	Percent Solids	42	[9]	42	J	HT	% BY WT.
1710294	% Solids	1710294-10	OR-T1-C2-B-17_SED_009-010CM	Percent Solids	43.6	[10]	43.6	J	HT	% BY WT.
1710294	% Solids	1710294-11	OR-T1-C2-B-17_SED_010-011CM	Percent Solids	42.6	[11]	42.6	J	HT	% BY WT.
1710294	% Solids	1710294-12	OR-T1-C2-B-17_SED_011-012CM	Percent Solids	43	[12]	43	J	HT	% BY WT.
1710294	% Solids	1710294-13	OR-T1-C2-B-17_SED_012-013CM	Percent Solids	42.3	[13]	42.3	J	HT	% BY WT.
1710294	% Solids	1710294-14	OR-T1-C2-B-17_SED_013-014CM	Percent Solids	44.1	[14]	44.1	J	HT	% BY WT.
1710294	% Solids	1710294-15	OR-T1-C2-B-17_SED_014-015CM	Percent Solids	44.6	[15]	44.6	J	HT	% BY WT.
1710294	% Solids	1710294-16	OR-T1-C2-B-17_SED_015-016CM	Percent Solids	45.1	[16]	45.1	J	HT	% BY WT.
1710294	% Solids	1710294-17	OR-T1-C2-B-17_SED_016-017CM	Percent Solids	44.3	[17]	44.3	J	HT	% BY WT.
1710294	% Solids	1710294-18	OR-T1-C2-B-17_SED_017-018CM	Percent Solids	44.5	[18]	44.5	J	HT	% BY WT.
1710294	% Solids	1710294-19	OR-T1-C2-B-17_SED_018-019CM	Percent Solids	44.6	[19]	44.6	J	HT	% BY WT.
1710294	% Solids	1710294-20	OR-T1-C2-B-17_SED_019-020CM	Percent Solids	44.5	[20]	44.5	J	HT	% BY WT.
1710294	% Solids	1710294-21	OR-T1-C2-B-17_SED_020-022CM	Percent Solids	43.8	[21]	43.8	J	HT	% BY WT.
1710294	% Solids	1710294-22	OR-T1-C2-B-17_SED_022-024CM	Percent Solids	44.6	[22]	44.6	J	HT	% BY WT.
1710294	% Solids	1710294-23	OR-T1-C2-B-17_SED_024-026CM	Percent Solids	44.9	[23]	44.9	J	HT	% BY WT.
1710294	% Solids	1710294-24	OR-T1-C2-B-17_SED_026-028CM	Percent Solids	44.8	[24]	44.8	J	HT	% BY WT.
1710294	% Solids	1710294-25	OR-T1-C2-B-17_SED_028-030CM	Percent Solids	45.6	[25]	45.6	J	HT	% BY WT.
1710294	% Solids	1710294-26	OR-T1-C2-B-17_SED_030-032CM	Percent Solids	44.2	[26]	44.2	J	HT	% BY WT.
1710294	% Solids	1710294-27	OR-T1-C2-B-17_SED_032-034CM	Percent Solids	44.4	[27]	44.4	J	HT	% BY WT.
1710294	% Solids	1710294-28	OR-T1-C2-B-17_SED_034-036CM	Percent Solids	44	[28]	44	J	HT	% BY WT.
1710294	% Solids	1710294-29	OR-T1-C2-B-17_SED_036-038CM	Percent Solids	43.2	[29]	43.2	J	HT	% BY WT.
1710294	% Solids	1710294-30	OR-T1-C2-B-17_SED_038-040CM	Percent Solids	40.7	[30]	40.7	J	HT	% BY WT.
1710294	% Solids	1710294-31	OR-T1-C2-B-17_SED_040-045CM	Percent Solids	39.7	[31]	39.7	J	HT	% BY WT.
1710294	% Solids	1710294-32	OR-T1-C2-B-17_SED_045-050CM	Percent Solids	39.6	[32]	39.6	J	HT	% BY WT.
1710294	% Solids	1710294-33	OR-T1-C2-B-17_SED_050-055CM	Percent Solids	39.4	[33]	39.4	J	HT	% BY WT.
1710294	% Solids	1710294-34	OR-T1-C2-B-17_SED_055-060CM	Percent Solids	43.7	[34]	43.7	J	HT	% BY WT.
1710294	% Solids	1710294-35	OR-T1-C2-B-17_SED_060-065CM	Percent Solids	41.5	[35]	41.5	J	HT	% BY WT.
1710294	% Solids	1710294-36	OR-T1-C2-B-17_SED_065-070CM	Percent Solids	41.3	[36]	41.3	J	HT	% BY WT.
1710294	% Solids	1710294-37	OR-T1-C2-B-17_SED_070-075CM	Percent Solids	39.3	[37]	39.3	J	HT	% BY WT.
1710294	% Solids	1710294-38	OR-T1-C2-B-17_SED_075-080CM	Percent Solids	40.5	[38]	40.5	J	HT	% BY WT.
1710294	% Solids	1710294-39	OR-T1-C2-B-17_SED_080-085CM	Percent Solids	62.4	[39]	62.4	J	HT	% BY WT.

TABLE 2
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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710294	% Solids	1710294-40	OR-T1-C2-B-17_SED_085-090CM	Percent Solids	63.4	[40]	63.4	J	HT	% BY WT.
1710307	% Solids	1710307-01	OR-T1-C5-A-17_SED_000-001CM	Percent Solids	40	[1]	40	J	HT	% BY WT.
1710307	% Solids	1710307-02	OR-T1-C5-A-17_SED_001-002CM	Percent Solids	42.5	[2]	42.5	J	HT	% BY WT.
1710307	% Solids	1710307-03	OR-T1-C5-A-17_SED_002-003CM	Percent Solids	47.3	[3]	47.3	J	HT	% BY WT.
1710307	% Solids	1710307-04	OR-T1-C5-A-17_SED_003-004CM	Percent Solids	42.6	[4]	42.6	J	HT	% BY WT.
1710307	% Solids	1710307-05	OR-T1-C5-A-17_SED_004-005CM	Percent Solids	44.1	[5]	44.1	J	HT	% BY WT.
1710307	% Solids	1710307-06	OR-T1-C5-A-17_SED_005-006CM	Percent Solids	45.2	[6]	45.2	J	HT	% BY WT.
1710307	% Solids	1710307-07	OR-T1-C5-A-17_SED_006-007CM	Percent Solids	42.6	[7]	42.6	J	HT	% BY WT.
1710307	% Solids	1710307-08	OR-T1-C5-A-17_SED_007-008CM	Percent Solids	40.6	[8]	40.6	J	HT	% BY WT.
1710307	% Solids	1710307-09	OR-T1-C5-A-17_SED_008-009CM	Percent Solids	41.8	[9]	41.8	J	HT	% BY WT.
1710307	% Solids	1710307-10	OR-T1-C5-A-17_SED_009-010CM	Percent Solids	42.3	[10]	42.3	J	HT	% BY WT.
1710307	% Solids	1710307-11	OR-T1-C5-A-17_SED_010-011CM	Percent Solids	43.6	[11]	43.6	J	HT	% BY WT.
1710307	% Solids	1710307-12	OR-T1-C5-A-17_SED_011-012CM	Percent Solids	46.9	[12]	46.9	J	HT	% BY WT.
1710307	% Solids	1710307-13	OR-T1-C5-A-17_SED_012-013CM	Percent Solids	48.7	[13]	48.7	J	HT	% BY WT.
1710307	% Solids	1710307-14	OR-T1-C5-A-17_SED_013-014CM	Percent Solids	50.5	[14]	50.5	J	HT	% BY WT.
1710307	% Solids	1710307-15	OR-T1-C5-A-17_SED_014-015CM	Percent Solids	50.8	[15]	50.8	J	HT	% BY WT.
1710307	% Solids	1710307-16	OR-T1-C5-A-17_SED_015-016CM	Percent Solids	49.4	[16]	49.4	J	HT	% BY WT.
1710307	% Solids	1710307-17	OR-T1-C5-A-17_SED_016-017CM	Percent Solids	48.9	[17]	48.9	J	HT	% BY WT.
1710307	% Solids	1710307-18	OR-T1-C5-A-17_SED_017-018CM	Percent Solids	46.2	[18]	46.2	J	HT	% BY WT.
1710307	% Solids	1710307-19	OR-T1-C5-A-17_SED_018-019CM	Percent Solids	45.5	[19]	45.5	J	HT	% BY WT.
1710307	% Solids	1710307-20	OR-T1-C5-A-17_SED_019-020CM	Percent Solids	46.7	[20]	46.7	J	HT	% BY WT.
1710307	% Solids	1710307-21	OR-T1-C5-A-17_SED_020-022CM	Percent Solids	46	[21]	46	J	HT	% BY WT.
1710307	% Solids	1710307-22	OR-T1-C5-A-17_SED_022-024CM	Percent Solids	48.1	[22]	48.1	J	HT	% BY WT.
1710307	% Solids	1710307-23	OR-T1-C5-A-17_SED_024-026CM	Percent Solids	49.1	[23]	49.1	J	HT	% BY WT.
1710307	% Solids	1710307-24	OR-T1-C5-A-17_SED_026-028CM	Percent Solids	47.3	[24]	47.3	J	HT	% BY WT.
1710307	% Solids	1710307-25	OR-T1-C5-A-17_SED_028-030CM	Percent Solids	45.9	[25]	45.9	J	HT	% BY WT.
1710307	% Solids	1710307-26	OR-T1-C5-A-17_SED_030-032CM	Percent Solids	43.1	[26]	43.1	J	HT	% BY WT.
1710307	% Solids	1710307-27	OR-T1-C5-A-17_SED_032-034CM	Percent Solids	49.6	[27]	49.6	J	HT	% BY WT.
1710307	% Solids	1710307-28	OR-T1-C5-A-17_SED_034-036CM	Percent Solids	49.1	[28]	49.1	J	HT	% BY WT.
1710307	% Solids	1710307-29	OR-T1-C5-A-17_SED_036-038CM	Percent Solids	48.6	[29]	48.6	J	HT	% BY WT.
1710307	% Solids	1710307-30	OR-T1-C5-A-17_SED_038-040CM	Percent Solids	48.3	[30]	48.3	J	HT	% BY WT.
1710307	% Solids	1710307-31	OR-T1-C5-A-17_SED_040-045CM	Percent Solids	47.4	[31]	47.4	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710307	% Solids	1710307-32	OR-T1-C5-A-17_SED_045-050CM	Percent Solids	52.9	[32]	52.9	J	HT	% BY WT.
1710307	% Solids	1710307-33	OR-T1-C5-A-17_SED_050-055CM	Percent Solids	50.9	[33]	50.9	J	HT	% BY WT.
1710307	% Solids	1710307-34	OR-T1-C5-A-17_SED_055-060CM	Percent Solids	46.5	[34]	46.5	J	HT	% BY WT.
1710307	7474_1631	1710307-35	OR-T1-C5-A-17_SED_060-065CM	Mercury	252		252	J	MS-L,MS-RPD	NG/G
1710307	% Solids	1710307-35	OR-T1-C5-A-17_SED_060-065CM	Percent Solids	42.4	[35]	42.4	J	HT	% BY WT.
1710307	% Solids	1710307-36	OR-T1-C5-A-17_SED_065-070CM	Percent Solids	44.7	[36]	44.7	J	HT	% BY WT.
1710307	% Solids	1710307-37	OR-T1-C5-A-17_SED_070-075CM	Percent Solids	47.5	[37]	47.5	J	HT	% BY WT.
1710307	% Solids	1710307-38	OR-T1-C5-A-17_SED_075-080CM	Percent Solids	43.4	[38]	43.4	J	HT	% BY WT.
1710307	% Solids	1710307-39	OR-T1-C5-A-17_SED_080-085CM	Percent Solids	42.6	[39]	42.6	J	HT	% BY WT.
1710307	% Solids	1710307-40	OR-T1-C5-A-17_SED_085-090CM	Percent Solids	45.8	[40]	45.8	J	HT	% BY WT.
1710310	% Solids	1710310-01	OR-T2-C1-C-17_SED_000-001CM	Percent Solids	40.6	[1]	40.6	J	HT	% BY WT.
1710310	% Solids	1710310-02	OR-T2-C1-C-17_SED_001-002CM	Percent Solids	38.5	[2]	38.5	J	HT	% BY WT.
1710310	% Solids	1710310-03	OR-T2-C1-C-17_SED_002-003CM	Percent Solids	37.6	[3]	37.6	J	HT	% BY WT.
1710310	% Solids	1710310-04	OR-T2-C1-C-17_SED_003-004CM	Percent Solids	36	[4]	36	J	HT	% BY WT.
1710310	% Solids	1710310-05	OR-T2-C1-C-17_SED_004-005CM	Percent Solids	40.5	[5]	40.5	J	HT	% BY WT.
1710310	% Solids	1710310-06	OR-T2-C1-C-17_SED_005-006CM	Percent Solids	38.6	[6]	38.6	J	HT	% BY WT.
1710310	% Solids	1710310-07	OR-T2-C1-C-17_SED_006-007CM	Percent Solids	41.7	[7]	41.7	J	HT	% BY WT.
1710310	% Solids	1710310-08	OR-T2-C1-C-17_SED_007-008CM	Percent Solids	42.4	[8]	42.4	J	HT	% BY WT.
1710310	% Solids	1710310-09	OR-T2-C1-C-17_SED_008-009CM	Percent Solids	43.9	[9]	43.9	J	HT	% BY WT.
1710310	% Solids	1710310-10	OR-T2-C1-C-17_SED_009-010CM	Percent Solids	43.7	[10]	43.7	J	HT	% BY WT.
1710310	% Solids	1710310-11	OR-T2-C1-C-17_SED_010-011CM	Percent Solids	42.8	[11]	42.8	J	HT	% BY WT.
1710310	% Solids	1710310-12	OR-T2-C1-C-17_SED_011-012CM	Percent Solids	42	[12]	42	J	HT	% BY WT.
1710310	% Solids	1710310-13	OR-T2-C1-C-17_SED_012-013CM	Percent Solids	41.8	[13]	41.8	J	HT	% BY WT.
1710310	% Solids	1710310-14	OR-T2-C1-C-17_SED_013-014CM	Percent Solids	42.7	[14]	42.7	J	HT	% BY WT.
1710310	% Solids	1710310-15	OR-T2-C1-C-17_SED_014-015CM	Percent Solids	39	[15]	39	J	HT	% BY WT.
1710310	% Solids	1710310-16	OR-T2-C1-C-17_SED_015-016CM	Percent Solids	40.4	[16]	40.4	J	HT	% BY WT.
1710310	% Solids	1710310-17	OR-T2-C1-C-17_SED_016-017CM	Percent Solids	43.6	[17]	43.6	J	HT	% BY WT.
1710310	% Solids	1710310-18	OR-T2-C1-C-17_SED_017-018CM	Percent Solids	42.9	[18]	42.9	J	HT	% BY WT.
1710310	% Solids	1710310-19	OR-T2-C1-C-17_SED_018-019CM	Percent Solids	42.6	[19]	42.6	J	HT	% BY WT.
1710310	% Solids	1710310-20	OR-T2-C1-C-17_SED_019-020CM	Percent Solids	41.4	[20]	41.4	J	HT	% BY WT.
1710310	% Solids	1710310-21	OR-T2-C1-C-17_SED_020-022CM	Percent Solids	43.1	[21]	43.1	J	HT	% BY WT.
1710310	% Solids	1710310-22	OR-T2-C1-C-17_SED_022-024CM	Percent Solids	43.2	[22]	43.2	J	HT	% BY WT.

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710310	% Solids	1710310-23	OR-T2-C1-C-17_SED_024-026CM	Percent Solids	41.2	[23]	41.2	J	HT	% BY WT.
1710310	% Solids	1710310-24	OR-T2-C1-C-17_SED_026-028CM	Percent Solids	45.8	[24]	45.8	J	HT	% BY WT.
1710310	% Solids	1710310-25	OR-T2-C1-C-17_SED_028-030CM	Percent Solids	46.2	[25]	46.2	J	HT	% BY WT.
1710310	% Solids	1710310-26	OR-T2-C1-C-17_SED_030-032CM	Percent Solids	47.6	[26]	47.6	J	HT	% BY WT.
1710310	% Solids	1710310-27	OR-T2-C1-C-17_SED_032-034CM	Percent Solids	48.6	[27]	48.6	J	HT	% BY WT.
1710310	% Solids	1710310-28	OR-T2-C1-C-17_SED_034-036CM	Percent Solids	48.2	[28]	48.2	J	HT	% BY WT.
1710310	% Solids	1710310-29	OR-T2-C1-C-17_SED_036-038CM	Percent Solids	49.1	[29]	49.1	J	HT	% BY WT.
1710310	% Solids	1710310-30	OR-T2-C1-C-17_SED_038-040CM	Percent Solids	53.9	[30]	53.9	J	HT	% BY WT.
1710310	% Solids	1710310-31	OR-T2-C1-C-17_SED_040-045CM	Percent Solids	57.2	[31]	57.2	J	HT	% BY WT.
1710310	% Solids	1710310-32	OR-T2-C1-C-17_SED_045-050CM	Percent Solids	68.8	[32]	68.8	J	HT	% BY WT.
1710310	% Solids	1710310-33	OR-T2-C1-C-17_SED_050-055CM	Percent Solids	70.8	[33]	70.8	J	HT	% BY WT.
1710310	% Solids	1710310-34	OR-T2-C1-C-17_SED_055-060CM	Percent Solids	68.5	[34]	68.5	J	HT	% BY WT.
1710310	% Solids	1710310-35	OR-T2-C1-C-17_SED_060-065CM	Percent Solids	64.9	[35]	64.9	J	HT	% BY WT.
1710313	% Solids	1710313-01	OR-T2-C4-A-17_SED_000-001CM	Percent Solids	47.2	[1]	47.2	J	HT	% BY WT.
1710313	% Solids	1710313-02	OR-T2-C4-A-17_SED_001-002CM	Percent Solids	48	[2]	48	J	HT	% BY WT.
1710313	% Solids	1710313-03	OR-T2-C4-A-17_SED_002-003CM	Percent Solids	47.4	[3]	47.4	J	HT	% BY WT.
1710313	% Solids	1710313-04	OR-T2-C4-A-17_SED_003-004CM	Percent Solids	49.1	[4]	49.1	J	HT	% BY WT.
1710313	% Solids	1710313-05	OR-T2-C4-A-17_SED_004-005CM	Percent Solids	49.1	[5]	49.1	J	HT	% BY WT.
1710313	% Solids	1710313-06	OR-T2-C4-A-17_SED_005-006CM	Percent Solids	46.7	[6]	46.7	J	HT	% BY WT.
1710313	% Solids	1710313-07	OR-T2-C4-A-17_SED_006-007CM	Percent Solids	44.7	[7]	44.7	J	HT	% BY WT.
1710313	% Solids	1710313-08	OR-T2-C4-A-17_SED_007-008CM	Percent Solids	42.4	[8]	42.4	J	HT	% BY WT.
1710313	% Solids	1710313-09	OR-T2-C4-A-17_SED_008-009CM	Percent Solids	42.6	[9]	42.6	J	HT	% BY WT.
1710313	% Solids	1710313-10	OR-T2-C4-A-17_SED_009-010CM	Percent Solids	40.9	[10]	40.9	J	HT	% BY WT.
1710313	% Solids	1710313-11	OR-T2-C4-A-17_SED_010-011CM	Percent Solids	42.3	[11]	42.3	J	HT	% BY WT.
1710313	% Solids	1710313-12	OR-T2-C4-A-17_SED_011-012CM	Percent Solids	44.9	[12]	44.9	J	HT	% BY WT.
1710313	% Solids	1710313-13	OR-T2-C4-A-17_SED_012-013CM	Percent Solids	42	[13]	42	J	HT	% BY WT.
1710313	% Solids	1710313-14	OR-T2-C4-A-17_SED_013-014CM	Percent Solids	43.8	[14]	43.8	J	HT	% BY WT.
1710313	% Solids	1710313-15	OR-T2-C4-A-17_SED_014-015CM	Percent Solids	45.2	[15]	45.2	J	HT	% BY WT.
1710313	% Solids	1710313-16	OR-T2-C4-A-17_SED_015-016CM	Percent Solids	45.5	[16]	45.5	J	HT	% BY WT.
1710313	% Solids	1710313-17	OR-T2-C4-A-17_SED_016-017CM	Percent Solids	46.8	[17]	46.8	J	HT	% BY WT.
1710313	% Solids	1710313-18	OR-T2-C4-A-17_SED_017-018CM	Percent Solids	46	[18]	46	J	HT	% BY WT.
1710313	% Solids	1710313-19	OR-T2-C4-A-17_SED_018-019CM	Percent Solids	41.1	[19]	41.1	J	HT	% BY WT.

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710313	% Solids	1710313-20	OR-T2-C4-A-17_SED_019-020CM	Percent Solids	42	[20]	42	J	HT	% BY WT.
1710313	% Solids	1710313-21	OR-T2-C4-A-17_SED_020-022CM	Percent Solids	40.7	[21]	40.7	J	HT	% BY WT.
1710313	% Solids	1710313-22	OR-T2-C4-A-17_SED_022-024CM	Percent Solids	40	[22]	40	J	HT	% BY WT.
1710313	% Solids	1710313-23	OR-T2-C4-A-17_SED_024-026CM	Percent Solids	39	[23]	39	J	HT	% BY WT.
1710313	% Solids	1710313-24	OR-T2-C4-A-17_SED_026-028CM	Percent Solids	35.3	[24]	35.3	J	HT	% BY WT.
1710313	% Solids	1710313-25	OR-T2-C4-A-17_SED_028-030CM	Percent Solids	37.3	[25]	37.3	J	HT	% BY WT.
1710313	% Solids	1710313-26	OR-T2-C4-A-17_SED_030-032CM	Percent Solids	39	[26]	39	J	HT	% BY WT.
1710313	% Solids	1710313-27	OR-T2-C4-A-17_SED_032-034CM	Percent Solids	42.4	[27]	42.4	J	HT	% BY WT.
1710313	% Solids	1710313-28	OR-T2-C4-A-17_SED_034-036CM	Percent Solids	40.7	[28]	40.7	J	HT	% BY WT.
1710313	% Solids	1710313-29	OR-T2-C4-A-17_SED_036-038CM	Percent Solids	40.2	[29]	40.2	J	HT	% BY WT.
1710313	% Solids	1710313-30	OR-T2-C4-A-17_SED_038-040CM	Percent Solids	43.4	[30]	43.4	J	HT	% BY WT.
1710313	% Solids	1710313-31	OR-T2-C4-A-17_SED_040-045CM	Percent Solids	42.8	[31]	42.8	J	HT	% BY WT.
1710313	% Solids	1710313-32	OR-T2-C4-A-17_SED_045-050CM	Percent Solids	41.5	[32]	41.5	J	HT	% BY WT.
1710313	% Solids	1710313-33	OR-T2-C4-A-17_SED_050-055CM	Percent Solids	33.1	[33]	33.1	J	HT	% BY WT.
1710313	% Solids	1710313-34	OR-T2-C4-A-17_SED_055-060CM	Percent Solids	39.8	[34]	39.8	J	HT	% BY WT.
1710313	% Solids	1710313-35	OR-T2-C4-A-17_SED_060-065CM	Percent Solids	37.8	[35]	37.8	J	HT	% BY WT.
1710313	% Solids	1710313-36	OR-T2-C4-A-17_SED_065-070CM	Percent Solids	31.5	[36]	31.5	J	HT	% BY WT.
1710313	% Solids	1710313-37	OR-T2-C4-A-17_SED_070-075CM	Percent Solids	34.2	[37]	34.2	J	HT	% BY WT.
1710313	% Solids	1710313-38	OR-T2-C4-A-17_SED_075-080CM	Percent Solids	35.5	[38]	35.5	J	HT	% BY WT.
1710313	% Solids	1710313-39	OR-T2-C4-A-17_SED_080-085CM	Percent Solids	37.4	[39]	37.4	J	HT	% BY WT.
1710313	% Solids	1710313-40	OR-T2-C4-A-17_SED_085-090CM	Percent Solids	43	[40]	43	J	HT	% BY WT.
1710315	% Solids	1710315-01	OR-T3-C3-B-17_SED_000-001CM	Percent Solids	28.3	[1]	28.3	J	HT	% BY WT.
1710315	% Solids	1710315-02	OR-T3-C3-B-17_SED_001-002CM	Percent Solids	26.7	[2]	26.7	J	HT	% BY WT.
1710315	% Solids	1710315-03	OR-T3-C3-B-17_SED_002-003CM	Percent Solids	23.5	[3]	23.5	J	HT	% BY WT.
1710315	% Solids	1710315-04	OR-T3-C3-B-17_SED_003-004CM	Percent Solids	23.3	[4]	23.3	J	HT	% BY WT.
1710315	% Solids	1710315-05	OR-T3-C3-B-17_SED_004-005CM	Percent Solids	26.7	[5]	26.7	J	HT	% BY WT.
1710315	% Solids	1710315-06	OR-T3-C3-B-17_SED_005-006CM	Percent Solids	32	[6]	32	J	HT	% BY WT.
1710315	% Solids	1710315-07	OR-T3-C3-B-17_SED_006-007CM	Percent Solids	29.7	[7]	29.7	J	HT	% BY WT.
1710315	% Solids	1710315-08	OR-T3-C3-B-17_SED_007-008CM	Percent Solids	27.3	[8]	27.3	J	HT	% BY WT.
1710315	% Solids	1710315-09	OR-T3-C3-B-17_SED_008-009CM	Percent Solids	27.2	[9]	27.2	J	HT	% BY WT.
1710315	% Solids	1710315-10	OR-T3-C3-B-17_SED_009-010CM	Percent Solids	26.3	[10]	26.3	J	HT	% BY WT.
1710315	% Solids	1710315-11	OR-T3-C3-B-17_SED_010-011CM	Percent Solids	22.3	[11]	22.3	J	HT	% BY WT.

TABLE 2
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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710315	% Solids	1710315-12	OR-T3-C3-B-17_SED_011-012CM	Percent Solids	19.3	O-04	19.3	J	HT	% BY WT.
1710315	% Solids	1710315-13	OR-T3-C3-B-17_SED_012-013CM	Percent Solids	20.3	O-04	20.3	J	HT	% BY WT.
1710315	% Solids	1710315-14	OR-T3-C3-B-17_SED_013-014CM	Percent Solids	19.1	O-04	19.1	J	HT	% BY WT.
1710315	% Solids	1710315-15	OR-T3-C3-B-17_SED_014-015CM	Percent Solids	17.1	O-04	17.1	J	HT	% BY WT.
1710315	% Solids	1710315-16	OR-T3-C3-B-17_SED_015-016CM	Percent Solids	16.1	O-04	16.1	J	HT	% BY WT.
1710315	% Solids	1710315-17	OR-T3-C3-B-17_SED_016-017CM	Percent Solids	18.1	O-04	18.1	J	HT	% BY WT.
1710315	% Solids	1710315-18	OR-T3-C3-B-17_SED_017-018CM	Percent Solids	19.7	O-04	19.7	J	HT	% BY WT.
1710315	% Solids	1710315-19	OR-T3-C3-B-17_SED_018-019CM	Percent Solids	18.7	O-04	18.7	J	HT	% BY WT.
1710315	% Solids	1710315-20	OR-T3-C3-B-17_SED_019-020CM	Percent Solids	18.2	O-04	18.2	J	HT	% BY WT.
1710315	% Solids	1710315-21	OR-T3-C3-B-17_SED_020-022CM	Percent Solids	24.1	O-04	24.1	J	HT	% BY WT.
1710315	% Solids	1710315-22	OR-T3-C3-B-17_SED_022-024CM	Percent Solids	30.5	O-04	30.5	J	HT	% BY WT.
1710315	% Solids	1710315-23	OR-T3-C3-B-17_SED_024-026CM	Percent Solids	28.1	O-04	28.1	J	HT	% BY WT.
1710315	% Solids	1710315-24	OR-T3-C3-B-17_SED_026-028CM	Percent Solids	36	O-04	36	J	HT	% BY WT.
1710315	% Solids	1710315-25	OR-T3-C3-B-17_SED_028-030CM	Percent Solids	34.4	O-04	34.4	J	HT	% BY WT.
1710315	% Solids	1710315-26	OR-T3-C3-B-17_SED_030-032CM	Percent Solids	36	O-04	36	J	HT	% BY WT.
1710315	% Solids	1710315-27	OR-T3-C3-B-17_SED_032-034CM	Percent Solids	40.4	O-04	40.4	J	HT	% BY WT.
1710315	% Solids	1710315-28	OR-T3-C3-B-17_SED_034-036CM	Percent Solids	32.4	O-04	32.4	J	HT	% BY WT.
1710315	% Solids	1710315-29	OR-T3-C3-B-17_SED_036-038CM	Percent Solids	30.7	O-04	30.7	J	HT	% BY WT.
1710315	% Solids	1710315-30	OR-T3-C3-B-17_SED_038-040CM	Percent Solids	31.3	O-04	31.3	J	HT	% BY WT.
1710315	% Solids	1710315-31	OR-T3-C3-B-17_SED_040-045CM	Percent Solids	35.4	O-04	35.4	J	HT	% BY WT.
1710315	% Solids	1710315-32	OR-T3-C3-B-17_SED_045-050CM	Percent Solids	47	O-04	47	J	HT	% BY WT.
1710315	% Solids	1710315-33	OR-T3-C3-B-17_SED_050-055CM	Percent Solids	34.7	O-04	34.7	J	HT	% BY WT.
1710315	% Solids	1710315-34	OR-T3-C3-B-17_SED_055-060CM	Percent Solids	39.8	O-04	39.8	J	HT	% BY WT.
1710315	% Solids	1710315-35	OR-T3-C3-B-17_SED_060-065CM	Percent Solids	37.2	O-04	37.2	J	HT	% BY WT.
1710315	% Solids	1710315-36	OR-T3-C3-B-17_SED_065-070CM	Percent Solids	30.2	O-04	30.2	J	HT	% BY WT.
1710315	% Solids	1710315-37	OR-T3-C3-B-17_SED_070-075CM	Percent Solids	33	O-04	33	J	HT	% BY WT.
1710315	% Solids	1710315-38	OR-T3-C3-B-17_SED_075-080CM	Percent Solids	29.1	O-04	29.1	J	HT	% BY WT.
1710315	% Solids	1710315-39	OR-T3-C3-B-17_SED_080-085CM	Percent Solids	34	O-04	34	J	HT	% BY WT.
1710315	% Solids	1710315-40	OR-T3-C3-B-17_SED_085-090CM	Percent Solids	37.3	O-04	37.3	J	HT	% BY WT.
1710633	% Solids	1710633-01	MM-T1-C6-A-17_SED_000-001CM	Percent Solids	17.9	[1]	17.9	J	HT	% BY WT.
1710633	% Solids	1710633-02	MM-T1-C6-A-17_SED_001-002CM	Percent Solids	14.4	[2]	14.4	J	HT	% BY WT.
1710633	% Solids	1710633-03	MM-T1-C6-A-17_SED_002-003CM	Percent Solids	16.5	[3]	16.5	J	HT	% BY WT.

TABLE 2
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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710633	% Solids	1710633-04	MM-T1-C6-A-17_SED_003-004CM	Percent Solids	16	[4]	16	J	HT	% BY WT.
1710633	% Solids	1710633-05	MM-T1-C6-A-17_SED_004-005CM	Percent Solids	18.2	[5]	18.2	J	HT	% BY WT.
1710633	% Solids	1710633-06	MM-T1-C6-A-17_SED_005-006CM	Percent Solids	17.5	[6]	17.5	J	HT	% BY WT.
1710633	% Solids	1710633-07	MM-T1-C6-A-17_SED_006-007CM	Percent Solids	17	[7]	17	J	HT	% BY WT.
1710633	% Solids	1710633-08	MM-T1-C6-A-17_SED_007-008CM	Percent Solids	14	[8]	14	J	HT	% BY WT.
1710633	% Solids	1710633-09	MM-T1-C6-A-17_SED_008-009CM	Percent Solids	16.1	[9]	16.1	J	HT	% BY WT.
1710633	% Solids	1710633-10	MM-T1-C6-A-17_SED_009-010CM	Percent Solids	16.6	[10]	16.6	J	HT	% BY WT.
1710633	% Solids	1710633-11	MM-T1-C6-A-17_SED_010-011CM	Percent Solids	16.2	[11]	16.2	J	HT	% BY WT.
1710633	% Solids	1710633-12	MM-T1-C6-A-17_SED_011-012CM	Percent Solids	19.9	[12]	19.9	J	HT	% BY WT.
1710633	% Solids	1710633-13	MM-T1-C6-A-17_SED_012-013CM	Percent Solids	19.2	[13]	19.2	J	HT	% BY WT.
1710633	% Solids	1710633-14	MM-T1-C6-A-17_SED_013-014CM	Percent Solids	17.3	[14]	17.3	J	HT	% BY WT.
1710633	% Solids	1710633-15	MM-T1-C6-A-17_SED_014-015CM	Percent Solids	15.8	[15]	15.8	J	HT	% BY WT.
1710633	% Solids	1710633-16	MM-T1-C6-A-17_SED_015-016CM	Percent Solids	16.3	[16]	16.3	J	HT	% BY WT.
1710633	% Solids	1710633-17	MM-T1-C6-A-17_SED_016-017CM	Percent Solids	16.8	[17]	16.8	J	HT	% BY WT.
1710633	% Solids	1710633-18	MM-T1-C6-A-17_SED_017-018CM	Percent Solids	15.8	[18]	15.8	J	HT	% BY WT.
1710633	% Solids	1710633-19	MM-T1-C6-A-17_SED_018-019CM	Percent Solids	15.6	[19]	15.6	J	HT	% BY WT.
1710633	% Solids	1710633-20	MM-T1-C6-A-17_SED_019-020CM	Percent Solids	15	[20]	15	J	HT	% BY WT.
1710633	% Solids	1710633-21	MM-T1-C6-A-17_SED_020-022CM	Percent Solids	16.5	O-04	16.5	J	HT	% BY WT.
1710633	% Solids	1710633-22	MM-T1-C6-A-17_SED_022-024CM	Percent Solids	17.6	O-04	17.6	J	HT	% BY WT.
1710633	% Solids	1710633-23	MM-T1-C6-A-17_SED_024-026CM	Percent Solids	17	O-04	17	J	HT	% BY WT.
1710633	% Solids	1710633-24	MM-T1-C6-A-17_SED_026-028CM	Percent Solids	18.9	O-04	18.9	J	HT	% BY WT.
1710633	% Solids	1710633-25	MM-T1-C6-A-17_SED_028-030CM	Percent Solids	17.7	O-04	17.7	J	HT	% BY WT.
1710633	% Solids	1710633-26	MM-T1-C6-A-17_SED_030-032CM	Percent Solids	18.9	O-04	18.9	J	HT	% BY WT.
1710633	% Solids	1710633-27	MM-T1-C6-A-17_SED_032-034CM	Percent Solids	23.3	O-04	23.3	J	HT	% BY WT.
1710633	% Solids	1710633-28	MM-T1-C6-A-17_SED_034-036CM	Percent Solids	21.8	O-04	21.8	J	HT	% BY WT.
1710633	% Solids	1710633-29	MM-T1-C6-A-17_SED_036-038CM	Percent Solids	20.5	O-04	20.5	J	HT	% BY WT.
1710633	% Solids	1710633-30	MM-T1-C6-A-17_SED_038-040CM	Percent Solids	22.7	O-04	22.7	J	HT	% BY WT.
1710633	% Solids	1710633-31	MM-T1-C6-A-17_SED_040-045CM	Percent Solids	23.8	O-04	23.8	J	HT	% BY WT.
1710633	% Solids	1710633-32	MM-T1-C6-A-17_SED_045-050CM	Percent Solids	19.7	O-04	19.7	J	HT	% BY WT.
1710633	% Solids	1710633-33	MM-T1-C6-A-17_SED_050-055CM	Percent Solids	20.9	O-04	20.9	J	HT	% BY WT.
1710633	% Solids	1710633-34	MM-T1-C6-A-17_SED_055-060CM	Percent Solids	19.3	O-04	19.3	J	HT	% BY WT.
1710633	% Solids	1710633-35	MM-T1-C6-A-17_SED_060-065CM	Percent Solids	23.3	O-04	23.3	J	HT	% BY WT.

TABLE 2
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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710633	% Solids	1710633-36	MM-T1-C6-A-17_SED_065-070CM	Percent Solids	23	O-04	23	J	HT	% BY WT.
1710634	% Solids	1710634-01	MM-C1-C-17_SED_000-001CM	Percent Solids	41	O-04	41	J	HT	% BY WT.
1710634	% Solids	1710634-02	MM-C1-C-17_SED_001-002CM	Percent Solids	41.4	O-04	41.4	J	HT	% BY WT.
1710634	% Solids	1710634-03	MM-C1-C-17_SED_002-003CM	Percent Solids	38.6	O-04	38.6	J	HT	% BY WT.
1710634	% Solids	1710634-04	MM-C1-C-17_SED_003-004CM	Percent Solids	39.8	O-04	39.8	J	HT	% BY WT.
1710634	% Solids	1710634-05	MM-C1-C-17_SED_004-005CM	Percent Solids	37.2	[1]	37.2	J	HT	% BY WT.
1710634	% Solids	1710634-06	MM-C1-C-17_SED_005-006CM	Percent Solids	39.7	[2]	39.7	J	HT	% BY WT.
1710634	% Solids	1710634-07	MM-C1-C-17_SED_006-007CM	Percent Solids	38.9	[3]	38.9	J	HT	% BY WT.
1710634	% Solids	1710634-08	MM-C1-C-17_SED_007-008CM	Percent Solids	39.7	[4]	39.7	J	HT	% BY WT.
1710634	% Solids	1710634-09	MM-C1-C-17_SED_008-009CM	Percent Solids	42	[5]	42	J	HT	% BY WT.
1710634	% Solids	1710634-10	MM-C1-C-17_SED_009-010CM	Percent Solids	31.9	[6]	31.9	J	HT	% BY WT.
1710634	% Solids	1710634-11	MM-C1-C-17_SED_010-011CM	Percent Solids	28	[7]	28	J	HT	% BY WT.
1710634	% Solids	1710634-12	MM-C1-C-17_SED_011-012CM	Percent Solids	40.3	[8]	40.3	J	HT	% BY WT.
1710634	% Solids	1710634-13	MM-C1-C-17_SED_012-013CM	Percent Solids	43.3	[9]	43.3	J	HT	% BY WT.
1710634	% Solids	1710634-14	MM-C1-C-17_SED_013-014CM	Percent Solids	42.7	[10]	42.7	J	HT	% BY WT.
1710634	% Solids	1710634-15	MM-C1-C-17_SED_014-015CM	Percent Solids	42.1	[11]	42.1	J	HT	% BY WT.
1710634	% Solids	1710634-16	MM-C1-C-17_SED_015-016CM	Percent Solids	40	[12]	40	J	HT	% BY WT.
1710634	% Solids	1710634-17	MM-C1-C-17_SED_016-017CM	Percent Solids	32.6	[13]	32.6	J	HT	% BY WT.
1710634	% Solids	1710634-18	MM-C1-C-17_SED_017-018CM	Percent Solids	40.4	[14]	40.4	J	HT	% BY WT.
1710634	% Solids	1710634-19	MM-C1-C-17_SED_018-019CM	Percent Solids	39.5	[15]	39.5	J	HT	% BY WT.
1710634	% Solids	1710634-20	MM-C1-C-17_SED_019-020CM	Percent Solids	39.8	[16]	39.8	J	HT	% BY WT.
1710634	% Solids	1710634-21	MM-C1-C-17_SED_020-022CM	Percent Solids	42.2	[17]	42.2	J	HT	% BY WT.
1710634	% Solids	1710634-22	MM-C1-C-17_SED_022-024CM	Percent Solids	43.6	[18]	43.6	J	HT	% BY WT.
1710634	% Solids	1710634-23	MM-C1-C-17_SED_024-026CM	Percent Solids	45.6	[19]	45.6	J	HT	% BY WT.
1710634	% Solids	1710634-24	MM-C1-C-17_SED_026-028CM	Percent Solids	45	[20]	45	J	HT	% BY WT.
1710634	% Solids	1710634-25	MM-C1-C-17_SED_028-030CM	Percent Solids	41.4	[21]	41.4	J	HT	% BY WT.
1710634	% Solids	1710634-26	MM-C1-C-17_SED_030-032CM	Percent Solids	41.1	[22]	41.1	J	HT	% BY WT.
1710634	% Solids	1710634-27	MM-C1-C-17_SED_032-034CM	Percent Solids	38.2	[23]	38.2	J	HT	% BY WT.
1710634	% Solids	1710634-28	MM-C1-C-17_SED_034-036CM	Percent Solids	40.4	[24]	40.4	J	HT	% BY WT.
1710634	% Solids	1710634-29	MM-C1-C-17_SED_036-038CM	Percent Solids	41.9	[25]	41.9	J	HT	% BY WT.
1710634	% Solids	1710634-30	MM-C1-C-17_SED_038-040CM	Percent Solids	41.2	[26]	41.2	J	HT	% BY WT.
1710634	% Solids	1710634-31	MM-C1-C-17_SED_040-045CM	Percent Solids	40.2	[27]	40.2	J	HT	% BY WT.

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710634	% Solids	1710634-32	MM-C1-C-17_SED_045-050CM	Percent Solids	44.9	[28]	44.9	J	HT	% BY WT.
1710634	% Solids	1710634-33	MM-C1-C-17_SED_050-055CM	Percent Solids	42.5	[29]	42.5	J	HT	% BY WT.
1710634	% Solids	1710634-34	MM-C1-C-17_SED_055-060CM	Percent Solids	43.5	[30]	43.5	J	HT	% BY WT.
1710634	% Solids	1710634-35	MM-C1-C-17_SED_060-065CM	Percent Solids	43.8	[31]	43.8	J	HT	% BY WT.
1710634	% Solids	1710634-36	MM-C1-C-17_SED_065-070CM	Percent Solids	42	[32]	42	J	HT	% BY WT.
1710634	% Solids	1710634-37	MM-C1-C-17_SED_070-075CM	Percent Solids	44	[33]	44	J	HT	% BY WT.
1710637	7474_1631	1710637-01	MM-T1-C1-A-17_SED_000-001CM	Mercury	608		608	J	LCS-RPD	NG/G
1710637	% Solids	1710637-01	MM-T1-C1-A-17_SED_000-001CM	Percent Solids	36.9	[1]	36.9	J	HT	% BY WT.
1710637	7474_1631	1710637-02	MM-T1-C1-A-17_SED_001-002CM	Mercury	791		791	J	LCS-RPD	NG/G
1710637	% Solids	1710637-02	MM-T1-C1-A-17_SED_001-002CM	Percent Solids	32.4	[2]	32.4	J	HT	% BY WT.
1710637	7474_1631	1710637-03	MM-T1-C1-A-17_SED_002-003CM	Mercury	735		735	J	LCS-RPD	NG/G
1710637	% Solids	1710637-03	MM-T1-C1-A-17_SED_002-003CM	Percent Solids	35.7	[3]	35.7	J	HT	% BY WT.
1710637	7474_1631	1710637-04	MM-T1-C1-A-17_SED_003-004CM	Mercury	726		726	J	LCS-RPD	NG/G
1710637	% Solids	1710637-04	MM-T1-C1-A-17_SED_003-004CM	Percent Solids	39.4	[4]	39.4	J	HT	% BY WT.
1710637	7474_1631	1710637-05	MM-T1-C1-A-17_SED_004-005CM	Mercury	773		773	J	LCS-RPD	NG/G
1710637	% Solids	1710637-05	MM-T1-C1-A-17_SED_004-005CM	Percent Solids	37.9	[5]	37.9	J	HT	% BY WT.
1710637	7474_1631	1710637-06	MM-T1-C1-A-17_SED_005-006CM	Mercury	714		714	J	LCS-RPD	NG/G
1710637	% Solids	1710637-06	MM-T1-C1-A-17_SED_005-006CM	Percent Solids	29.2	[6]	29.2	J	HT	% BY WT.
1710637	7474_1631	1710637-07	MM-T1-C1-A-17_SED_006-007CM	Mercury	769		769	J	LCS-RPD	NG/G
1710637	% Solids	1710637-07	MM-T1-C1-A-17_SED_006-007CM	Percent Solids	37.4	[7]	37.4	J	HT	% BY WT.
1710637	7474_1631	1710637-08	MM-T1-C1-A-17_SED_007-008CM	Mercury	780		780	J	LCS-RPD	NG/G
1710637	% Solids	1710637-08	MM-T1-C1-A-17_SED_007-008CM	Percent Solids	36.7	O-04	36.7	J	HT	% BY WT.
1710637	7474_1631	1710637-09	MM-T1-C1-A-17_SED_008-009CM	Mercury	816		816	J	LCS-RPD	NG/G
1710637	% Solids	1710637-09	MM-T1-C1-A-17_SED_008-009CM	Percent Solids	33.9	O-04	33.9	J	HT	% BY WT.
1710637	7474_1631	1710637-10	MM-T1-C1-A-17_SED_009-010CM	Mercury	702		702	J	LCS-RPD	NG/G
1710637	% Solids	1710637-10	MM-T1-C1-A-17_SED_009-010CM	Percent Solids	35.6	O-04	35.6	J	HT	% BY WT.
1710637	7474_1631	1710637-11	MM-T1-C1-A-17_SED_010-011CM	Mercury	775		775	J	LCS-RPD	NG/G
1710637	% Solids	1710637-11	MM-T1-C1-A-17_SED_010-011CM	Percent Solids	35.9	O-04	35.9	J	HT	% BY WT.
1710637	% Solids	1710637-12	MM-T1-C1-A-17_SED_011-012CM	Percent Solids	36.7	O-04	36.7	J	HT	% BY WT.
1710637	% Solids	1710637-13	MM-T1-C1-A-17_SED_012-013CM	Percent Solids	38.1	O-04	38.1	J	HT	% BY WT.
1710637	% Solids	1710637-14	MM-T1-C1-A-17_SED_013-014CM	Percent Solids	40.6	O-04	40.6	J	HT	% BY WT.
1710637	% Solids	1710637-15	MM-T1-C1-A-17_SED_014-015CM	Percent Solids	42.1	O-04	42.1	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710637	% Solids	1710637-16	MM-T1-C1-A-17_SED_015-016CM	Percent Solids	38	O-04	38	J	HT	% BY WT.
1710637	% Solids	1710637-17	MM-T1-C1-A-17_SED_016-017CM	Percent Solids	37.7	O-04	37.7	J	HT	% BY WT.
1710637	% Solids	1710637-18	MM-T1-C1-A-17_SED_017-018CM	Percent Solids	37.2	O-04	37.2	J	HT	% BY WT.
1710637	% Solids	1710637-19	MM-T1-C1-A-17_SED_018-019CM	Percent Solids	38.4	O-04	38.4	J	HT	% BY WT.
1710637	% Solids	1710637-20	MM-T1-C1-A-17_SED_019-020CM	Percent Solids	41.1	O-04	41.1	J	HT	% BY WT.
1710637	% Solids	1710637-21	MM-T1-C1-A-17_SED_020-022CM	Percent Solids	40	O-04	40	J	HT	% BY WT.
1710637	% Solids	1710637-22	MM-T1-C1-A-17_SED_022-024CM	Percent Solids	41.8	O-04	41.8	J	HT	% BY WT.
1710637	% Solids	1710637-23	MM-T1-C1-A-17_SED_024-026CM	Percent Solids	37.4	O-04	37.4	J	HT	% BY WT.
1710637	% Solids	1710637-24	MM-T1-C1-A-17_SED_026-028CM	Percent Solids	50.1	O-04	50.1	J	HT	% BY WT.
1710637	% Solids	1710637-25	MM-T1-C1-A-17_SED_028-030CM	Percent Solids	48.2	O-04	48.2	J	HT	% BY WT.
1710637	% Solids	1710637-26	MM-T1-C1-A-17_SED_030-032CM	Percent Solids	51.6	O-04	51.6	J	HT	% BY WT.
1710637	% Solids	1710637-27	MM-T1-C1-A-17_SED_032-034CM	Percent Solids	51.6	O-04	51.6	J	HT	% BY WT.
1710637	% Solids	1710637-28	MM-T1-C1-A-17_SED_034-036CM	Percent Solids	46.7	O-04	46.7	J	HT	% BY WT.
1710637	% Solids	1710637-29	MM-T1-C1-A-17_SED_036-038CM	Percent Solids	51.1	O-04	51.1	J	HT	% BY WT.
1710637	% Solids	1710637-30	MM-T1-C1-A-17_SED_038-040CM	Percent Solids	42	O-04	42	J	HT	% BY WT.
1710637	% Solids	1710637-31	MM-T1-C1-A-17_SED_040-045CM	Percent Solids	51.1	O-04	51.1	J	HT	% BY WT.
1710637	% Solids	1710637-32	MM-T1-C1-A-17_SED_045-050CM	Percent Solids	56.4	O-04	56.4	J	HT	% BY WT.
1710637	% Solids	1710637-33	MM-T1-C1-A-17_SED_050-055CM	Percent Solids	56	O-04	56	J	HT	% BY WT.
1710637	% Solids	1710637-34	MM-T1-C1-A-17_SED_055-060CM	Percent Solids	57.7	O-04	57.7	J	HT	% BY WT.
1710637	% Solids	1710637-35	MM-T1-C1-A-17_SED_060-065CM	Percent Solids	57.1	O-04	57.1	J	HT	% BY WT.
1710637	% Solids	1710637-36	MM-T1-C1-A-17_SED_065-070CM	Percent Solids	56.9	O-04	56.9	J	HT	% BY WT.
1710637	% Solids	1710637-37	MM-T1-C1-A-17_SED_070-075CM	Percent Solids	59.1	O-04	59.1	J	HT	% BY WT.
1710639	% Solids	1710639-01	OR-T2-C3-B-17_SED_000-001CM	Percent Solids	18.4	O-04	18.4	J	HT	% BY WT.
1710639	% Solids	1710639-02	OR-T2-C3-B-17_SED_001-002CM	Percent Solids	52.5	O-04	52.5	J	HT	% BY WT.
1710639	% Solids	1710639-03	OR-T2-C3-B-17_SED_002-003CM	Percent Solids	40	O-04	40	J	HT	% BY WT.
1710639	% Solids	1710639-04	OR-T2-C3-B-17_SED_003-004CM	Percent Solids	41.8	O-04	41.8	J	HT	% BY WT.
1710639	% Solids	1710639-05	OR-T2-C3-B-17_SED_004-005CM	Percent Solids	17.1	O-04	17.1	J	HT	% BY WT.
1710639	% Solids	1710639-06	OR-T2-C3-B-17_SED_005-006CM	Percent Solids	49.9	O-04	49.9	J	HT	% BY WT.
1710639	% Solids	1710639-07	OR-T2-C3-B-17_SED_006-007CM	Percent Solids	51.2	O-04	51.2	J	HT	% BY WT.
1710639	% Solids	1710639-08	OR-T2-C3-B-17_SED_007-008CM	Percent Solids	53	O-04	53	J	HT	% BY WT.
1710639	% Solids	1710639-09	OR-T2-C3-B-17_SED_008-009CM	Percent Solids	52.4	O-04	52.4	J	HT	% BY WT.
1710639	% Solids	1710639-10	OR-T2-C3-B-17_SED_009-010CM	Percent Solids	51.7	O-04	51.7	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710639	% Solids	1710639-11	OR-T2-C3-B-17_SED_010-011CM	Percent Solids	55.1	[1]	55.1	J	HT	% BY WT.
1710639	% Solids	1710639-12	OR-T2-C3-B-17_SED_011-012CM	Percent Solids	55.7	[2]	55.7	J	HT	% BY WT.
1710639	% Solids	1710639-13	OR-T2-C3-B-17_SED_012-013CM	Percent Solids	51.4	[3]	51.4	J	HT	% BY WT.
1710639	% Solids	1710639-14	OR-T2-C3-B-17_SED_013-014CM	Percent Solids	58.7	[4]	58.7	J	HT	% BY WT.
1710639	% Solids	1710639-15	OR-T2-C3-B-17_SED_014-015CM	Percent Solids	61.3	[5]	61.3	J	HT	% BY WT.
1710639	% Solids	1710639-16	OR-T2-C3-B-17_SED_015-016CM	Percent Solids	62.6	[6]	62.6	J	HT	% BY WT.
1710639	% Solids	1710639-17	OR-T2-C3-B-17_SED_016-017CM	Percent Solids	63.4	[7]	63.4	J	HT	% BY WT.
1710639	% Solids	1710639-18	OR-T2-C3-B-17_SED_017-018CM	Percent Solids	63.8	[8]	63.8	J	HT	% BY WT.
1710639	% Solids	1710639-19	OR-T2-C3-B-17_SED_018-019CM	Percent Solids	64.5	[9]	64.5	J	HT	% BY WT.
1710639	% Solids	1710639-20	OR-T2-C3-B-17_SED_019-020CM	Percent Solids	63.8	[10]	63.8	J	HT	% BY WT.
1710639	% Solids	1710639-21	OR-T2-C3-B-17_SED_020-022CM	Percent Solids	63.6	[11]	63.6	J	HT	% BY WT.
1710639	% Solids	1710639-22	OR-T2-C3-B-17_SED_022-024CM	Percent Solids	7.1	[12]	7.1	J	HT	% BY WT.
1710639	% Solids	1710639-23	OR-T2-C3-B-17_SED_024-026CM	Percent Solids	64.6	[13]	64.6	J	HT	% BY WT.
1710639	% Solids	1710639-24	OR-T2-C3-B-17_SED_026-028CM	Percent Solids	65.8	[14]	65.8	J	HT	% BY WT.
1710639	% Solids	1710639-25	OR-T2-C3-B-17_SED_028-030CM	Percent Solids	65.5	[15]	65.5	J	HT	% BY WT.
1710639	% Solids	1710639-26	OR-T2-C3-B-17_SED_030-032CM	Percent Solids	67	[16]	67	J	HT	% BY WT.
1710639	% Solids	1710639-27	OR-T2-C3-B-17_SED_032-034CM	Percent Solids	65.3	[17]	65.3	J	HT	% BY WT.
1710639	% Solids	1710639-28	OR-T2-C3-B-17_SED_034-036CM	Percent Solids	65.8	[18]	65.8	J	HT	% BY WT.
1710639	% Solids	1710639-29	OR-T2-C3-B-17_SED_036-038CM	Percent Solids	70.6	[19]	70.6	J	HT	% BY WT.
1710639	% Solids	1710639-30	OR-T2-C3-B-17_SED_038-040CM	Percent Solids	66.8	[20]	66.8	J	HT	% BY WT.
1710639	% Solids	1710639-31	OR-T2-C3-B-17_SED_040-045CM	Percent Solids	66.5	[21]	66.5	J	HT	% BY WT.
1710639	% Solids	1710639-32	OR-T2-C3-B-17_SED_045-050CM	Percent Solids	66.4	[22]	66.4	J	HT	% BY WT.
1710639	% Solids	1710639-33	OR-T2-C3-B-17_SED_050-055CM	Percent Solids	67	[23]	67	J	HT	% BY WT.
1710639	% Solids	1710639-34	OR-T2-C3-B-17_SED_055-060CM	Percent Solids	66.6	[24]	66.6	J	HT	% BY WT.
1710639	% Solids	1710639-35	OR-T2-C3-B-17_SED_060-065CM	Percent Solids	65.2	[25]	65.2	J	HT	% BY WT.
1710639	% Solids	1710639-36	OR-T2-C3-B-17_SED_065-070CM	Percent Solids	63.7	[26]	63.7	J	HT	% BY WT.
1710641	% Solids	1710641-01	MM-T1-C5-A-17_SED_000-001CM	Percent Solids	29.5	[1]	29.5	J	HT	% BY WT.
1710641	% Solids	1710641-02	MM-T1-C5-A-17_SED_001-002CM	Percent Solids	29.4	[2]	29.4	J	HT	% BY WT.
1710641	% Solids	1710641-03	MM-T1-C5-A-17_SED_002-003CM	Percent Solids	27.2	[3]	27.2	J	HT	% BY WT.
1710641	% Solids	1710641-04	MM-T1-C5-A-17_SED_003-004CM	Percent Solids	26.1	[4]	26.1	J	HT	% BY WT.
1710641	% Solids	1710641-05	MM-T1-C5-A-17_SED_004-005CM	Percent Solids	26.3	[5]	26.3	J	HT	% BY WT.
1710641	% Solids	1710641-06	MM-T1-C5-A-17_SED_005-006CM	Percent Solids	24.9	[6]	24.9	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710641	% Solids	1710641-07	MM-T1-C5-A-17_SED_006-007CM	Percent Solids	26.1	[7]	26.1	J	HT	% BY WT.
1710641	% Solids	1710641-08	MM-T1-C5-A-17_SED_007-008CM	Percent Solids	28.2	[8]	28.2	J	HT	% BY WT.
1710641	% Solids	1710641-09	MM-T1-C5-A-17_SED_008-009CM	Percent Solids	27.9	[9]	27.9	J	HT	% BY WT.
1710641	% Solids	1710641-10	MM-T1-C5-A-17_SED_009-010CM	Percent Solids	28	[10]	28	J	HT	% BY WT.
1710641	% Solids	1710641-11	MM-T1-C5-A-17_SED_010-011CM	Percent Solids	27.7	[11]	27.7	J	HT	% BY WT.
1710641	% Solids	1710641-12	MM-T1-C5-A-17_SED_011-012CM	Percent Solids	25.4	[12]	25.4	J	HT	% BY WT.
1710641	% Solids	1710641-13	MM-T1-C5-A-17_SED_012-013CM	Percent Solids	26.3	[13]	26.3	J	HT	% BY WT.
1710641	% Solids	1710641-14	MM-T1-C5-A-17_SED_013-014CM	Percent Solids	29	[14]	29	J	HT	% BY WT.
1710641	% Solids	1710641-15	MM-T1-C5-A-17_SED_014-015CM	Percent Solids	29.8	[15]	29.8	J	HT	% BY WT.
1710641	% Solids	1710641-16	MM-T1-C5-A-17_SED_015-016CM	Percent Solids	30.9	[16]	30.9	J	HT	% BY WT.
1710641	% Solids	1710641-17	MM-T1-C5-A-17_SED_016-017CM	Percent Solids	30.7	[17]	30.7	J	HT	% BY WT.
1710641	% Solids	1710641-18	MM-T1-C5-A-17_SED_017-018CM	Percent Solids	30.3	[18]	30.3	J	HT	% BY WT.
1710641	% Solids	1710641-19	MM-T1-C5-A-17_SED_018-019CM	Percent Solids	30.6	[19]	30.6	J	HT	% BY WT.
1710641	% Solids	1710641-20	MM-T1-C5-A-17_SED_019-020CM	Percent Solids	30.2	[20]	30.2	J	HT	% BY WT.
1710641	% Solids	1710641-21	MM-T1-C5-A-17_SED_020-022CM	Percent Solids	26.7	[21]	26.7	J	HT	% BY WT.
1710641	% Solids	1710641-22	MM-T1-C5-A-17_SED_022-024CM	Percent Solids	30.9	[22]	30.9	J	HT	% BY WT.
1710641	% Solids	1710641-23	MM-T1-C5-A-17_SED_024-026CM	Percent Solids	32	[23]	32	J	HT	% BY WT.
1710641	% Solids	1710641-24	MM-T1-C5-A-17_SED_026-028CM	Percent Solids	31.9	[24]	31.9	J	HT	% BY WT.
1710641	% Solids	1710641-25	MM-T1-C5-A-17_SED_028-030CM	Percent Solids	28	[25]	28	J	HT	% BY WT.
1710641	% Solids	1710641-26	MM-T1-C5-A-17_SED_030-032CM	Percent Solids	28.8	[26]	28.8	J	HT	% BY WT.
1710641	% Solids	1710641-27	MM-T1-C5-A-17_SED_032-034CM	Percent Solids	26	[27]	26	J	HT	% BY WT.
1710641	% Solids	1710641-28	MM-T1-C5-A-17_SED_034-036CM	Percent Solids	23.9	[28]	23.9	J	HT	% BY WT.
1710641	% Solids	1710641-29	MM-T1-C5-A-17_SED_036-038CM	Percent Solids	28.5	[29]	28.5	J	HT	% BY WT.
1710641	% Solids	1710641-30	MM-T1-C5-A-17_SED_038-040CM	Percent Solids	29.3	[30]	29.3	J	HT	% BY WT.
1710641	% Solids	1710641-31	MM-T1-C5-A-17_SED_040-045CM	Percent Solids	34.4	[31]	34.4	J	HT	% BY WT.
1710641	% Solids	1710641-32	MM-T1-C5-A-17_SED_045-050CM	Percent Solids	36.3	[32]	36.3	J	HT	% BY WT.
1710641	% Solids	1710641-33	MM-T1-C5-A-17_SED_050-055CM	Percent Solids	41.4	[33]	41.4	J	HT	% BY WT.
1710641	% Solids	1710641-34	MM-T1-C5-A-17_SED_055-060CM	Percent Solids	41.8	[34]	41.8	J	HT	% BY WT.
1710641	% Solids	1710641-35	MM-T1-C5-A-17_SED_060-065CM	Percent Solids	45.3	[35]	45.3	J	HT	% BY WT.
1710641	% Solids	1710641-36	MM-T1-C5-A-17_SED_065-070CM	Percent Solids	44.6	[36]	44.6	J	HT	% BY WT.
1710682	% Solids	1710682-01	MM-T1-C4-17_SED_000-001CM	Percent Solids	37.5	[1]	37.5	J	HT	% BY WT.
1710682	% Solids	1710682-02	MM-T1-C4-17_SED_000-001CM_DUP	Percent Solids	38.3	[2]	38.3	J	HT	% BY WT.

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710682	% Solids	1710682-03	MM-T1-C4-17_SED_001-002CM	Percent Solids	37.3	[3]	37.3	J	HT	% BY WT.
1710682	% Solids	1710682-04	MM-T1-C4-17_SED_001-002CM_DUP	Percent Solids	38.2	[4]	38.2	J	HT	% BY WT.
1710682	% Solids	1710682-05	MM-T1-C4-17_SED_002-003CM	Percent Solids	35.9	[5]	35.9	J	HT	% BY WT.
1710682	% Solids	1710682-06	MM-T1-C4-17_SED_002-003CM_DUP	Percent Solids	35.7	[6]	35.7	J	HT	% BY WT.
1710682	% Solids	1710682-07	MM-T1-C4-17_SED_003-004CM	Percent Solids	36.4	[7]	36.4	J	HT	% BY WT.
1710682	% Solids	1710682-08	MM-T1-C4-17_SED_003-004CM_DUP	Percent Solids	36.8	[8]	36.8	J	HT	% BY WT.
1710682	% Solids	1710682-09	MM-T1-C4-17_SED_004-005CM	Percent Solids	35.8	[9]	35.8	J	HT	% BY WT.
1710682	% Solids	1710682-10	MM-T1-C4-17_SED_005-006CM	Percent Solids	39.7	[10]	39.7	J	HT	% BY WT.
1710682	% Solids	1710682-11	MM-T1-C4-17_SED_005-006CM_DUP	Percent Solids	39.6	[11]	39.6	J	HT	% BY WT.
1710682	% Solids	1710682-12	MM-T1-C4-17_SED_006-007CM	Percent Solids	40.4	[12]	40.4	J	HT	% BY WT.
1710682	% Solids	1710682-13	MM-T1-C4-17_SED_006-007CM_DUP	Percent Solids	39	[13]	39	J	HT	% BY WT.
1710682	% Solids	1710682-14	MM-T1-C4-17_SED_007-008CM	Percent Solids	40.7	[14]	40.7	J	HT	% BY WT.
1710682	% Solids	1710682-15	MM-T1-C4-17_SED_007-008CM_DUP	Percent Solids	39.8	[15]	39.8	J	HT	% BY WT.
1710682	% Solids	1710682-16	MM-T1-C4-17_SED_008-009CM	Percent Solids	40.7	[16]	40.7	J	HT	% BY WT.
1710682	% Solids	1710682-17	MM-T1-C4-17_SED_008-009CM_DUP	Percent Solids	40.9	[17]	40.9	J	HT	% BY WT.
1710682	% Solids	1710682-18	MM-T1-C4-17_SED_009-010CM	Percent Solids	41.2	[18]	41.2	J	HT	% BY WT.
1710682	% Solids	1710682-19	MM-T1-C4-17_SED_009-010CM_DUP	Percent Solids	43.2	O-04	43.2	J	HT	% BY WT.
1710682	% Solids	1710682-20	MM-T1-C4-17_SED_010-011CM	Percent Solids	40.1	O-04	40.1	J	HT	% BY WT.
1710682	% Solids	1710682-21	MM-T1-C4-17_SED_010-011CM_DUP	Percent Solids	40.3	O-04	40.3	J	HT	% BY WT.
1710682	% Solids	1710682-22	MM-T1-C4-17_SED_011-012CM	Percent Solids	5.9	O-04	5.9	J	HT	% BY WT.
1710682	% Solids	1710682-23	MM-T1-C4-17_SED_011-012CM_DUP	Percent Solids	6.1	O-04	6.1	J	HT	% BY WT.
1710682	% Solids	1710682-24	MM-T1-C4-17_SED_012-013CM	Percent Solids	36.8	O-04	36.8	J	HT	% BY WT.
1710682	% Solids	1710682-25	MM-T1-C4-17_SED_012-013CM_DUP	Percent Solids	37.4	O-04	37.4	J	HT	% BY WT.
1710682	% Solids	1710682-26	MM-T1-C4-17_SED_013-014CM	Percent Solids	37.4	O-04	37.4	J	HT	% BY WT.
1710682	% Solids	1710682-27	MM-T1-C4-17_SED_013-014CM_DUP	Percent Solids	37.3	O-04	37.3	J	HT	% BY WT.
1710682	% Solids	1710682-28	MM-T1-C4-17_SED_014-015CM	Percent Solids	38	O-04	38	J	HT	% BY WT.
1710682	% Solids	1710682-29	MM-T1-C4-17_SED_014-015CM_DUP	Percent Solids	38.3	O-04	38.3	J	HT	% BY WT.
1710682	% Solids	1710682-30	MM-T1-C4-17_SED_015-016CM	Percent Solids	36	O-04	36	J	HT	% BY WT.
1710682	% Solids	1710682-31	MM-T1-C4-17_SED_015-016CM_DUP	Percent Solids	35.7	O-04	35.7	J	HT	% BY WT.
1710682	% Solids	1710682-32	MM-T1-C4-17_SED_016-017CM	Percent Solids	36.7	O-04	36.7	J	HT	% BY WT.
1710682	% Solids	1710682-33	MM-T1-C4-17_SED_016-017CM_DUP	Percent Solids	36.5	O-04	36.5	J	HT	% BY WT.
1710682	% Solids	1710682-34	MM-T1-C4-17_SED_017-018CM	Percent Solids	35.9	O-04	35.9	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710682	% Solids	1710682-35	MM-T1-C4-17_SED_017-018CM_DUP	Percent Solids	37.3	O-04	37.3	J	HT	% BY WT.
1710682	% Solids	1710682-36	MM-T1-C4-17_SED_018-019CM	Percent Solids	37	O-04	37	J	HT	% BY WT.
1710682	% Solids	1710682-37	MM-T1-C4-17_SED_018-019CM_DUP	Percent Solids	36.9	O-04	36.9	J	HT	% BY WT.
1710682	% Solids	1710682-38	MM-T1-C4-17_SED_019-020CM	Percent Solids	36.8	O-04	36.8	J	HT	% BY WT.
1710682	% Solids	1710682-39	MM-T1-C4-17_SED_019-020CM_DUP	Percent Solids	37.8	O-04	37.8	J	HT	% BY WT.
1710682	% Solids	1710682-40	MM-T1-C4-17_SED_020-022CM	Percent Solids	36.6	O-04	36.6	J	HT	% BY WT.
1710682	% Solids	1710682-41	MM-T1-C4-17_SED_020-022CM_DUP	Percent Solids	37.2	O-04	37.2	J	HT	% BY WT.
1710682	% Solids	1710682-42	MM-T1-C4-17_SED_022-024CM	Percent Solids	36.2	O-04	36.2	J	HT	% BY WT.
1710682	% Solids	1710682-43	MM-T1-C4-17_SED_022-024CM_DUP	Percent Solids	37.6	O-04	37.6	J	HT	% BY WT.
1710682	% Solids	1710682-44	MM-T1-C4-17_SED_024-026CM	Percent Solids	36.7	O-04	36.7	J	HT	% BY WT.
1710682	% Solids	1710682-45	MM-T1-C4-17_SED_024-026CM_DUP	Percent Solids	37.3	O-04	37.3	J	HT	% BY WT.
1710682	% Solids	1710682-46	MM-T1-C4-17_SED_026-028CM	Percent Solids	39.4	O-04	39.4	J	HT	% BY WT.
1710682	% Solids	1710682-47	MM-T1-C4-17_SED_026-028CM_DUP	Percent Solids	39.2	O-04	39.2	J	HT	% BY WT.
1710682	% Solids	1710682-48	MM-T1-C4-17_SED_028-030CM	Percent Solids	39.2	O-04	39.2	J	HT	% BY WT.
1710682	% Solids	1710682-49	MM-T1-C4-17_SED_028-030CM_DUP	Percent Solids	38.6	O-04	38.6	J	HT	% BY WT.
1710682	% Solids	1710682-50	MM-T1-C4-17_SED_030-032CM	Percent Solids	39.9	O-04	39.9	J	HT	% BY WT.
1710682	% Solids	1710682-51	MM-T1-C4-17_SED_030-032CM_DUP	Percent Solids	40	O-04	40	J	HT	% BY WT.
1710682	% Solids	1710682-52	MM-T1-C4-17_SED_032-034CM	Percent Solids	38.1	O-04	38.1	J	HT	% BY WT.
1710682	% Solids	1710682-53	MM-T1-C4-17_SED_032-034CM_DUP	Percent Solids	39.1	O-04	39.1	J	HT	% BY WT.
1710682	% Solids	1710682-54	MM-T1-C4-17_SED_034-036CM	Percent Solids	37.7	O-04	37.7	J	HT	% BY WT.
1710682	% Solids	1710682-55	MM-T1-C4-17_SED_034-036CM_DUP	Percent Solids	39.2	O-04	39.2	J	HT	% BY WT.
1710682	% Solids	1710682-56	MM-T1-C4-17_SED_036-038CM	Percent Solids	42.7	O-04	42.7	J	HT	% BY WT.
1710682	% Solids	1710682-57	MM-T1-C4-17_SED_036-038CM_DUP	Percent Solids	42.3	O-04	42.3	J	HT	% BY WT.
1710682	% Solids	1710682-58	MM-T1-C4-17_SED_038-040CM	Percent Solids	36.7	O-04	36.7	J	HT	% BY WT.
1710682	% Solids	1710682-59	MM-T1-C4-17_SED_038-040CM_DUP	Percent Solids	38	O-04	38	J	HT	% BY WT.
1710682	% Solids	1710682-60	MM-T1-C4-17_SED_040-045CM	Percent Solids	38.9	O-04	38.9	J	HT	% BY WT.
1710682	% Solids	1710682-61	MM-T1-C4-17_SED_040-045CM_DUP	Percent Solids	38.7	O-04	38.7	J	HT	% BY WT.
1710682	7474_1631	1710682-62	MM-T1-C4-17_SED_045-050CM	Mercury	136		136	J	FD	NG/G
1710682	% Solids	1710682-62	MM-T1-C4-17_SED_045-050CM	Percent Solids	33.2	O-04	33.2	J	HT	% BY WT.
1710682	7474_1631	1710682-63	MM-T1-C4-17_SED_045-050CM_DUP	Mercury	295		295	J	FD	NG/G
1710682	% Solids	1710682-63	MM-T1-C4-17_SED_045-050CM_DUP	Percent Solids	34.9	O-04	34.9	J	HT	% BY WT.
1710682	% Solids	1710682-64	MM-T1-C4-17_SED_050-055CM	Percent Solids	43.2	O-04	43.2	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710682	% Solids	1710682-65	MM-T1-C4-17_SED_050-055CM_DUP	Percent Solids	43.4	O-04	43.4	J	HT	% BY WT.
1710682	% Solids	1710682-66	MM-T1-C4-17_SED_055-060CM	Percent Solids	44.5	O-04	44.5	J	HT	% BY WT.
1710682	% Solids	1710682-67	MM-T1-C4-17_SED_055-060CM_DUP	Percent Solids	44.7	O-04	44.7	J	HT	% BY WT.
1710682	% Solids	1710682-68	MM-T1-C4-17_SED_060-065CM	Percent Solids	45	O-04	45	J	HT	% BY WT.
1710682	% Solids	1710682-69	MM-T1-C4-17_SED_060-065CM_DUP	Percent Solids	46.1	O-04	46.1	J	HT	% BY WT.
1710682	% Solids	1710682-70	MM-T1-C4-17_SED_065-070CM	Percent Solids	48.2	O-04	48.2	J	HT	% BY WT.
1710682	% Solids	1710682-71	MM-T1-C4-17_SED_065-070CM_DUP	Percent Solids	48.1	O-04	48.1	J	HT	% BY WT.
1710682	% Solids	1710682-72	MM-T1-C4-17_SED_070-075CM	Percent Solids	47.2	O-04	47.2	J	HT	% BY WT.
1710682	% Solids	1710682-73	MM-T1-C4-17_SED_070-075CM_DUP	Percent Solids	45.7	O-04	45.7	J	HT	% BY WT.
1710682	% Solids	1710682-74	MM-T1-C4-17_SED_075-080CM	Percent Solids	55.9	O-04	55.9	J	HT	% BY WT.
1710682	% Solids	1710682-75	MM-T1-C4-17_SED_075-080CM_DUP	Percent Solids	51.4	O-04	51.4	J	HT	% BY WT.
1710682	% Solids	1710682-76	MM-T1-C4-17_SED_080-085CM	Percent Solids	55.2	O-04	55.2	J	HT	% BY WT.
1710682	% Solids	1710682-77	MM-T1-C4-17_SED_080-085CM_DUP	Percent Solids	54.9	O-04	54.9	J	HT	% BY WT.
1710684	% Solids	1710684-01	MM-T3-C3-B2-17_SED_000-001CM	Percent Solids	43.3	O-04	43.3	J	HT	% BY WT.
1710684	% Solids	1710684-02	MM-T3-C3-B2-17_SED_000-001CM_DUP	Percent Solids	41.8	[1]	41.8	J	HT	% BY WT.
1710684	% Solids	1710684-03	MM-T3-C3-B2-17_SED_001-002CM	Percent Solids	42.8	[2]	42.8	J	HT	% BY WT.
1710684	% Solids	1710684-04	MM-T3-C3-B2-17_SED_001-002CM_DUP	Percent Solids	44.2	[3]	44.2	J	HT	% BY WT.
1710684	% Solids	1710684-05	MM-T3-C3-B2-17_SED_002-003CM	Percent Solids	45.3	[4]	45.3	J	HT	% BY WT.
1710684	% Solids	1710684-06	MM-T3-C3-B2-17_SED_002-003CM_DUP	Percent Solids	46.4	[5]	46.4	J	HT	% BY WT.
1710684	% Solids	1710684-07	MM-T3-C3-B2-17_SED_003-004CM	Percent Solids	54.2	[6]	54.2	J	HT	% BY WT.
1710684	% Solids	1710684-08	MM-T3-C3-B2-17_SED_003-004CM_DUP	Percent Solids	53.3	[7]	53.3	J	HT	% BY WT.
1710684	% Solids	1710684-09	MM-T3-C3-B2-17_SED_004-005CM	Percent Solids	51.6	[8]	51.6	J	HT	% BY WT.
1710684	% Solids	1710684-10	MM-T3-C3-B2-17_SED_004-005CM_DUP	Percent Solids	52.9	[9]	52.9	J	HT	% BY WT.
1710684	% Solids	1710684-11	MM-T3-C3-B2-17_SED_005-006CM	Percent Solids	50.1	[10]	50.1	J	HT	% BY WT.
1710684	% Solids	1710684-12	MM-T3-C3-B2-17_SED_005-006CM_DUP	Percent Solids	49.2	[11]	49.2	J	HT	% BY WT.
1710684	% Solids	1710684-13	MM-T3-C3-B2-17_SED_006-007CM	Percent Solids	54.3	[12]	54.3	J	HT	% BY WT.
1710684	% Solids	1710684-14	MM-T3-C3-B2-17_SED_006-007CM_DUP	Percent Solids	54.6	[13]	54.6	J	HT	% BY WT.
1710684	% Solids	1710684-15	MM-T3-C3-B2-17_SED_007-008CM	Percent Solids	49.9	[14]	49.9	J	HT	% BY WT.
1710684	% Solids	1710684-16	MM-T3-C3-B2-17_SED_007-008CM_DUP	Percent Solids	49.7	[15]	49.7	J	HT	% BY WT.
1710684	% Solids	1710684-17	MM-T3-C3-B2-17_SED_008-009CM	Percent Solids	55.8	[16]	55.8	J	HT	% BY WT.
1710684	% Solids	1710684-18	MM-T3-C3-B2-17_SED_008-009CM_DUP	Percent Solids	56.4	[17]	56.4	J	HT	% BY WT.
1710684	% Solids	1710684-19	MM-T3-C3-B2-17_SED_009-010CM	Percent Solids	48.3	[18]	48.3	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710684	% Solids	1710684-20	MM-T3-C3-B2-17_SED_009-010CM_DUP	Percent Solids	48.4	[19]	48.4	J	HT	% BY WT.
1710684	% Solids	1710684-21	MM-T3-C3-B2-17_SED_010-011CM	Percent Solids	53.7	[20]	53.7	J	HT	% BY WT.
1710684	% Solids	1710684-22	MM-T3-C3-B2-17_SED_010-011CM_DUP	Percent Solids	54	[21]	54	J	HT	% BY WT.
1710684	% Solids	1710684-23	MM-T3-C3-B2-17_SED_011-012CM	Percent Solids	50.3	[22]	50.3	J	HT	% BY WT.
1710684	% Solids	1710684-24	MM-T3-C3-B2-17_SED_011-012CM_DUP	Percent Solids	51.3	[23]	51.3	J	HT	% BY WT.
1710684	% Solids	1710684-25	MM-T3-C3-B2-17_SED_012-013CM	Percent Solids	44.8	[24]	44.8	J	HT	% BY WT.
1710684	% Solids	1710684-26	MM-T3-C3-B2-17_SED_012-013CM_DUP	Percent Solids	45.8	[25]	45.8	J	HT	% BY WT.
1710684	% Solids	1710684-27	MM-T3-C3-B2-17_SED_013-014CM	Percent Solids	43	[26]	43	J	HT	% BY WT.
1710684	% Solids	1710684-28	MM-T3-C3-B2-17_SED_013-014CM_DUP	Percent Solids	43.7	[27]	43.7	J	HT	% BY WT.
1710684	% Solids	1710684-29	MM-T3-C3-B2-17_SED_014-015CM	Percent Solids	44.9	[28]	44.9	J	HT	% BY WT.
1710684	% Solids	1710684-30	MM-T3-C3-B2-17_SED_014-015CM_DUP	Percent Solids	43.6	[29]	43.6	J	HT	% BY WT.
1710684	% Solids	1710684-31	MM-T3-C3-B2-17_SED_015-016CM	Percent Solids	46.2	[30]	46.2	J	HT	% BY WT.
1710684	% Solids	1710684-32	MM-T3-C3-B2-17_SED_015-016CM_DUP	Percent Solids	46.3	[31]	46.3	J	HT	% BY WT.
1710684	% Solids	1710684-33	MM-T3-C3-B2-17_SED_016-017CM	Percent Solids	59.8	[32]	59.8	J	HT	% BY WT.
1710684	% Solids	1710684-34	MM-T3-C3-B2-17_SED_016-017CM_DUP	Percent Solids	59	[33]	59	J	HT	% BY WT.
1710684	% Solids	1710684-35	MM-T3-C3-B2-17_SED_017-018CM	Percent Solids	52.4	[34]	52.4	J	HT	% BY WT.
1710684	% Solids	1710684-36	MM-T3-C3-B2-17_SED_017-018CM_DUP	Percent Solids	52.6	[35]	52.6	J	HT	% BY WT.
1710684	% Solids	1710684-37	MM-T3-C3-B2-17_SED_018-019CM	Percent Solids	38.9	[36]	38.9	J	HT	% BY WT.
1710684	% Solids	1710684-38	MM-T3-C3-B2-17_SED_018-019CM_DUP	Percent Solids	37.3	[37]	37.3	J	HT	% BY WT.
1710684	% Solids	1710684-39	MM-T3-C3-B2-17_SED_019-020CM	Percent Solids	50.7	[38]	50.7	J	HT	% BY WT.
1710684	% Solids	1710684-40	MM-T3-C3-B2-17_SED_019-020CM_DUP	Percent Solids	48.7	[39]	48.7	J	HT	% BY WT.
1710684	% Solids	1710684-41	MM-T3-C3-B2-17_SED_020-022CM	Percent Solids	49	[40]	49	J	HT	% BY WT.
1710684	% Solids	1710684-42	MM-T3-C3-B2-17_SED_020-022CM_DUP	Percent Solids	48.4	[41]	48.4	J	HT	% BY WT.
1710684	% Solids	1710684-43	MM-T3-C3-B2-17_SED_022-024CM	Percent Solids	60.9	[42]	60.9	J	HT	% BY WT.
1710684	% Solids	1710684-44	MM-T3-C3-B2-17_SED_022-024CM_DUP	Percent Solids	61.4	[43]	61.4	J	HT	% BY WT.
1710684	% Solids	1710684-45	MM-T3-C3-B2-17_SED_024-026CM	Percent Solids	77.3	[44]	77.3	J	HT	% BY WT.
1710684	% Solids	1710684-46	MM-T3-C3-B2-17_SED_024-026CM_DUP	Percent Solids	77.5	[45]	77.5	J	HT	% BY WT.
1710684	% Solids	1710684-47	MM-T3-C3-B2-17_SED_026-028CM	Percent Solids	80.3	[46]	80.3	J	HT	% BY WT.
1710684	% Solids	1710684-48	MM-T3-C3-B2-17_SED_026-028CM_DUP	Percent Solids	81	[47]	81	J	HT	% BY WT.
1710684	% Solids	1710684-49	MM-T3-C3-B2-17_SED_028-030CM	Percent Solids	79.5	[48]	79.5	J	HT	% BY WT.
1710684	% Solids	1710684-50	MM-T3-C3-B2-17_SED_028-030CM_DUP	Percent Solids	79.2	[49]	79.2	J	HT	% BY WT.
1710684	% Solids	1710684-51	MM-T3-C3-B2-17_SED_030-032CM	Percent Solids	77.8	[50]	77.8	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710684	% Solids	1710684-52	MM-T3-C3-B2-17_SED_030-032CM_DUP	Percent Solids	77.5	[51]	77.5	J	HT	% BY WT.
1710684	% Solids	1710684-53	MM-T3-C3-B2-17_SED_032-034CM	Percent Solids	69.4	[52]	69.4	J	HT	% BY WT.
1710684	% Solids	1710684-54	MM-T3-C3-B2-17_SED_032-034CM_DUP	Percent Solids	69.6	[53]	69.6	J	HT	% BY WT.
1710684	% Solids	1710684-55	MM-T3-C3-B2-17_SED_034-036CM	Percent Solids	79.6	[54]	79.6	J	HT	% BY WT.
1710684	% Solids	1710684-56	MM-T3-C3-B2-17_SED_034-036CM_DUP	Percent Solids	80.1	[55]	80.1	J	HT	% BY WT.
1710684	% Solids	1710684-57	MM-T3-C3-B2-17_SED_036-038CM	Percent Solids	81.6	[56]	81.6	J	HT	% BY WT.
1710684	% Solids	1710684-58	MM-T3-C3-B2-17_SED_036-038CM_DUP	Percent Solids	81.5	[57]	81.5	J	HT	% BY WT.
1710684	% Solids	1710684-59	MM-T3-C3-B2-17_SED_038-040CM	Percent Solids	82.6	[58]	82.6	J	HT	% BY WT.
1710684	% Solids	1710684-60	MM-T3-C3-B2-17_SED_038-040CM_DUP	Percent Solids	82.2	[59]	82.2	J	HT	% BY WT.
1710684	% Solids	1710684-61	MM-T3-C3-B2-17_SED_040-045CM	Percent Solids	84.6	[60]	84.6	J	HT	% BY WT.
1710684	% Solids	1710684-62	MM-T3-C3-B2-17_SED_040-045CM_DUP	Percent Solids	84.9	[61]	84.9	J	HT	% BY WT.
1710684	% Solids	1710684-63	MM-T3-C3-B2-17_SED_045-050CM	Percent Solids	85.3	[62]	85.3	J	HT	% BY WT.
1710684	% Solids	1710684-64	MM-T3-C3-B2-17_SED_045-050CM_DUP	Percent Solids	85.2	[63]	85.2	J	HT	% BY WT.
1710684	% Solids	1710684-65	MM-T3-C3-B2-17_SED_050-055CM	Percent Solids	81	[64]	81	J	HT	% BY WT.
1710684	% Solids	1710684-66	MM-T3-C3-B2-17_SED_050-055CM_DUP	Percent Solids	80.7	[65]	80.7	J	HT	% BY WT.
1710684	% Solids	1710684-67	MM-T3-C3-B2-17_SED_055-060CM	Percent Solids	74	[66]	74	J	HT	% BY WT.
1710684	% Solids	1710684-68	MM-T3-C3-B2-17_SED_055-060CM_DUP	Percent Solids	77.6	[67]	77.6	J	HT	% BY WT.
1710684	% Solids	1710684-69	MM-T3-C3-B2-17_SED_060-065CM	Percent Solids	80	[68]	80	J	HT	% BY WT.
1710684	% Solids	1710684-70	MM-T3-C3-B2-17_SED_060-065CM_DUP	Percent Solids	79.7	[69]	79.7	J	HT	% BY WT.
1710684	% Solids	1710684-71	MM-T3-C3-B2-17_SED_065-070CM	Percent Solids	85.9	[70]	85.9	J	HT	% BY WT.
1710684	% Solids	1710684-72	MM-T3-C3-B2-17_SED_065-070CM_DUP	Percent Solids	86.2	[71]	86.2	J	HT	% BY WT.
1710684	% Solids	1710684-73	MM-T3-C3-B2-17_SED_070-075CM	Percent Solids	85.5	[72]	85.5	J	HT	% BY WT.
1710684	% Solids	1710684-74	MM-T3-C3-B2-17_SED_070-075CM_DUP	Percent Solids	84.7	[73]	84.7	J	HT	% BY WT.
1710684	% Solids	1710684-75	MM-T3-C3-B2-17_SED_075-080CM	Percent Solids	83.6	[74]	83.6	J	HT	% BY WT.
1710684	% Solids	1710684-76	MM-T3-C3-B2-17_SED_075-080CM_DUP	Percent Solids	87.1	[75]	87.1	J	HT	% BY WT.
1710685	% Solids	1710685-01	OR-T1-C3-A-17_SED_000-001CM	Percent Solids	47.4	[1]	47.4	J	HT	% BY WT.
1710685	% Solids	1710685-02	OR-T1-C3-A-17_SED_000-001CM_DUP	Percent Solids	47	[2]	47	J	HT	% BY WT.
1710685	% Solids	1710685-03	OR-T1-C3-A-17_SED_001-002CM	Percent Solids	43.2	[3]	43.2	J	HT	% BY WT.
1710685	% Solids	1710685-04	OR-T1-C3-A-17_SED_001-002CM_DUP	Percent Solids	42.4	[4]	42.4	J	HT	% BY WT.
1710685	% Solids	1710685-05	OR-T1-C3-A-17_SED_002-003CM	Percent Solids	43.9	[5]	43.9	J	HT	% BY WT.
1710685	% Solids	1710685-06	OR-T1-C3-A-17_SED_003-004CM	Percent Solids	40.2	[6]	40.2	J	HT	% BY WT.
1710685	% Solids	1710685-07	OR-T1-C3-A-17_SED_003-004CM_DUP	Percent Solids	40.4	[7]	40.4	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710685	% Solids	1710685-08	OR-T1-C3-A-17_SED_004-005CM	Percent Solids	38.8	[8]	38.8	J	HT	% BY WT.
1710685	% Solids	1710685-09	OR-T1-C3-A-17_SED_004-005CM_DUP	Percent Solids	38.8	[9]	38.8	J	HT	% BY WT.
1710685	% Solids	1710685-10	OR-T1-C3-A-17_SED_005-006CM	Percent Solids	38.9	[10]	38.9	J	HT	% BY WT.
1710685	% Solids	1710685-11	OR-T1-C3-A-17_SED_005-006CM_DUP	Percent Solids	39	[11]	39	J	HT	% BY WT.
1710685	% Solids	1710685-12	OR-T1-C3-A-17_SED_006-007CM	Percent Solids	38.1	[12]	38.1	J	HT	% BY WT.
1710685	% Solids	1710685-13	OR-T1-C3-A-17_SED_006-007CM_DUP	Percent Solids	38.4	[13]	38.4	J	HT	% BY WT.
1710685	% Solids	1710685-14	OR-T1-C3-A-17_SED_007-008CM	Percent Solids	40	[14]	40	J	HT	% BY WT.
1710685	% Solids	1710685-15	OR-T1-C3-A-17_SED_008-009CM	Percent Solids	38	[15]	38	J	HT	% BY WT.
1710685	% Solids	1710685-16	OR-T1-C3-A-17_SED_008-009CM_DUP	Percent Solids	37.7	[16]	37.7	J	HT	% BY WT.
1710685	% Solids	1710685-17	OR-T1-C3-A-17_SED_009-010CM	Percent Solids	39	[17]	39	J	HT	% BY WT.
1710685	% Solids	1710685-18	OR-T1-C3-A-17_SED_009-010CM_DUP	Percent Solids	38.9	[18]	38.9	J	HT	% BY WT.
1710685	% Solids	1710685-19	OR-T1-C3-A-17_SED_010-011CM	Percent Solids	40.2	[19]	40.2	J	HT	% BY WT.
1710685	% Solids	1710685-20	OR-T1-C3-A-17_SED_010-011CM_DUP	Percent Solids	40.4	[20]	40.4	J	HT	% BY WT.
1710685	% Solids	1710685-21	OR-T1-C3-A-17_SED_011-012CM	Percent Solids	42.3	[21]	42.3	J	HT	% BY WT.
1710685	% Solids	1710685-22	OR-T1-C3-A-17_SED_011-012CM_DUP	Percent Solids	42.8	[22]	42.8	J	HT	% BY WT.
1710685	% Solids	1710685-23	OR-T1-C3-A-17_SED_012-013CM	Percent Solids	42.1	[23]	42.1	J	HT	% BY WT.
1710685	% Solids	1710685-24	OR-T1-C3-A-17_SED_012-013CM_DUP	Percent Solids	42.4	[24]	42.4	J	HT	% BY WT.
1710685	% Solids	1710685-25	OR-T1-C3-A-17_SED_013-014CM	Percent Solids	42.6	[25]	42.6	J	HT	% BY WT.
1710685	% Solids	1710685-26	OR-T1-C3-A-17_SED_013-014CM_DUP	Percent Solids	43.6	[26]	43.6	J	HT	% BY WT.
1710685	% Solids	1710685-27	OR-T1-C3-A-17_SED_014-015CM	Percent Solids	42.2	[27]	42.2	J	HT	% BY WT.
1710685	% Solids	1710685-28	OR-T1-C3-A-17_SED_014-015CM_DUP	Percent Solids	41.9	[28]	41.9	J	HT	% BY WT.
1710685	% Solids	1710685-29	OR-T1-C3-A-17_SED_015-016CM	Percent Solids	42.2	[29]	42.2	J	HT	% BY WT.
1710685	% Solids	1710685-30	OR-T1-C3-A-17_SED_015-016CM_DUP	Percent Solids	41.8	[30]	41.8	J	HT	% BY WT.
1710685	% Solids	1710685-31	OR-T1-C3-A-17_SED_016-017CM	Percent Solids	40.6	[31]	40.6	J	HT	% BY WT.
1710685	% Solids	1710685-32	OR-T1-C3-A-17_SED_016-017CM_DUP	Percent Solids	41.1	[32]	41.1	J	HT	% BY WT.
1710685	% Solids	1710685-33	OR-T1-C3-A-17_SED_017-018CM	Percent Solids	41.3	[33]	41.3	J	HT	% BY WT.
1710685	% Solids	1710685-34	OR-T1-C3-A-17_SED_017-018CM_DUP	Percent Solids	42.5	[34]	42.5	J	HT	% BY WT.
1710685	7474_1631	1710685-35	OR-T1-C3-A-17_SED_018-019CM	Mercury	800		800	J	FD	NG/G
1710685	% Solids	1710685-35	OR-T1-C3-A-17_SED_018-019CM	Percent Solids	24.1	[35]	24.1	J	HT	% BY WT.
1710685	7474_1631	1710685-36	OR-T1-C3-A-17_SED_018-019CM_DUP	Mercury	1570		1,570	J	FD	NG/G
1710685	% Solids	1710685-36	OR-T1-C3-A-17_SED_018-019CM_DUP	Percent Solids	12.3	[36]	12.3	J	HT	% BY WT.
1710685	% Solids	1710685-37	OR-T1-C3-A-17_SED_019-020CM	Percent Solids	40.9	[37]	40.9	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710685	% Solids	1710685-38	OR-T1-C3-A-17_SED_019-020CM_DUP	Percent Solids	41	[38]	41	J	HT	% BY WT.
1710685	% Solids	1710685-39	OR-T1-C3-A-17_SED_020-022CM	Percent Solids	40.7	[39]	40.7	J	HT	% BY WT.
1710685	% Solids	1710685-40	OR-T1-C3-A-17_SED_020-022CM_DUP	Percent Solids	41	[40]	41	J	HT	% BY WT.
1710685	% Solids	1710685-41	OR-T1-C3-A-17_SED_022-024CM	Percent Solids	43.5	[41]	43.5	J	HT	% BY WT.
1710685	% Solids	1710685-42	OR-T1-C3-A-17_SED_022-024CM_DUP	Percent Solids	43.3	[42]	43.3	J	HT	% BY WT.
1710685	% Solids	1710685-43	OR-T1-C3-A-17_SED_024-026CM	Percent Solids	42.7	[43]	42.7	J	HT	% BY WT.
1710685	% Solids	1710685-44	OR-T1-C3-A-17_SED_024-026CM_DUP	Percent Solids	42.6	[44]	42.6	J	HT	% BY WT.
1710685	% Solids	1710685-45	OR-T1-C3-A-17_SED_026-028CM	Percent Solids	41.2	[45]	41.2	J	HT	% BY WT.
1710685	% Solids	1710685-46	OR-T1-C3-A-17_SED_026-028CM_DUP	Percent Solids	41	[46]	41	J	HT	% BY WT.
1710685	% Solids	1710685-47	OR-T1-C3-A-17_SED_028-030CM	Percent Solids	41.6	[47]	41.6	J	HT	% BY WT.
1710685	% Solids	1710685-48	OR-T1-C3-A-17_SED_028-030CM_DUP	Percent Solids	41.4	[48]	41.4	J	HT	% BY WT.
1710685	% Solids	1710685-49	OR-T1-C3-A-17_SED_030-032CM	Percent Solids	40.9	[49]	40.9	J	HT	% BY WT.
1710685	% Solids	1710685-50	OR-T1-C3-A-17_SED_030-032CM_DUP	Percent Solids	41.4	[50]	41.4	J	HT	% BY WT.
1710685	% Solids	1710685-51	OR-T1-C3-A-17_SED_032-034CM	Percent Solids	41.3	[51]	41.3	J	HT	% BY WT.
1710685	% Solids	1710685-52	OR-T1-C3-A-17_SED_032-034CM_DUP	Percent Solids	41.5	[52]	41.5	J	HT	% BY WT.
1710685	% Solids	1710685-53	OR-T1-C3-A-17_SED_034-036CM	Percent Solids	32.4	[53]	32.4	J	HT	% BY WT.
1710685	% Solids	1710685-54	OR-T1-C3-A-17_SED_034-036CM_DUP	Percent Solids	32.8	[54]	32.8	J	HT	% BY WT.
1710685	% Solids	1710685-55	OR-T1-C3-A-17_SED_036-038CM	Percent Solids	40.2	[55]	40.2	J	HT	% BY WT.
1710685	% Solids	1710685-56	OR-T1-C3-A-17_SED_036-038CM_DUP	Percent Solids	40.3	[56]	40.3	J	HT	% BY WT.
1710685	% Solids	1710685-57	OR-T1-C3-A-17_SED_038-040CM	Percent Solids	39.7	[57]	39.7	J	HT	% BY WT.
1710685	% Solids	1710685-58	OR-T1-C3-A-17_SED_038-040CM_DUP	Percent Solids	39.6	[58]	39.6	J	HT	% BY WT.
1710685	% Solids	1710685-59	OR-T1-C3-A-17_SED_040-045CM	Percent Solids	39.4	[59]	39.4	J	HT	% BY WT.
1710685	% Solids	1710685-60	OR-T1-C3-A-17_SED_040-045CM_DUP	Percent Solids	39.7	[60]	39.7	J	HT	% BY WT.
1710685	% Solids	1710685-61	OR-T1-C3-A-17_SED_045-050CM	Percent Solids	42.2	[61]	42.2	J	HT	% BY WT.
1710685	% Solids	1710685-62	OR-T1-C3-A-17_SED_045-050CM_DUP	Percent Solids	42.1	[62]	42.1	J	HT	% BY WT.
1710685	% Solids	1710685-63	OR-T1-C3-A-17_SED_050-055CM	Percent Solids	42.6	[63]	42.6	J	HT	% BY WT.
1710685	% Solids	1710685-64	OR-T1-C3-A-17_SED_050-055CM_DUP	Percent Solids	42.7	[64]	42.7	J	HT	% BY WT.
1710685	% Solids	1710685-65	OR-T1-C3-A-17_SED_055-060CM	Percent Solids	50.2	[65]	50.2	J	HT	% BY WT.
1710685	% Solids	1710685-66	OR-T1-C3-A-17_SED_055-060CM_DUP	Percent Solids	50.1	[66]	50.1	J	HT	% BY WT.
1710685	% Solids	1710685-67	OR-T1-C3-A-17_SED_060-065CM	Percent Solids	42.9	[67]	42.9	J	HT	% BY WT.
1710685	% Solids	1710685-68	OR-T1-C3-A-17_SED_060-065CM_DUP	Percent Solids	41.9	[68]	41.9	J	HT	% BY WT.
1710685	% Solids	1710685-69	OR-T1-C3-A-17_SED_065-070CM	Percent Solids	44	[69]	44	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710685	% Solids	1710685-70	OR-T1-C3-A-17_SED_065-070CM_DUP	Percent Solids	44.5	[70]	44.5	J	HT	% BY WT.
1710685	% Solids	1710685-71	OR-T1-C3-A-17_SED_070-075CM	Percent Solids	45.3	[71]	45.3	J	HT	% BY WT.
1710685	% Solids	1710685-72	OR-T1-C3-A-17_SED_070-075CM_DUP	Percent Solids	44.9	[72]	44.9	J	HT	% BY WT.
1710685	% Solids	1710685-73	OR-T1-C3-A-17_SED_075-080CM	Percent Solids	42	[73]	42	J	HT	% BY WT.
1710685	% Solids	1710685-74	OR-T1-C3-A-17_SED_075-080CM_DUP	Percent Solids	43.1	[74]	43.1	J	HT	% BY WT.
1710685	% Solids	1710685-75	OR-T1-C3-A-17_SED_080-085CM	Percent Solids	44.2	[75]	44.2	J	HT	% BY WT.
1710685	% Solids	1710685-76	OR-T1-C3-A-17_SED_080-085CM_DUP	Percent Solids	44.5	[76]	44.5	J	HT	% BY WT.
1710685	% Solids	1710685-77	OR-T1-C3-A-17_SED_085-090CM	Percent Solids	47.7	[77]	47.7	J	HT	% BY WT.
1710685	% Solids	1710685-78	OR-T1-C3-A-17_SED_085-090CM_DUP	Percent Solids	48.8	[78]	48.8	J	HT	% BY WT.
1710685	% Solids	1710685-79	OR-T1-C3-A-17_SED_090-095CM	Percent Solids	51	[79]	51	J	HT	% BY WT.
1710685	% Solids	1710685-80	OR-T1-C3-A-17_SED_090-095CM_DUP	Percent Solids	51.6	[80]	51.6	J	HT	% BY WT.
1710685	% Solids	1710685-81	OR-T1-C3-A-17_SED_095-101CM	Percent Solids	55.2	[81]	55.2	J	HT	% BY WT.
1710685	% Solids	1710685-82	OR-T1-C3-A-17_SED_095-101CM_DUP	Percent Solids	51.4	[82]	51.4	J	HT	% BY WT.
1710728	% Solids	1710728-01	MM-T3-C6-17_SED_000-001CM	Percent Solids	23.2	[1]	23.2	J	HT	% BY WT.
1710728	% Solids	1710728-02	MM-T3-C6-17_SED_001-002CM	Percent Solids	22.4	[2]	22.4	J	HT	% BY WT.
1710728	% Solids	1710728-03	MM-T3-C6-17_SED_002-003CM	Percent Solids	23.9	[3]	23.9	J	HT	% BY WT.
1710728	% Solids	1710728-04	MM-T3-C6-17_SED_003-004CM	Percent Solids	19.4	O-04	19.4	J	HT	% BY WT.
1710728	% Solids	1710728-05	MM-T3-C6-17_SED_004-005CM	Percent Solids	19.8	O-04	19.8	J	HT	% BY WT.
1710728	% Solids	1710728-06	MM-T3-C6-17_SED_005-006CM	Percent Solids	20	O-04	20	J	HT	% BY WT.
1710728	% Solids	1710728-07	MM-T3-C6-17_SED_006-007CM	Percent Solids	31.2	O-04	31.2	J	HT	% BY WT.
1710728	% Solids	1710728-08	MM-T3-C6-17_SED_007-008CM	Percent Solids	24.5	O-04	24.5	J	HT	% BY WT.
1710728	% Solids	1710728-09	MM-T3-C6-17_SED_008-009CM	Percent Solids	30.5	O-04	30.5	J	HT	% BY WT.
1710728	% Solids	1710728-10	MM-T3-C6-17_SED_009-010CM	Percent Solids	31.5	O-04	31.5	J	HT	% BY WT.
1710728	% Solids	1710728-11	MM-T3-C6-17_SED_010-011CM	Percent Solids	22.5	O-04	22.5	J	HT	% BY WT.
1710728	% Solids	1710728-12	MM-T3-C6-17_SED_011-012CM	Percent Solids	21.6	O-04	21.6	J	HT	% BY WT.
1710728	% Solids	1710728-13	MM-T3-C6-17_SED_012-013CM	Percent Solids	20.6	O-04	20.6	J	HT	% BY WT.
1710728	% Solids	1710728-14	MM-T3-C6-17_SED_013-014CM	Percent Solids	22.5	O-04	22.5	J	HT	% BY WT.
1710728	% Solids	1710728-15	MM-T3-C6-17_SED_014-015CM	Percent Solids	25.6	O-04	25.6	J	HT	% BY WT.
1710728	% Solids	1710728-16	MM-T3-C6-17_SED_015-016CM	Percent Solids	27.9	O-04	27.9	J	HT	% BY WT.
1710728	% Solids	1710728-17	MM-T3-C6-17_SED_016-017CM	Percent Solids	28.5	O-04	28.5	J	HT	% BY WT.
1710728	% Solids	1710728-18	MM-T3-C6-17_SED_017-018CM	Percent Solids	30.1	O-04	30.1	J	HT	% BY WT.
1710728	% Solids	1710728-19	MM-T3-C6-17_SED_018-019CM	Percent Solids	28.6	O-04	28.6	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710728	% Solids	1710728-20	MM-T3-C6-17_SED_019-020CM	Percent Solids	28.6	O-04	28.6	J	HT	% BY WT.
1710728	% Solids	1710728-21	MM-T3-C6-17_SED_020-022CM	Percent Solids	28.7	O-04	28.7	J	HT	% BY WT.
1710728	% Solids	1710728-22	MM-T3-C6-17_SED_022-024CM	Percent Solids	31.8	O-04	31.8	J	HT	% BY WT.
1710728	% Solids	1710728-23	MM-T3-C6-17_SED_024-026CM	Percent Solids	34.7	O-04	34.7	J	HT	% BY WT.
1710728	% Solids	1710728-24	MM-T3-C6-17_SED_026-028CM	Percent Solids	32.5	O-04	32.5	J	HT	% BY WT.
1710728	% Solids	1710728-25	MM-T3-C6-17_SED_028-030CM	Percent Solids	38.5	O-04	38.5	J	HT	% BY WT.
1710728	% Solids	1710728-26	MM-T3-C6-17_SED_030-032CM	Percent Solids	38.3	O-04	38.3	J	HT	% BY WT.
1710728	% Solids	1710728-27	MM-T3-C6-17_SED_032-034CM	Percent Solids	37.2	O-04	37.2	J	HT	% BY WT.
1710728	% Solids	1710728-28	MM-T3-C6-17_SED_034-036CM	Percent Solids	34.4	O-04	34.4	J	HT	% BY WT.
1710728	% Solids	1710728-29	MM-T3-C6-17_SED_036-038CM	Percent Solids	41.6	O-04	41.6	J	HT	% BY WT.
1710728	% Solids	1710728-30	MM-T3-C6-17_SED_038-040CM	Percent Solids	40.6	O-04	40.6	J	HT	% BY WT.
1710728	% Solids	1710728-31	MM-T3-C6-17_SED_040-045CM	Percent Solids	37.6	O-04	37.6	J	HT	% BY WT.
1710728	% Solids	1710728-32	MM-T3-C6-17_SED_045-050CM	Percent Solids	37.8	O-04	37.8	J	HT	% BY WT.
1710728	% Solids	1710728-33	MM-T3-C6-17_SED_050-055CM	Percent Solids	37.9	O-04	37.9	J	HT	% BY WT.
1710728	% Solids	1710728-34	MM-T3-C6-17_SED_055-060CM	Percent Solids	28.5	O-04	28.5	J	HT	% BY WT.
1710728	% Solids	1710728-35	MM-T3-C6-17_SED_060-065CM	Percent Solids	28.2	O-04	28.2	J	HT	% BY WT.
1710728	% Solids	1710728-36	MM-T3-C6-17_SED_065-070CM	Percent Solids	27.8	O-04	27.8	J	HT	% BY WT.
1710729	% Solids	1710729-01	MM-T5-C2-17_SED_000-001CM	Percent Solids	41	O-04	41	J	HT	% BY WT.
1710729	% Solids	1710729-02	MM-T5-C2-17_SED_001-002CM	Percent Solids	43.9	O-04	43.9	J	HT	% BY WT.
1710729	% Solids	1710729-03	MM-T5-C2-17_SED_002-003CM	Percent Solids	45.9	O-04	45.9	J	HT	% BY WT.
1710729	% Solids	1710729-04	MM-T5-C2-17_SED_003-004CM	Percent Solids	47.2	O-04	47.2	J	HT	% BY WT.
1710729	% Solids	1710729-05	MM-T5-C2-17_SED_004-005CM	Percent Solids	47.6	O-04	47.6	J	HT	% BY WT.
1710729	% Solids	1710729-06	MM-T5-C2-17_SED_005-006CM	Percent Solids	48.7	O-04	48.7	J	HT	% BY WT.
1710729	% Solids	1710729-07	MM-T5-C2-17_SED_006-007CM	Percent Solids	48	O-04	48	J	HT	% BY WT.
1710729	% Solids	1710729-08	MM-T5-C2-17_SED_007-008CM	Percent Solids	50.1	[1]	50.1	J	HT	% BY WT.
1710729	% Solids	1710729-09	MM-T5-C2-17_SED_008-009CM	Percent Solids	47.7	[2]	47.7	J	HT	% BY WT.
1710729	% Solids	1710729-10	MM-T5-C2-17_SED_009-010CM	Percent Solids	44.7	[3]	44.7	J	HT	% BY WT.
1710729	% Solids	1710729-11	MM-T5-C2-17_SED_010-011CM	Percent Solids	45.1	[4]	45.1	J	HT	% BY WT.
1710729	% Solids	1710729-12	MM-T5-C2-17_SED_011-012CM	Percent Solids	42.5	[5]	42.5	J	HT	% BY WT.
1710729	% Solids	1710729-13	MM-T5-C2-17_SED_012-013CM	Percent Solids	40.4	[6]	40.4	J	HT	% BY WT.
1710729	% Solids	1710729-14	MM-T5-C2-17_SED_013-014CM	Percent Solids	38	[7]	38	J	HT	% BY WT.
1710729	% Solids	1710729-15	MM-T5-C2-17_SED_014-015CM	Percent Solids	38.8	[8]	38.8	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710729	% Solids	1710729-16	MM-T5-C2-17_SED_015-016CM	Percent Solids	40.5	[9]	40.5	J	HT	% BY WT.
1710729	% Solids	1710729-17	MM-T5-C2-17_SED_016-017CM	Percent Solids	49.7	[10]	49.7	J	HT	% BY WT.
1710729	% Solids	1710729-18	MM-T5-C2-17_SED_017-018CM	Percent Solids	50.7	[11]	50.7	J	HT	% BY WT.
1710729	% Solids	1710729-19	MM-T5-C2-17_SED_018-019CM	Percent Solids	48.1	[12]	48.1	J	HT	% BY WT.
1710729	% Solids	1710729-20	MM-T5-C2-17_SED_019-020CM	Percent Solids	45.9	[13]	45.9	J	HT	% BY WT.
1710729	% Solids	1710729-21	MM-T5-C2-17_SED_020-022CM	Percent Solids	48.1	[14]	48.1	J	HT	% BY WT.
1710729	% Solids	1710729-22	MM-T5-C2-17_SED_022-024CM	Percent Solids	53	[15]	53	J	HT	% BY WT.
1710729	% Solids	1710729-23	MM-T5-C2-17_SED_024-026CM	Percent Solids	51.1	[16]	51.1	J	HT	% BY WT.
1710729	% Solids	1710729-24	MM-T5-C2-17_SED_026-028CM	Percent Solids	48.9	[17]	48.9	J	HT	% BY WT.
1710729	% Solids	1710729-25	MM-T5-C2-17_SED_028-030CM	Percent Solids	47.5	[18]	47.5	J	HT	% BY WT.
1710729	% Solids	1710729-26	MM-T5-C2-17_SED_030-032CM	Percent Solids	46.7	[19]	46.7	J	HT	% BY WT.
1710729	% Solids	1710729-27	MM-T5-C2-17_SED_032-034CM	Percent Solids	47.6	[20]	47.6	J	HT	% BY WT.
1710729	% Solids	1710729-28	MM-T5-C2-17_SED_034-036CM	Percent Solids	48.3	[21]	48.3	J	HT	% BY WT.
1710729	% Solids	1710729-29	MM-T5-C2-17_SED_036-038CM	Percent Solids	47.6	[22]	47.6	J	HT	% BY WT.
1710729	% Solids	1710729-30	MM-T5-C2-17_SED_038-040CM	Percent Solids	49.7	[23]	49.7	J	HT	% BY WT.
1710729	% Solids	1710729-31	MM-T5-C2-17_SED_040-045CM	Percent Solids	52.3	[24]	52.3	J	HT	% BY WT.
1710729	% Solids	1710729-32	MM-T5-C2-17_SED_045-050CM	Percent Solids	56.8	[25]	56.8	J	HT	% BY WT.
1710729	% Solids	1710729-33	MM-T5-C2-17_SED_050-055CM	Percent Solids	64	[26]	64	J	HT	% BY WT.
1710729	% Solids	1710729-34	MM-T5-C2-17_SED_055-060CM	Percent Solids	69.5	[27]	69.5	J	HT	% BY WT.
1710729	% Solids	1710729-35	MM-T5-C2-17_SED_060-065CM	Percent Solids	66.6	[28]	66.6	J	HT	% BY WT.
1710730	% Solids	1710730-01	MM-T4-C6-17_SED_000-001CM	Percent Solids	40.2	[1]	40.2	J	HT	% BY WT.
1710730	% Solids	1710730-02	MM-T4-C6-17_SED_001-002CM	Percent Solids	42	[2]	42	J	HT	% BY WT.
1710730	% Solids	1710730-03	MM-T4-C6-17_SED_002-003CM	Percent Solids	41.2	[3]	41.2	J	HT	% BY WT.
1710730	% Solids	1710730-04	MM-T4-C6-17_SED_003-004CM	Percent Solids	41.9	[4]	41.9	J	HT	% BY WT.
1710730	% Solids	1710730-05	MM-T4-C6-17_SED_004-005CM	Percent Solids	42.7	[5]	42.7	J	HT	% BY WT.
1710730	% Solids	1710730-06	MM-T4-C6-17_SED_005-006CM	Percent Solids	43.7	[6]	43.7	J	HT	% BY WT.
1710730	% Solids	1710730-07	MM-T4-C6-17_SED_006-007CM	Percent Solids	43.8	[7]	43.8	J	HT	% BY WT.
1710730	% Solids	1710730-08	MM-T4-C6-17_SED_007-008CM	Percent Solids	42.3	[8]	42.3	J	HT	% BY WT.
1710730	% Solids	1710730-09	MM-T4-C6-17_SED_008-009CM	Percent Solids	42.5	[9]	42.5	J	HT	% BY WT.
1710730	% Solids	1710730-10	MM-T4-C6-17_SED_009-010CM	Percent Solids	45.3	[10]	45.3	J	HT	% BY WT.
1710730	% Solids	1710730-11	MM-T4-C6-17_SED_010-011CM	Percent Solids	45.3	[11]	45.3	J	HT	% BY WT.
1710730	% Solids	1710730-12	MM-T4-C6-17_SED_011-012CM	Percent Solids	45.8	[12]	45.8	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710730	% Solids	1710730-13	MM-T4-C6-17_SED_012-013CM	Percent Solids	45.9	[13]	45.9	J	HT	% BY WT.
1710730	% Solids	1710730-14	MM-T4-C6-17_SED_013-014CM	Percent Solids	45.5	[14]	45.5	J	HT	% BY WT.
1710730	% Solids	1710730-15	MM-T4-C6-17_SED_014-015CM	Percent Solids	42	[15]	42	J	HT	% BY WT.
1710730	% Solids	1710730-16	MM-T4-C6-17_SED_015-016CM	Percent Solids	42.2	[16]	42.2	J	HT	% BY WT.
1710730	% Solids	1710730-17	MM-T4-C6-17_SED_016-017CM	Percent Solids	42	[17]	42	J	HT	% BY WT.
1710730	7474_1631	1710730-18	MM-T4-C6-17_SED_017-018CM	Mercury	2960		2,960	J	MS-L	NG/G
1710730	% Solids	1710730-18	MM-T4-C6-17_SED_017-018CM	Percent Solids	42.5	[18]	42.5	J	HT	% BY WT.
1710730	% Solids	1710730-19	MM-T4-C6-17_SED_018-019CM	Percent Solids	43.5	[19]	43.5	J	HT	% BY WT.
1710730	% Solids	1710730-20	MM-T4-C6-17_SED_019-020CM	Percent Solids	42.5	[20]	42.5	J	HT	% BY WT.
1710730	% Solids	1710730-21	MM-T4-C6-17_SED_020-022CM	Percent Solids	42.5	[21]	42.5	J	HT	% BY WT.
1710730	% Solids	1710730-22	MM-T4-C6-17_SED_022-024CM	Percent Solids	40.1	[22]	40.1	J	HT	% BY WT.
1710730	% Solids	1710730-23	MM-T4-C6-17_SED_024-026CM	Percent Solids	42.3	[23]	42.3	J	HT	% BY WT.
1710730	% Solids	1710730-24	MM-T4-C6-17_SED_026-028CM	Percent Solids	41.3	[24]	41.3	J	HT	% BY WT.
1710730	% Solids	1710730-25	MM-T4-C6-17_SED_028-030CM	Percent Solids	39.8	[25]	39.8	J	HT	% BY WT.
1710730	% Solids	1710730-26	MM-T4-C6-17_SED_030-032CM	Percent Solids	35.8	[26]	35.8	J	HT	% BY WT.
1710730	% Solids	1710730-27	MM-T4-C6-17_SED_032-034CM	Percent Solids	41	[27]	41	J	HT	% BY WT.
1710730	% Solids	1710730-28	MM-T4-C6-17_SED_034-036CM	Percent Solids	39.4	[28]	39.4	J	HT	% BY WT.
1710730	% Solids	1710730-29	MM-T4-C6-17_SED_036-038CM	Percent Solids	41.7	[29]	41.7	J	HT	% BY WT.
1710730	% Solids	1710730-30	MM-T4-C6-17_SED_038-040CM	Percent Solids	42.3	[30]	42.3	J	HT	% BY WT.
1710730	% Solids	1710730-31	MM-T4-C6-17_SED_040-045CM	Percent Solids	45.8	[31]	45.8	J	HT	% BY WT.
1710730	% Solids	1710730-32	MM-T4-C6-17_SED_045-050CM	Percent Solids	50.1	[32]	50.1	J	HT	% BY WT.
1710730	% Solids	1710730-33	MM-T4-C6-17_SED_050-055CM	Percent Solids	48.9	[33]	48.9	J	HT	% BY WT.
1710730	% Solids	1710730-34	MM-T4-C6-17_SED_055-060CM	Percent Solids	48.7	[34]	48.7	J	HT	% BY WT.
1710730	% Solids	1710730-35	MM-T4-C6-17_SED_060-065CM	Percent Solids	48.3	[35]	48.3	J	HT	% BY WT.
1710730	% Solids	1710730-36	MM-T4-C6-17_SED_065-070CM	Percent Solids	51.1	[36]	51.1	J	HT	% BY WT.
1710730	% Solids	1710730-37	MM-T4-C6-17_SED_070-075CM	Percent Solids	54.8	[37]	54.8	J	HT	% BY WT.
1710730	% Solids	1710730-38	MM-T4-C6-17_SED_075-080CM	Percent Solids	56.6	[38]	56.6	J	HT	% BY WT.
1710731	% Solids	1710731-01	MM-T4-C5-17_SED_000-001CM	Percent Solids	26.5	[1]	26.5	J	HT	% BY WT.
1710731	% Solids	1710731-02	MM-T4-C5-17_SED_001-002CM	Percent Solids	26.1	[2]	26.1	J	HT	% BY WT.
1710731	% Solids	1710731-03	MM-T4-C5-17_SED_002-003CM	Percent Solids	24.5	[3]	24.5	J	HT	% BY WT.
1710731	% Solids	1710731-04	MM-T4-C5-17_SED_003-004CM	Percent Solids	22	[4]	22	J	HT	% BY WT.
1710731	% Solids	1710731-05	MM-T4-C5-17_SED_004-005CM	Percent Solids	24.1	[5]	24.1	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710731	% Solids	1710731-06	MM-T4-C5-17_SED_005-006CM	Percent Solids	22.8	[6]	22.8	J	HT,LD	% BY WT.
1710731	% Solids	1710731-07	MM-T4-C5-17_SED_006-007CM	Percent Solids	23.4	[7]	23.4	J	HT	% BY WT.
1710731	% Solids	1710731-08	MM-T4-C5-17_SED_007-008CM	Percent Solids	24.7	[8]	24.7	J	HT	% BY WT.
1710731	% Solids	1710731-09	MM-T4-C5-17_SED_008-009CM	Percent Solids	30.1	[9]	30.1	J	HT	% BY WT.
1710731	% Solids	1710731-10	MM-T4-C5-17_SED_009-010CM	Percent Solids	29.4	[10]	29.4	J	HT	% BY WT.
1710731	% Solids	1710731-11	MM-T4-C5-17_SED_010-011CM	Percent Solids	27	[11]	27	J	HT	% BY WT.
1710731	% Solids	1710731-12	MM-T4-C5-17_SED_011-012CM	Percent Solids	27.4	[12]	27.4	J	HT	% BY WT.
1710731	% Solids	1710731-13	MM-T4-C5-17_SED_012-013CM	Percent Solids	27.2	[13]	27.2	J	HT	% BY WT.
1710731	% Solids	1710731-14	MM-T4-C5-17_SED_013-014CM	Percent Solids	27.6	[14]	27.6	J	HT	% BY WT.
1710731	% Solids	1710731-15	MM-T4-C5-17_SED_014-015CM	Percent Solids	26.6	[15]	26.6	J	HT	% BY WT.
1710731	% Solids	1710731-16	MM-T4-C5-17_SED_015-016CM	Percent Solids	26.1	[16]	26.1	J	HT	% BY WT.
1710731	% Solids	1710731-17	MM-T4-C5-17_SED_016-017CM	Percent Solids	27.7	[17]	27.7	J	HT	% BY WT.
1710731	% Solids	1710731-18	MM-T4-C5-17_SED_017-018CM	Percent Solids	29.1	[18]	29.1	J	HT	% BY WT.
1710731	% Solids	1710731-19	MM-T4-C5-17_SED_018-019CM	Percent Solids	32.5	[19]	32.5	J	HT	% BY WT.
1710731	% Solids	1710731-20	MM-T4-C5-17_SED_019-020CM	Percent Solids	33.1	[20]	33.1	J	HT	% BY WT.
1710731	% Solids	1710731-21	MM-T4-C5-17_SED_020-022CM	Percent Solids	36.7	[21]	36.7	J	HT	% BY WT.
1710731	% Solids	1710731-22	MM-T4-C5-17_SED_022-024CM	Percent Solids	31.3	[22]	31.3	J	HT	% BY WT.
1710731	% Solids	1710731-23	MM-T4-C5-17_SED_024-026CM	Percent Solids	33.9	[23]	33.9	J	HT	% BY WT.
1710731	% Solids	1710731-24	MM-T4-C5-17_SED_026-028CM	Percent Solids	37.5	[24]	37.5	J	HT	% BY WT.
1710731	% Solids	1710731-25	MM-T4-C5-17_SED_028-030CM	Percent Solids	39.5	[25]	39.5	J	HT	% BY WT.
1710731	% Solids	1710731-26	MM-T4-C5-17_SED_030-032CM	Percent Solids	37.3	[26]	37.3	J	HT	% BY WT.
1710731	% Solids	1710731-27	MM-T4-C5-17_SED_032-034CM	Percent Solids	38.4	[27]	38.4	J	HT	% BY WT.
1710731	% Solids	1710731-28	MM-T4-C5-17_SED_034-036CM	Percent Solids	34.5	[28]	34.5	J	HT	% BY WT.
1710731	% Solids	1710731-29	MM-T4-C5-17_SED_036-038CM	Percent Solids	33.7	[29]	33.7	J	HT	% BY WT.
1710731	% Solids	1710731-30	MM-T4-C5-17_SED_038-040CM	Percent Solids	39.2	[30]	39.2	J	HT	% BY WT.
1710731	% Solids	1710731-31	MM-T4-C5-17_SED_040-045CM	Percent Solids	43.8	[31]	43.8	J	HT	% BY WT.
1710731	% Solids	1710731-32	MM-T4-C5-17_SED_045-050CM	Percent Solids	42.6	[32]	42.6	J	HT	% BY WT.
1710731	% Solids	1710731-33	MM-T4-C5-17_SED_050-055CM	Percent Solids	49.1	[33]	49.1	J	HT	% BY WT.
1710731	% Solids	1710731-34	MM-T4-C5-17_SED_055-060CM	Percent Solids	53.7	[34]	53.7	J	HT	% BY WT.
1710731	% Solids	1710731-35	MM-T4-C5-17_SED_060-065CM	Percent Solids	51.7	[35]	51.7	J	HT	% BY WT.
1710731	% Solids	1710731-36	MM-T4-C5-17_SED_065-070CM	Percent Solids	51.1	[36]	51.1	J	HT	% BY WT.
1710731	% Solids	1710731-37	MM-T4-C5-17_SED_070-075CM	Percent Solids	65	[37]	65	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710731	% Solids	1710731-38	MM-T4-C5-17_SED_075-080CM	Percent Solids	57.1	[38]	57.1	J	HT	% BY WT.
1710731	% Solids	1710731-39	MM-T4-C5-17_SED_080-085CM	Percent Solids	52	[39]	52	J	HT	% BY WT.
1710732	% Solids	1710732-01	MM-T4-C1-17_SED_000-001CM	Percent Solids	34.4	[1]	34.4	J	HT	% BY WT.
1710732	% Solids	1710732-02	MM-T4-C1-17_SED_001-002CM	Percent Solids	31.1	[2]	31.1	J	HT	% BY WT.
1710732	% Solids	1710732-03	MM-T4-C1-17_SED_002-003CM	Percent Solids	33.8	[3]	33.8	J	HT	% BY WT.
1710732	% Solids	1710732-04	MM-T4-C1-17_SED_003-004CM	Percent Solids	35.7	[4]	35.7	J	HT	% BY WT.
1710732	% Solids	1710732-05	MM-T4-C1-17_SED_004-005CM	Percent Solids	34.1	[5]	34.1	J	HT	% BY WT.
1710732	% Solids	1710732-06	MM-T4-C1-17_SED_005-006CM	Percent Solids	31.8	[6]	31.8	J	HT	% BY WT.
1710732	% Solids	1710732-07	MM-T4-C1-17_SED_006-007CM	Percent Solids	29.3	[7]	29.3	J	HT	% BY WT.
1710732	% Solids	1710732-08	MM-T4-C1-17_SED_007-008CM	Percent Solids	29.5	[8]	29.5	J	HT	% BY WT.
1710732	% Solids	1710732-09	MM-T4-C1-17_SED_008-009CM	Percent Solids	32.8	[9]	32.8	J	HT	% BY WT.
1710732	% Solids	1710732-10	MM-T4-C1-17_SED_009-010CM	Percent Solids	33.5	[10]	33.5	J	HT	% BY WT.
1710732	% Solids	1710732-11	MM-T4-C1-17_SED_010-011CM	Percent Solids	29.5	[11]	29.5	J	HT	% BY WT.
1710732	% Solids	1710732-12	MM-T4-C1-17_SED_011-012CM	Percent Solids	31.4	[12]	31.4	J	HT	% BY WT.
1710732	% Solids	1710732-13	MM-T4-C1-17_SED_012-013CM	Percent Solids	32	[13]	32	J	HT	% BY WT.
1710732	% Solids	1710732-14	MM-T4-C1-17_SED_013-014CM	Percent Solids	34.4	[14]	34.4	J	HT	% BY WT.
1710732	% Solids	1710732-15	MM-T4-C1-17_SED_014-015CM	Percent Solids	37.9	[15]	37.9	J	HT	% BY WT.
1710732	% Solids	1710732-16	MM-T4-C1-17_SED_015-016CM	Percent Solids	35.9	[16]	35.9	J	HT	% BY WT.
1710732	% Solids	1710732-17	MM-T4-C1-17_SED_016-017CM	Percent Solids	35.4	[17]	35.4	J	HT	% BY WT.
1710732	% Solids	1710732-18	MM-T4-C1-17_SED_017-018CM	Percent Solids	34.7	[18]	34.7	J	HT	% BY WT.
1710732	% Solids	1710732-19	MM-T4-C1-17_SED_018-019CM	Percent Solids	33.9	[19]	33.9	J	HT	% BY WT.
1710732	% Solids	1710732-20	MM-T4-C1-17_SED_019-020CM	Percent Solids	35.7	[20]	35.7	J	HT	% BY WT.
1710732	% Solids	1710732-21	MM-T4-C1-17_SED_020-022CM	Percent Solids	34.7	[21]	34.7	J	HT	% BY WT.
1710732	% Solids	1710732-22	MM-T4-C1-17_SED_022-024CM	Percent Solids	27.9	[22]	27.9	J	HT	% BY WT.
1710732	% Solids	1710732-23	MM-T4-C1-17_SED_024-026CM	Percent Solids	33	[23]	33	J	HT	% BY WT.
1710732	% Solids	1710732-24	MM-T4-C1-17_SED_026-028CM	Percent Solids	37.3	[24]	37.3	J	HT	% BY WT.
1710732	% Solids	1710732-25	MM-T4-C1-17_SED_028-030CM	Percent Solids	36.4	[25]	36.4	J	HT	% BY WT.
1710732	% Solids	1710732-26	MM-T4-C1-17_SED_030-032CM	Percent Solids	43.7	[26]	43.7	J	HT	% BY WT.
1710732	% Solids	1710732-27	MM-T4-C1-17_SED_032-034CM	Percent Solids	38.7	[27]	38.7	J	HT	% BY WT.
1710732	% Solids	1710732-28	MM-T4-C1-17_SED_034-036CM	Percent Solids	45.1	[28]	45.1	J	HT	% BY WT.
1710732	% Solids	1710732-29	MM-T4-C1-17_SED_036-038CM	Percent Solids	44.3	[29]	44.3	J	HT	% BY WT.
1710732	% Solids	1710732-30	MM-T4-C1-17_SED_038-040CM	Percent Solids	41.1	[30]	41.1	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710732	% Solids	1710732-31	MM-T4-C1-17_SED_040-045CM	Percent Solids	31.1	[31]	31.1	J	HT	% BY WT.
1710732	% Solids	1710732-32	MM-T4-C1-17_SED_045-050CM	Percent Solids	31.5	[32]	31.5	J	HT	% BY WT.
1710732	% Solids	1710732-33	MM-T4-C1-17_SED_050-055CM	Percent Solids	35.4	[33]	35.4	J	HT	% BY WT.
1710732	% Solids	1710732-34	MM-T4-C1-17_SED_055-060CM	Percent Solids	30.9	[34]	30.9	J	HT	% BY WT.
1710732	% Solids	1710732-35	MM-T4-C1-17_SED_060-065CM	Percent Solids	24.4	[35]	24.4	J	HT	% BY WT.
1710732	% Solids	1710732-36	MM-T4-C1-17_SED_065-070CM	Percent Solids	25.3	[36]	25.3	J	HT	% BY WT.
1710732	% Solids	1710732-37	MM-T4-C1-17_SED_070-075CM	Percent Solids	20.8	[37]	20.8	J	HT	% BY WT.
1710732	% Solids	1710732-38	MM-T4-C1-17_SED_075-080CM	Percent Solids	18.5	[38]	18.5	J	HT	% BY WT.
1710732	% Solids	1710732-39	MM-T4-C1-17_SED_080-085CM	Percent Solids	19.3	[39]	19.3	J	HT	% BY WT.
1710733	% Solids	1710733-01	MM-T5-C1-17_SED_000-001CM	Percent Solids	26.7	[1]	26.7	J	HT	% BY WT.
1710733	% Solids	1710733-02	MM-T5-C1-17_SED_001-002CM	Percent Solids	27.2	[2]	27.2	J	HT	% BY WT.
1710733	% Solids	1710733-03	MM-T5-C1-17_SED_002-003CM	Percent Solids	27.5	[3]	27.5	J	HT	% BY WT.
1710733	% Solids	1710733-04	MM-T5-C1-17_SED_003-004CM	Percent Solids	27.5	[4]	27.5	J	HT	% BY WT.
1710733	% Solids	1710733-05	MM-T5-C1-17_SED_004-005CM	Percent Solids	28.5	[5]	28.5	J	HT	% BY WT.
1710733	% Solids	1710733-06	MM-T5-C1-17_SED_005-006CM	Percent Solids	25.9	[6]	25.9	J	HT	% BY WT.
1710733	% Solids	1710733-07	MM-T5-C1-17_SED_006-007CM	Percent Solids	26.5	[7]	26.5	J	HT	% BY WT.
1710733	% Solids	1710733-08	MM-T5-C1-17_SED_007-008CM	Percent Solids	23.7	[8]	23.7	J	HT	% BY WT.
1710733	% Solids	1710733-09	MM-T5-C1-17_SED_008-009CM	Percent Solids	26	[9]	26	J	HT	% BY WT.
1710733	% Solids	1710733-10	MM-T5-C1-17_SED_009-010CM	Percent Solids	26.7	[10]	26.7	J	HT	% BY WT.
1710733	% Solids	1710733-11	MM-T5-C1-17_SED_010-011CM	Percent Solids	27.8	[11]	27.8	J	HT	% BY WT.
1710733	% Solids	1710733-12	MM-T5-C1-17_SED_011-012CM	Percent Solids	26.5	[12]	26.5	J	HT	% BY WT.
1710733	% Solids	1710733-13	MM-T5-C1-17_SED_012-013CM	Percent Solids	22	[13]	22	J	HT	% BY WT.
1710733	% Solids	1710733-14	MM-T5-C1-17_SED_013-014CM	Percent Solids	21.3	[14]	21.3	J	HT	% BY WT.
1710733	% Solids	1710733-15	MM-T5-C1-17_SED_014-015CM	Percent Solids	18.2	[15]	18.2	J	HT	% BY WT.
1710733	% Solids	1710733-16	MM-T5-C1-17_SED_015-016CM	Percent Solids	18.9	[16]	18.9	J	HT	% BY WT.
1710733	% Solids	1710733-17	MM-T5-C1-17_SED_016-017CM	Percent Solids	18.6	[17]	18.6	J	HT	% BY WT.
1710733	% Solids	1710733-18	MM-T5-C1-17_SED_017-018CM	Percent Solids	18.4	[18]	18.4	J	HT	% BY WT.
1710733	% Solids	1710733-19	MM-T5-C1-17_SED_018-019CM	Percent Solids	21	[19]	21	J	HT	% BY WT.
1710733	% Solids	1710733-20	MM-T5-C1-17_SED_019-020CM	Percent Solids	22.4	[20]	22.4	J	HT	% BY WT.
1710733	% Solids	1710733-21	MM-T5-C1-17_SED_020-022CM	Percent Solids	20.6	[21]	20.6	J	HT	% BY WT.
1710733	% Solids	1710733-22	MM-T5-C1-17_SED_022-024CM	Percent Solids	24.6	[22]	24.6	J	HT	% BY WT.
1710733	% Solids	1710733-23	MM-T5-C1-17_SED_024-026CM	Percent Solids	25.6	[23]	25.6	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710733	% Solids	1710733-24	MM-T5-C1-17_SED_026-028CM	Percent Solids	23.7	[24]	23.7	J	HT	% BY WT.
1710733	% Solids	1710733-25	MM-T5-C1-17_SED_028-030CM	Percent Solids	23.8	[25]	23.8	J	HT	% BY WT.
1710733	% Solids	1710733-26	MM-T5-C1-17_SED_030-032CM	Percent Solids	26.6	[26]	26.6	J	HT	% BY WT.
1710733	% Solids	1710733-27	MM-T5-C1-17_SED_032-034CM	Percent Solids	34.6	[27]	34.6	J	HT	% BY WT.
1710733	% Solids	1710733-28	MM-T5-C1-17_SED_034-036CM	Percent Solids	33.6	[28]	33.6	J	HT	% BY WT.
1710733	% Solids	1710733-29	MM-T5-C1-17_SED_036-038CM	Percent Solids	28.4	[29]	28.4	J	HT	% BY WT.
1710733	% Solids	1710733-30	MM-T5-C1-17_SED_038-040CM	Percent Solids	31.8	[30]	31.8	J	HT	% BY WT.
1710733	% Solids	1710733-31	MM-T5-C1-17_SED_040-045CM	Percent Solids	31.7	[31]	31.7	J	HT	% BY WT.
1710733	% Solids	1710733-32	MM-T5-C1-17_SED_045-050CM	Percent Solids	46	[32]	46	J	HT	% BY WT.
1710733	% Solids	1710733-33	MM-T5-C1-17_SED_050-055CM	Percent Solids	51.4	[33]	51.4	J	HT	% BY WT.
1710733	% Solids	1710733-34	MM-T5-C1-17_SED_055-060CM	Percent Solids	36.2	[34]	36.2	J	HT	% BY WT.
1710733	% Solids	1710733-35	MM-T5-C1-17_SED_060-065CM	Percent Solids	35.8	[35]	35.8	J	HT	% BY WT.
1710733	% Solids	1710733-36	MM-T5-C1-17_SED_065-070CM	Percent Solids	39.6	[36]	39.6	J	HT	% BY WT.
1710733	% Solids	1710733-37	MM-T5-C1-17_SED_070-075CM	Percent Solids	35.5	[37]	35.5	J	HT	% BY WT.
1710733	% Solids	1710733-38	MM-T5-C1-17_SED_075-080CM	Percent Solids	34.2	[38]	34.2	J	HT	% BY WT.
1710733	% Solids	1710733-39	MM-T5-C1-17_SED_080-085CM	Percent Solids	29.1	[39]	29.1	J	HT	% BY WT.
1710733	% Solids	1710733-40	MM-T5-C1-17_SED_085-090CM	Percent Solids	34.3	[40]	34.3	J	HT	% BY WT.
1710907	% Solids	1710907-01	MM-T3-C4-D-17_SED_000-001CM	Percent Solids	46.8	[1]	46.8	J	HT	% BY WT.
1710907	% Solids	1710907-02	MM-T3-C4-D-17_SED_000-001CM_DUP	Percent Solids	46	[2]	46	J	HT	% BY WT.
1710907	% Solids	1710907-03	MM-T3-C4-D-17_SED_001-002CM	Percent Solids	45.7	[3]	45.7	J	HT	% BY WT.
1710907	% Solids	1710907-04	MM-T3-C4-D-17_SED_001-002CM_DUP	Percent Solids	46.1	[4]	46.1	J	HT	% BY WT.
1710907	% Solids	1710907-05	MM-T3-C4-D-17_SED_002-003CM	Percent Solids	42.1	[5]	42.1	J	HT	% BY WT.
1710907	% Solids	1710907-06	MM-T3-C4-D-17_SED_002-003CM_DUP	Percent Solids	44.1	[6]	44.1	J	HT	% BY WT.
1710907	% Solids	1710907-07	MM-T3-C4-D-17_SED_003-004CM	Percent Solids	44	[7]	44	J	HT	% BY WT.
1710907	% Solids	1710907-08	MM-T3-C4-D-17_SED_003-004CM_DUP	Percent Solids	44.1	[8]	44.1	J	HT	% BY WT.
1710907	% Solids	1710907-09	MM-T3-C4-D-17_SED_004-005CM	Percent Solids	45.6	[9]	45.6	J	HT	% BY WT.
1710907	% Solids	1710907-10	MM-T3-C4-D-17_SED_004-005CM_DUP	Percent Solids	45.8	[10]	45.8	J	HT	% BY WT.
1710907	% Solids	1710907-11	MM-T3-C4-D-17_SED_005-006CM	Percent Solids	47.2	[11]	47.2	J	HT	% BY WT.
1710907	% Solids	1710907-12	MM-T3-C4-D-17_SED_005-006CM_DUP	Percent Solids	47.2	[12]	47.2	J	HT	% BY WT.
1710907	% Solids	1710907-13	MM-T3-C4-D-17_SED_006-007CM	Percent Solids	46.5	[13]	46.5	J	HT	% BY WT.
1710907	% Solids	1710907-14	MM-T3-C4-D-17_SED_006-007CM_DUP	Percent Solids	46.4	[14]	46.4	J	HT	% BY WT.
1710907	% Solids	1710907-15	MM-T3-C4-D-17_SED_007-008CM	Percent Solids	44	[15]	44	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710907	% Solids	1710907-16	MM-T3-C4-D-17_SED_007-008CM_DUP	Percent Solids	44.6	[16]	44.6	J	HT	% BY WT.
1710907	% Solids	1710907-17	MM-T3-C4-D-17_SED_008-009CM	Percent Solids	44.1	[17]	44.1	J	HT	% BY WT.
1710907	% Solids	1710907-18	MM-T3-C4-D-17_SED_008-009CM_DUP	Percent Solids	44	[18]	44	J	HT	% BY WT.
1710907	% Solids	1710907-19	MM-T3-C4-D-17_SED_009-010CM	Percent Solids	46.1	[19]	46.1	J	HT	% BY WT.
1710907	% Solids	1710907-20	MM-T3-C4-D-17_SED_009-010CM_DUP	Percent Solids	46.9	[20]	46.9	J	HT	% BY WT.
1710907	% Solids	1710907-21	MM-T3-C4-D-17_SED_010-011CM	Percent Solids	45.8	[21]	45.8	J	HT	% BY WT.
1710907	% Solids	1710907-22	MM-T3-C4-D-17_SED_010-011CM_DUP	Percent Solids	45.5	[22]	45.5	J	HT	% BY WT.
1710907	% Solids	1710907-23	MM-T3-C4-D-17_SED_011-012CM	Percent Solids	44	[23]	44	J	HT	% BY WT.
1710907	% Solids	1710907-24	MM-T3-C4-D-17_SED_011-012CM_DUP	Percent Solids	43	[24]	43	J	HT	% BY WT.
1710907	% Solids	1710907-25	MM-T3-C4-D-17_SED_012-013CM	Percent Solids	41.3	[25]	41.3	J	HT	% BY WT.
1710907	% Solids	1710907-26	MM-T3-C4-D-17_SED_012-013CM_DUP	Percent Solids	40.8	[26]	40.8	J	HT	% BY WT.
1710907	% Solids	1710907-27	MM-T3-C4-D-17_SED_013-014CM	Percent Solids	44.7	[27]	44.7	J	HT	% BY WT.
1710907	% Solids	1710907-28	MM-T3-C4-D-17_SED_013-014CM_DUP	Percent Solids	44.9	[28]	44.9	J	HT	% BY WT.
1710907	% Solids	1710907-29	MM-T3-C4-D-17_SED_014-015CM	Percent Solids	42.4	[29]	42.4	J	HT	% BY WT.
1710907	% Solids	1710907-30	MM-T3-C4-D-17_SED_014-015CM_DUP	Percent Solids	43.3	[30]	43.3	J	HT	% BY WT.
1710907	% Solids	1710907-31	MM-T3-C4-D-17_SED_015-016CM	Percent Solids	43	[31]	43	J	HT	% BY WT.
1710907	% Solids	1710907-32	MM-T3-C4-D-17_SED_015-016CM_DUP	Percent Solids	42.8	[32]	42.8	J	HT	% BY WT.
1710907	% Solids	1710907-33	MM-T3-C4-D-17_SED_016-017CM	Percent Solids	47.5	[33]	47.5	J	HT	% BY WT.
1710907	% Solids	1710907-34	MM-T3-C4-D-17_SED_016-017CM_DUP	Percent Solids	44.7	[34]	44.7	J	HT	% BY WT.
1710907	% Solids	1710907-35	MM-T3-C4-D-17_SED_017-018CM	Percent Solids	47.5	[35]	47.5	J	HT	% BY WT.
1710907	% Solids	1710907-36	MM-T3-C4-D-17_SED_017-018CM_DUP	Percent Solids	46.1	[36]	46.1	J	HT	% BY WT.
1710907	% Solids	1710907-37	MM-T3-C4-D-17_SED_018-019CM	Percent Solids	44.8	[37]	44.8	J	HT	% BY WT.
1710907	% Solids	1710907-38	MM-T3-C4-D-17_SED_018-019CM_DUP	Percent Solids	44.2	[38]	44.2	J	HT	% BY WT.
1710907	% Solids	1710907-39	MM-T3-C4-D-17_SED_019-020CM	Percent Solids	46	[39]	46	J	HT	% BY WT.
1710907	% Solids	1710907-40	MM-T3-C4-D-17_SED_019-020CM_DUP	Percent Solids	45.7	[40]	45.7	J	HT	% BY WT.
1710907	% Solids	1710907-41	MM-T3-C4-D-17_SED_020-022CM	Percent Solids	45.3	[41]	45.3	J	HT	% BY WT.
1710907	% Solids	1710907-42	MM-T3-C4-D-17_SED_020-022CM_DUP	Percent Solids	46.3	[42]	46.3	J	HT	% BY WT.
1710907	% Solids	1710907-45	MM-T3-C4-D-17_SED_024-026CM	Percent Solids	44.8	[43]	44.8	J	HT	% BY WT.
1710907	% Solids	1710907-46	MM-T3-C4-D-17_SED_024-026CM_DUP	Percent Solids	46.1	[44]	46.1	J	HT	% BY WT.
1710907	% Solids	1710907-47	MM-T3-C4-D-17_SED_026-028CM	Percent Solids	47.7	[45]	47.7	J	HT	% BY WT.
1710907	% Solids	1710907-48	MM-T3-C4-D-17_SED_026-028CM_DUP	Percent Solids	47.4	[46]	47.4	J	HT	% BY WT.
1710907	% Solids	1710907-49	MM-T3-C4-D-17_SED_028-030CM	Percent Solids	45.7	[47]	45.7	J	HT	% BY WT.

TABLE 2
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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710907	% Solids	1710907-50	MM-T3-C4-D-17_SED_028-030CM_DUP	Percent Solids	45.4	[48]	45.4	J	HT	% BY WT.
1710907	% Solids	1710907-51	MM-T3-C4-D-17_SED_030-032CM	Percent Solids	44.3	[49]	44.3	J	HT	% BY WT.
1710907	% Solids	1710907-52	MM-T3-C4-D-17_SED_030-032CM_DUP	Percent Solids	42.8	[50]	42.8	J	HT	% BY WT.
1710907	% Solids	1710907-53	MM-T3-C4-D-17_SED_032-034CM	Percent Solids	45.6	[51]	45.6	J	HT	% BY WT.
1710907	% Solids	1710907-54	MM-T3-C4-D-17_SED_032-034CM_DUP	Percent Solids	46.5	[52]	46.5	J	HT	% BY WT.
1710907	% Solids	1710907-55	MM-T3-C4-D-17_SED_034-036CM	Percent Solids	44.9	[53]	44.9	J	HT	% BY WT.
1710907	% Solids	1710907-56	MM-T3-C4-D-17_SED_034-036CM_DUP	Percent Solids	44.9	[54]	44.9	J	HT	% BY WT.
1710907	% Solids	1710907-57	MM-T3-C4-D-17_SED_036-038CM	Percent Solids	42.9	[55]	42.9	J	HT	% BY WT.
1710907	% Solids	1710907-58	MM-T3-C4-D-17_SED_036-038CM_DUP	Percent Solids	43.7	[56]	43.7	J	HT	% BY WT.
1710907	% Solids	1710907-59	MM-T3-C4-D-17_SED_038-040CM	Percent Solids	42.6	[57]	42.6	J	HT	% BY WT.
1710907	% Solids	1710907-60	MM-T3-C4-D-17_SED_038-040CM_DUP	Percent Solids	42.7	[58]	42.7	J	HT	% BY WT.
1710907	% Solids	1710907-61	MM-T3-C4-D-17_SED_040-045CM	Percent Solids	41.5	[59]	41.5	J	HT	% BY WT.
1710907	% Solids	1710907-62	MM-T3-C4-D-17_SED_040-045CM_DUP	Percent Solids	42.1	[60]	42.1	J	HT	% BY WT.
1710907	% Solids	1710907-63	MM-T3-C4-D-17_SED_045-050CM	Percent Solids	39.6	[61]	39.6	J	HT	% BY WT.
1710907	% Solids	1710907-64	MM-T3-C4-D-17_SED_045-050CM_DUP	Percent Solids	40.5	[62]	40.5	J	HT	% BY WT.
1710907	% Solids	1710907-65	MM-T3-C4-D-17_SED_050-055CM	Percent Solids	43.4	[63]	43.4	J	HT	% BY WT.
1710907	% Solids	1710907-66	MM-T3-C4-D-17_SED_050-055CM_DUP	Percent Solids	44	[64]	44	J	HT	% BY WT.
1710907	% Solids	1710907-67	MM-T3-C4-D-17_SED_055-060CM	Percent Solids	46.7	[65]	46.7	J	HT	% BY WT.
1710907	% Solids	1710907-68	MM-T3-C4-D-17_SED_055-060CM_DUP	Percent Solids	46.6	[66]	46.6	J	HT	% BY WT.
1710907	% Solids	1710907-69	MM-T3-C4-D-17_SED_060-065CM	Percent Solids	48.9	[67]	48.9	J	HT	% BY WT.
1710907	% Solids	1710907-70	MM-T3-C4-D-17_SED_060-065CM_DUP	Percent Solids	47.9	[68]	47.9	J	HT	% BY WT.
1710907	% Solids	1710907-71	MM-T3-C4-D-17_SED_065-070CM	Percent Solids	43.7	[69]	43.7	J	HT	% BY WT.
1710907	% Solids	1710907-72	MM-T3-C4-D-17_SED_065-070CM_DUP	Percent Solids	43.6	[70]	43.6	J	HT	% BY WT.
1710907	% Solids	1710907-73	MM-T3-C4-D-17_SED_070-075CM	Percent Solids	39.4	[71]	39.4	J	HT	% BY WT.
1710907	% Solids	1710907-74	MM-T3-C4-D-17_SED_070-075CM_DUP	Percent Solids	39.5	[72]	39.5	J	HT	% BY WT.
1710907	% Solids	1710907-75	MM-T3-C4-D-17_SED_075-080CM	Percent Solids	21.6	[73]	21.6	J	HT	% BY WT.
1710907	% Solids	1710907-76	MM-T3-C4-D-17_SED_075-080CM_DUP	Percent Solids	22	[74]	22	J	HT	% BY WT.
1710910	% Solids	1710910-01	MM-T3-C7-17_SED_000-001CM	Percent Solids	20.6	[1]	20.6	J	HT	% BY WT.
1710910	% Solids	1710910-02	MM-T3-C7-17_SED_001-002CM	Percent Solids	20.2	[2]	20.2	J	HT	% BY WT.
1710910	% Solids	1710910-03	MM-T3-C7-17_SED_002-003CM	Percent Solids	18.9	[3]	18.9	J	HT	% BY WT.
1710910	% Solids	1710910-04	MM-T3-C7-17_SED_003-004CM	Percent Solids	19.9	[4]	19.9	J	HT	% BY WT.
1710910	% Solids	1710910-05	MM-T3-C7-17_SED_004-005CM	Percent Solids	22.1	[5]	22.1	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710910	% Solids	1710910-06	MM-T3-C7-17_SED_005-006CM	Percent Solids	21.9	[6]	21.9	J	HT	% BY WT.
1710910	% Solids	1710910-07	MM-T3-C7-17_SED_006-007CM	Percent Solids	19.4	[7]	19.4	J	HT	% BY WT.
1710910	% Solids	1710910-08	MM-T3-C7-17_SED_007-008CM	Percent Solids	19.8	[8]	19.8	J	HT	% BY WT.
1710910	% Solids	1710910-09	MM-T3-C7-17_SED_008-009CM	Percent Solids	20.5	[9]	20.5	J	HT	% BY WT.
1710910	% Solids	1710910-10	MM-T3-C7-17_SED_009-010CM	Percent Solids	20.6	[10]	20.6	J	HT	% BY WT.
1710910	% Solids	1710910-11	MM-T3-C7-17_SED_010-011CM	Percent Solids	21.3	[11]	21.3	J	HT	% BY WT.
1710910	% Solids	1710910-12	MM-T3-C7-17_SED_011-012CM	Percent Solids	23.8	[12]	23.8	J	HT	% BY WT.
1710910	% Solids	1710910-13	MM-T3-C7-17_SED_012-013CM	Percent Solids	23.5	[13]	23.5	J	HT	% BY WT.
1710910	% Solids	1710910-14	MM-T3-C7-17_SED_013-014CM	Percent Solids	24	[14]	24	J	HT	% BY WT.
1710910	% Solids	1710910-15	MM-T3-C7-17_SED_014-015CM	Percent Solids	22.7	[15]	22.7	J	HT	% BY WT.
1710910	% Solids	1710910-16	MM-T3-C7-17_SED_015-016CM	Percent Solids	22.4	[16]	22.4	J	HT	% BY WT.
1710910	% Solids	1710910-17	MM-T3-C7-17_SED_016-017CM	Percent Solids	24.2	[17]	24.2	J	HT	% BY WT.
1710910	% Solids	1710910-18	MM-T3-C7-17_SED_017-018CM	Percent Solids	27.7	O-04	27.7	J	HT	% BY WT.
1710910	% Solids	1710910-19	MM-T3-C7-17_SED_018-019CM	Percent Solids	27.6	O-04	27.6	J	HT	% BY WT.
1710910	% Solids	1710910-20	MM-T3-C7-17_SED_019-020CM	Percent Solids	27.9	O-04	27.9	J	HT	% BY WT.
1710910	% Solids	1710910-21	MM-T3-C7-17_SED_020-022CM	Percent Solids	29.6	O-04	29.6	J	HT	% BY WT.
1710910	% Solids	1710910-22	MM-T3-C7-17_SED_022-024CM	Percent Solids	30.7	O-04	30.7	J	HT	% BY WT.
1710910	% Solids	1710910-23	MM-T3-C7-17_SED_024-026CM	Percent Solids	26.8	O-04	26.8	J	HT	% BY WT.
1710910	% Solids	1710910-24	MM-T3-C7-17_SED_026-028CM	Percent Solids	22.1	O-04	22.1	J	HT	% BY WT.
1710910	% Solids	1710910-25	MM-T3-C7-17_SED_028-030CM	Percent Solids	21.5	O-04	21.5	J	HT	% BY WT.
1710910	% Solids	1710910-26	MM-T3-C7-17_SED_030-032CM	Percent Solids	23.4	O-04	23.4	J	HT	% BY WT.
1710910	% Solids	1710910-27	MM-T3-C7-17_SED_032-034CM	Percent Solids	25.1	O-04	25.1	J	HT	% BY WT.
1710910	% Solids	1710910-28	MM-T3-C7-17_SED_034-036CM	Percent Solids	25	O-04	25	J	HT	% BY WT.
1710910	% Solids	1710910-29	MM-T3-C7-17_SED_036-038CM	Percent Solids	21.4	O-04	21.4	J	HT	% BY WT.
1710910	% Solids	1710910-30	MM-T3-C7-17_SED_038-040CM	Percent Solids	23.2	O-04	23.2	J	HT	% BY WT.
1710910	% Solids	1710910-31	MM-T3-C7-17_SED_040-045CM	Percent Solids	26.5	O-04	26.5	J	HT	% BY WT.
1710910	% Solids	1710910-32	MM-T3-C7-17_SED_045-050CM	Percent Solids	26.6	O-04	26.6	J	HT	% BY WT.
1710910	% Solids	1710910-33	MM-T3-C7-17_SED_050-055CM	Percent Solids	27.6	O-04	27.6	J	HT	% BY WT.
1710910	% Solids	1710910-34	MM-T3-C7-17_SED_055-060CM	Percent Solids	30.7	O-04	30.7	J	HT	% BY WT.
1710910	% Solids	1710910-35	MM-T3-C7-17_SED_060-065CM	Percent Solids	32.8	O-04	32.8	J	HT	% BY WT.
1710910	% Solids	1710910-36	MM-T3-C7-17_SED_065-070CM	Percent Solids	35	O-04	35	J	HT	% BY WT.
1710913	% Solids	1710913-01	MM-T4-C7-17_SED_000-001CM	Percent Solids	35.2	O-04	35.2	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710913	% Solids	1710913-02	MM-T4-C7-17_SED_000-001CM_DUP	Percent Solids	36.5	O-04	36.5	J	HT	% BY WT.
1710913	% Solids	1710913-03	MM-T4-C7-17_SED_001-002CM	Percent Solids	37.5	O-04	37.5	J	HT	% BY WT.
1710913	% Solids	1710913-04	MM-T4-C7-17_SED_001-002CM_DUP	Percent Solids	37.7	O-04	37.7	J	HT	% BY WT.
1710913	% Solids	1710913-05	MM-T4-C7-17_SED_002-003CM	Percent Solids	40	O-04	40	J	HT	% BY WT.
1710913	% Solids	1710913-06	MM-T4-C7-17_SED_002-003CM_DUP	Percent Solids	40	O-04	40	J	HT	% BY WT.
1710913	% Solids	1710913-07	MM-T4-C7-17_SED_003-004CM	Percent Solids	43.7	O-04	43.7	J	HT	% BY WT.
1710913	% Solids	1710913-08	MM-T4-C7-17_SED_003-004CM_DUP	Percent Solids	41.5	O-04	41.5	J	HT	% BY WT.
1710913	% Solids	1710913-09	MM-T4-C7-17_SED_004-005CM	Percent Solids	44.6	O-04	44.6	J	HT	% BY WT.
1710913	% Solids	1710913-10	MM-T4-C7-17_SED_004-005CM_DUP	Percent Solids	45.1	O-04	45.1	J	HT	% BY WT.
1710913	% Solids	1710913-11	MM-T4-C7-17_SED_005-006CM	Percent Solids	46.8	O-04	46.8	J	HT	% BY WT.
1710913	% Solids	1710913-12	MM-T4-C7-17_SED_005-006CM_DUP	Percent Solids	46.8	O-04	46.8	J	HT	% BY WT.
1710913	% Solids	1710913-13	MM-T4-C7-17_SED_006-007CM	Percent Solids	48.7	O-04	48.7	J	HT	% BY WT.
1710913	% Solids	1710913-14	MM-T4-C7-17_SED_006-007CM_DUP	Percent Solids	49	O-04	49	J	HT	% BY WT.
1710913	% Solids	1710913-15	MM-T4-C7-17_SED_007-008CM	Percent Solids	48	O-04	48	J	HT	% BY WT.
1710913	% Solids	1710913-16	MM-T4-C7-17_SED_007-008CM_DUP	Percent Solids	48.4	O-04	48.4	J	HT	% BY WT.
1710913	% Solids	1710913-17	MM-T4-C7-17_SED_008-009CM	Percent Solids	41.9	O-04	41.9	J	HT	% BY WT.
1710913	% Solids	1710913-18	MM-T4-C7-17_SED_008-009CM_DUP	Percent Solids	33	O-04	33	J	HT	% BY WT.
1710913	% Solids	1710913-19	MM-T4-C7-17_SED_009-010CM	Percent Solids	42.5	O-04	42.5	J	HT	% BY WT.
1710913	% Solids	1710913-20	MM-T4-C7-17_SED_009-010CM_DUP	Percent Solids	39	O-04	39	J	HT	% BY WT.
1710913	% Solids	1710913-21	MM-T4-C7-17_SED_010-011CM	Percent Solids	40.8	O-04	40.8	J	HT	% BY WT.
1710913	% Solids	1710913-22	MM-T4-C7-17_SED_010-011CM_DUP	Percent Solids	37.1	O-04	37.1	J	HT	% BY WT.
1710913	% Solids	1710913-23	MM-T4-C7-17_SED_011-012CM	Percent Solids	37.6	O-04	37.6	J	HT	% BY WT.
1710913	% Solids	1710913-24	MM-T4-C7-17_SED_011-012CM_DUP	Percent Solids	38.4	O-04	38.4	J	HT	% BY WT.
1710913	% Solids	1710913-25	MM-T4-C7-17_SED_012-013CM	Percent Solids	39.1	O-04	39.1	J	HT	% BY WT.
1710913	% Solids	1710913-26	MM-T4-C7-17_SED_012-013CM_DUP	Percent Solids	39.1	O-04	39.1	J	HT	% BY WT.
1710913	% Solids	1710913-27	MM-T4-C7-17_SED_013-014CM	Percent Solids	37.7	O-04	37.7	J	HT	% BY WT.
1710913	% Solids	1710913-28	MM-T4-C7-17_SED_013-014CM_DUP	Percent Solids	37.4	O-04	37.4	J	HT	% BY WT.
1710913	% Solids	1710913-29	MM-T4-C7-17_SED_014-015CM	Percent Solids	33.9	O-04	33.9	J	HT	% BY WT.
1710913	% Solids	1710913-30	MM-T4-C7-17_SED_014-015CM_DUP	Percent Solids	36.7	O-04	36.7	J	HT	% BY WT.
1710913	% Solids	1710913-31	MM-T4-C7-17_SED_015-016CM	Percent Solids	40.5	O-04	40.5	J	HT	% BY WT.
1710913	% Solids	1710913-32	MM-T4-C7-17_SED_015-016CM_DUP	Percent Solids	42.9	O-04	42.9	J	HT	% BY WT.
1710913	% Solids	1710913-33	MM-T4-C7-17_SED_016-017CM	Percent Solids	39.7	O-04	39.7	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710913	% Solids	1710913-34	MM-T4-C7-17_SED_016-017CM_DUP	Percent Solids	37.7	O-04	37.7	J	HT	% BY WT.
1710913	% Solids	1710913-35	MM-T4-C7-17_SED_017-018CM	Percent Solids	46.7	O-04	46.7	J	HT	% BY WT.
1710913	% Solids	1710913-36	MM-T4-C7-17_SED_017-018CM_DUP	Percent Solids	46.9	O-04	46.9	J	HT	% BY WT.
1710913	% Solids	1710913-37	MM-T4-C7-17_SED_018-019CM	Percent Solids	43.4	O-04	43.4	J	HT	% BY WT.
1710913	% Solids	1710913-38	MM-T4-C7-17_SED_018-019CM_DUP	Percent Solids	42.7	O-04	42.7	J	HT	% BY WT.
1710913	% Solids	1710913-39	MM-T4-C7-17_SED_019-020CM	Percent Solids	46.9	O-04	46.9	J	HT	% BY WT.
1710913	% Solids	1710913-40	MM-T4-C7-17_SED_019-020CM_DUP	Percent Solids	53.9	O-04	53.9	J	HT	% BY WT.
1710913	% Solids	1710913-41	MM-T4-C7-17_SED_020-022CM	Percent Solids	74.8	O-04	74.8	J	HT	% BY WT.
1710913	% Solids	1710913-42	MM-T4-C7-17_SED_020-022CM_DUP	Percent Solids	72.9	O-04	72.9	J	HT	% BY WT.
1710913	% Solids	1710913-43	MM-T4-C7-17_SED_022-024CM	Percent Solids	76.6	O-04	76.6	J	HT	% BY WT.
1710913	% Solids	1710913-44	MM-T4-C7-17_SED_022-024CM_DUP	Percent Solids	78.1	O-04	78.1	J	HT	% BY WT.
1710913	% Solids	1710913-45	MM-T4-C7-17_SED_024-026CM	Percent Solids	76	O-04	76	J	HT	% BY WT.
1710913	% Solids	1710913-46	MM-T4-C7-17_SED_024-026CM_DUP	Percent Solids	76.3	O-04	76.3	J	HT	% BY WT.
1710913	% Solids	1710913-47	MM-T4-C7-17_SED_026-028CM	Percent Solids	69.8	O-04	69.8	J	HT	% BY WT.
1710913	% Solids	1710913-48	MM-T4-C7-17_SED_026-028CM_DUP	Percent Solids	72	O-04	72	J	HT	% BY WT.
1710913	% Solids	1710913-49	MM-T4-C7-17_SED_028-030CM	Percent Solids	73.3	O-04	73.3	J	HT	% BY WT.
1710913	% Solids	1710913-50	MM-T4-C7-17_SED_028-030CM_DUP	Percent Solids	74	O-04	74	J	HT	% BY WT.
1710913	% Solids	1710913-51	MM-T4-C7-17_SED_030-032CM	Percent Solids	74.1	O-04	74.1	J	HT	% BY WT.
1710913	% Solids	1710913-52	MM-T4-C7-17_SED_030-032CM_DUP	Percent Solids	72.9	O-04	72.9	J	HT	% BY WT.
1710913	% Solids	1710913-53	MM-T4-C7-17_SED_032-034CM	Percent Solids	78.1	O-04	78.1	J	HT	% BY WT.
1710913	% Solids	1710913-54	MM-T4-C7-17_SED_032-034CM_DUP	Percent Solids	78.5	O-04	78.5	J	HT	% BY WT.
1710913	% Solids	1710913-55	MM-T4-C7-17_SED_034-036CM	Percent Solids	75.8	O-04	75.8	J	HT	% BY WT.
1710913	% Solids	1710913-56	MM-T4-C7-17_SED_034-036CM_DUP	Percent Solids	75.4	O-04	75.4	J	HT	% BY WT.
1710913	% Solids	1710913-57	MM-T4-C7-17_SED_036-038CM	Percent Solids	78.6	O-04	78.6	J	HT	% BY WT.
1710913	% Solids	1710913-58	MM-T4-C7-17_SED_036-038CM_DUP	Percent Solids	79.7	O-04	79.7	J	HT	% BY WT.
1710913	% Solids	1710913-59	MM-T4-C7-17_SED_038-040CM	Percent Solids	78.6	O-04	78.6	J	HT	% BY WT.
1710913	% Solids	1710913-60	MM-T4-C7-17_SED_038-040CM_DUP	Percent Solids	78.7	O-04	78.7	J	HT	% BY WT.
1710913	% Solids	1710913-61	MM-T4-C7-17_SED_040-045CM	Percent Solids	76.1	O-04	76.1	J	HT	% BY WT.
1710913	% Solids	1710913-62	MM-T4-C7-17_SED_040-045CM_DUP	Percent Solids	77.9	O-04	77.9	J	HT	% BY WT.
1710913	% Solids	1710913-65	MM-T4-C7-17_SED_050-055CM	Percent Solids	73.9	O-04	73.9	J	HT	% BY WT.
1710913	% Solids	1710913-66	MM-T4-C7-17_SED_050-055CM_DUP	Percent Solids	75	O-04	75	J	HT	% BY WT.
1710913	% Solids	1710913-69	MM-T4-C7-17_SED_060-065CM	Percent Solids	73.5	O-04	73.5	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1710913	% Solids	1710913-70	MM-T4-C7-17_SED_060-065CM_DUP	Percent Solids	73.5	O-04	73.5	J	HT	% BY WT.
1710913	% Solids	1710913-71	MM-T4-C7-17_SED_065-070CM	Percent Solids	70	O-04	70	J	HT	% BY WT.
1710913	% Solids	1710913-72	MM-T4-C7-17_SED_065-070CM_DUP	Percent Solids	72.3	O-04	72.3	J	HT	% BY WT.
1710913	% Solids	1710913-73	MM-T4-C7-17_SED_070-075CM	Percent Solids	74.8	O-04	74.8	J	HT	% BY WT.
1710913	% Solids	1710913-74	MM-T4-C7-17_SED_070-075CM_DUP	Percent Solids	76	O-04	76	J	HT	% BY WT.
1710913	% Solids	1710913-75	MM-T4-C7-17_SED_075-080CM	Percent Solids	74.6	O-04	74.6	J	HT	% BY WT.
1710913	% Solids	1710913-76	MM-T4-C7-17_SED_075-080CM_DUP	Percent Solids	73	O-04	73	J	HT	% BY WT.
1710913	% Solids	1710913-77	MM-T4-C7-17_SED_080-085CM	Percent Solids	74.9	O-04	74.9	J	HT	% BY WT.
1710913	% Solids	1710913-78	MM-T4-C7-17_SED_080-085CM_DUP	Percent Solids	75	O-04	75	J	HT	% BY WT.
1710913	% Solids	1710913-79	MM-T4-C7-17_SED_085-090CM	Percent Solids	76.1	O-04	76.1	J	HT	% BY WT.
1710913	% Solids	1710913-80	MM-T4-C7-17_SED_085-090CM_DUP	Percent Solids	76.9	O-04	76.9	J	HT	% BY WT.
1710916	% Solids	1710916-01	MM-T5-C3-17_SED_000-001CM	Percent Solids	29	O-04	29	J	HT	% BY WT.
1710916	% Solids	1710916-02	MM-T5-C3-17_SED_001-002CM	Percent Solids	26.7	O-04	26.7	J	HT	% BY WT.
1710916	% Solids	1710916-03	MM-T5-C3-17_SED_002-003CM	Percent Solids	31.1	O-04	31.1	J	HT	% BY WT.
1710916	% Solids	1710916-04	MM-T5-C3-17_SED_003-004CM	Percent Solids	29.9	O-04	29.9	J	HT	% BY WT.
1710916	% Solids	1710916-05	MM-T5-C3-17_SED_004-005CM	Percent Solids	28.3	O-04	28.3	J	HT	% BY WT.
1710916	% Solids	1710916-06	MM-T5-C3-17_SED_005-006CM	Percent Solids	27.9	O-04	27.9	J	HT	% BY WT.
1710916	7474_1631	1710916-07	MM-T5-C3-17_SED_006-007CM	Mercury	840		840	J	MS-L	NG/G
1710916	% Solids	1710916-07	MM-T5-C3-17_SED_006-007CM	Percent Solids	28.6	O-04	28.6	J	HT	% BY WT.
1710916	% Solids	1710916-08	MM-T5-C3-17_SED_007-008CM	Percent Solids	33.9	O-04	33.9	J	HT	% BY WT.
1710916	% Solids	1710916-09	MM-T5-C3-17_SED_008-009CM	Percent Solids	35.1	O-04	35.1	J	HT	% BY WT.
1710916	% Solids	1710916-10	MM-T5-C3-17_SED_009-010CM	Percent Solids	31.7	O-04	31.7	J	HT	% BY WT.
1710916	% Solids	1710916-11	MM-T5-C3-17_SED_010-011CM	Percent Solids	29.6	O-04	29.6	J	HT	% BY WT.
1710916	% Solids	1710916-12	MM-T5-C3-17_SED_011-012CM	Percent Solids	30.3	O-04	30.3	J	HT	% BY WT.
1710916	% Solids	1710916-13	MM-T5-C3-17_SED_012-013CM	Percent Solids	30.3	O-04	30.3	J	HT	% BY WT.
1710916	% Solids	1710916-14	MM-T5-C3-17_SED_013-014CM	Percent Solids	30.6	O-04	30.6	J	HT	% BY WT.
1710916	% Solids	1710916-15	MM-T5-C3-17_SED_014-015CM	Percent Solids	29.7	O-04	29.7	J	HT	% BY WT.
1710916	% Solids	1710916-16	MM-T5-C3-17_SED_015-016CM	Percent Solids	26.6	O-04	26.6	J	HT	% BY WT.
1710916	% Solids	1710916-17	MM-T5-C3-17_SED_016-017CM	Percent Solids	28.1	O-04	28.1	J	HT	% BY WT.
1710916	% Solids	1710916-18	MM-T5-C3-17_SED_017-018CM	Percent Solids	27.5	O-04	27.5	J	HT	% BY WT.
1710916	% Solids	1710916-19	MM-T5-C3-17_SED_018-019CM	Percent Solids	26.1	O-04	26.1	J	HT	% BY WT.
1710916	% Solids	1710916-20	MM-T5-C3-17_SED_019-020CM	Percent Solids	26	O-04	26	J	HT	% BY WT.

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1710916	% Solids	1710916-21	MM-T5-C3-17_SED_020-022CM	Percent Solids	29.3	O-04	29.3	J	HT	% BY WT.
1710916	% Solids	1710916-22	MM-T5-C3-17_SED_022-024CM	Percent Solids	29.1	O-04	29.1	J	HT	% BY WT.
1710916	% Solids	1710916-23	MM-T5-C3-17_SED_024-026CM	Percent Solids	27.7	O-04	27.7	J	HT	% BY WT.
1710916	% Solids	1710916-24	MM-T5-C3-17_SED_026-028CM	Percent Solids	29.3	O-04	29.3	J	HT	% BY WT.
1710916	% Solids	1710916-25	MM-T5-C3-17_SED_028-030CM	Percent Solids	28.9	O-04	28.9	J	HT	% BY WT.
1710916	% Solids	1710916-26	MM-T5-C3-17_SED_030-032CM	Percent Solids	26.2	O-04	26.2	J	HT	% BY WT.
1710916	% Solids	1710916-27	MM-T5-C3-17_SED_032-034CM	Percent Solids	25.2	O-04	25.2	J	HT	% BY WT.
1710916	% Solids	1710916-28	MM-T5-C3-17_SED_034-036CM	Percent Solids	27.5	O-04	27.5	J	HT	% BY WT.
1710916	% Solids	1710916-29	MM-T5-C3-17_SED_036-038CM	Percent Solids	28.3	O-04	28.3	J	HT	% BY WT.
1710916	% Solids	1710916-30	MM-T5-C3-17_SED_038-040CM	Percent Solids	32.4	O-04	32.4	J	HT	% BY WT.
1710916	% Solids	1710916-31	MM-T5-C3-17_SED_040-045CM	Percent Solids	34.9	O-04	34.9	J	HT	% BY WT.
1710916	% Solids	1710916-32	MM-T5-C3-17_SED_045-050CM	Percent Solids	39.8	O-04	39.8	J	HT	% BY WT.
1710916	% Solids	1710916-33	MM-T5-C3-17_SED_050-055CM	Percent Solids	44.1	O-04	44.1	J	HT	% BY WT.
1710916	% Solids	1710916-34	MM-T5-C3-17_SED_055-060CM	Percent Solids	45.9	O-04	45.9	J	HT	% BY WT.
1710916	% Solids	1710916-35	MM-T5-C3-17_SED_060-065CM	Percent Solids	52.3	O-04	52.3	J	HT	% BY WT.
1710916	% Solids	1710916-36	MM-T5-C3-17_SED_065-070CM	Percent Solids	42.1	O-04	42.1	J	HT	% BY WT.
1710916	% Solids	1710916-37	MM-T5-C3-17_SED_070-075CM	Percent Solids	43.9	O-04	43.9	J	HT	% BY WT.
1710916	% Solids	1710916-38	MM-T5-C3-17_SED_075-080CM	Percent Solids	43.5	O-04	43.5	J	HT	% BY WT.
1710917	% Solids	1710917-01	OR-T3-C4-A-17_SED_000-001CM	Percent Solids	45.7	O-04	45.7	J	HT	% BY WT.
1710917	% Solids	1710917-02	OR-T3-C4-A-17_SED_001-002CM	Percent Solids	42	O-04	42	J	HT	% BY WT.
1710917	% Solids	1710917-03	OR-T3-C4-A-17_SED_002-003CM	Percent Solids	43	O-04	43	J	HT	% BY WT.
1710917	% Solids	1710917-04	OR-T3-C4-A-17_SED_003-004CM	Percent Solids	42.2	O-04	42.2	J	HT	% BY WT.
1710917	% Solids	1710917-05	OR-T3-C4-A-17_SED_004-005CM	Percent Solids	42.1	O-04	42.1	J	HT	% BY WT.
1710917	% Solids	1710917-06	OR-T3-C4-A-17_SED_005-006CM	Percent Solids	41.6	O-04	41.6	J	HT	% BY WT.
1710917	% Solids	1710917-07	OR-T3-C4-A-17_SED_006-007CM	Percent Solids	41.5	O-04	41.5	J	HT	% BY WT.
1710917	% Solids	1710917-08	OR-T3-C4-A-17_SED_007-008CM	Percent Solids	43.3	O-04	43.3	J	HT	% BY WT.
1710917	% Solids	1710917-09	OR-T3-C4-A-17_SED_008-009CM	Percent Solids	40.9	O-04	40.9	J	HT	% BY WT.
1710917	% Solids	1710917-10	OR-T3-C4-A-17_SED_009-010CM	Percent Solids	43.2	O-04	43.2	J	HT	% BY WT.
1710917	% Solids	1710917-11	OR-T3-C4-A-17_SED_010-011CM	Percent Solids	41.5	O-04	41.5	J	HT	% BY WT.
1710917	% Solids	1710917-12	OR-T3-C4-A-17_SED_011-012CM	Percent Solids	43.2	O-04	43.2	J	HT	% BY WT.
1710917	% Solids	1710917-13	OR-T3-C4-A-17_SED_012-013CM	Percent Solids	45.7	O-04	45.7	J	HT	% BY WT.
1710917	% Solids	1710917-14	OR-T3-C4-A-17_SED_013-014CM	Percent Solids	44.7	O-04	44.7	J	HT	% BY WT.

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1710917	% Solids	1710917-15	OR-T3-C4-A-17_SED_014-015CM	Percent Solids	47.9	O-04	47.9	J	HT	% BY WT.
1710917	% Solids	1710917-16	OR-T3-C4-A-17_SED_015-016CM	Percent Solids	50.2	O-04	50.2	J	HT	% BY WT.
1710917	% Solids	1710917-17	OR-T3-C4-A-17_SED_016-017CM	Percent Solids	49.8	O-04	49.8	J	HT	% BY WT.
1710917	% Solids	1710917-18	OR-T3-C4-A-17_SED_017-018CM	Percent Solids	49.5	O-04	49.5	J	HT	% BY WT.
1710917	% Solids	1710917-19	OR-T3-C4-A-17_SED_018-019CM	Percent Solids	52.7	O-04	52.7	J	HT	% BY WT.
1710917	% Solids	1710917-20	OR-T3-C4-A-17_SED_019-020CM	Percent Solids	51	O-04	51	J	HT	% BY WT.
1710917	% Solids	1710917-21	OR-T3-C4-A-17_SED_020-022CM	Percent Solids	50	O-04	50	J	HT	% BY WT.
1710917	% Solids	1710917-22	OR-T3-C4-A-17_SED_022-024CM	Percent Solids	52	O-04	52	J	HT	% BY WT.
1710917	% Solids	1710917-23	OR-T3-C4-A-17_SED_024-026CM	Percent Solids	54	O-04	54	J	HT	% BY WT.
1710917	% Solids	1710917-24	OR-T3-C4-A-17_SED_026-028CM	Percent Solids	52.9	O-04	52.9	J	HT	% BY WT.
1710917	% Solids	1710917-25	OR-T3-C4-A-17_SED_028-030CM	Percent Solids	54.1	O-04	54.1	J	HT	% BY WT.
1710917	% Solids	1710917-26	OR-T3-C4-A-17_SED_030-032CM	Percent Solids	54.2	O-04	54.2	J	HT	% BY WT.
1710917	% Solids	1710917-27	OR-T3-C4-A-17_SED_032-034CM	Percent Solids	50.8	O-04	50.8	J	HT	% BY WT.
1710917	% Solids	1710917-28	OR-T3-C4-A-17_SED_034-036CM	Percent Solids	56.3	O-04	56.3	J	HT	% BY WT.
1710917	% Solids	1710917-29	OR-T3-C4-A-17_SED_036-038CM	Percent Solids	61.5	O-04	61.5	J	HT	% BY WT.
1710917	% Solids	1710917-30	OR-T3-C4-A-17_SED_038-040CM	Percent Solids	62.4	O-04	62.4	J	HT	% BY WT.
1710917	% Solids	1710917-31	OR-T3-C4-A-17_SED_040-045CM	Percent Solids	64	O-04	64	J	HT	% BY WT.
1710917	% Solids	1710917-32	OR-T3-C4-A-17_SED_045-050CM	Percent Solids	66.7	O-04	66.7	J	HT	% BY WT.
1710917	% Solids	1710917-34	OR-T3-C4-A-17_SED_055-060CM	Percent Solids	66	O-04	66	J	HT	% BY WT.
1710917	% Solids	1710917-35	OR-T3-C4-A-17_SED_060-065CM	Percent Solids	62.7	O-04	62.7	J	HT	% BY WT.
1710917	% Solids	1710917-36	OR-T3-C4-A-17_SED_065-070CM	Percent Solids	65.6	O-04	65.6	J	HT	% BY WT.
1710917	% Solids	1710917-37	OR-T3-C4-A-17_SED_070-075CM	Percent Solids	41.1	O-04	41.1	J	HT	% BY WT.
1710917	% Solids	1710917-38	OR-T3-C4-A-17_SED_075-080CM	Percent Solids	49	O-04	49	J	HT	% BY WT.
1710917	% Solids	1710917-39	OR-T3-C4-A-17_SED_080-085CM	Percent Solids	63.4	O-04	63.4	J	HT	% BY WT.
1710918	% Solids	1710918-01	VN-MU3-GC-1-G-17_SED_00-01	Percent Solids	50.6	O-04	50.6	J	HT	% BY WT.
1710918	% Solids	1710918-02	VN-MU3-GC-1-G-17_SED_01-03	Percent Solids	49.4	O-04	49.4	J	HT	% BY WT.
1710918	% Solids	1710918-03	VN-MU3-GC-1-G-17_SED_03-05	Percent Solids	49.2	O-04	49.2	J	HT	% BY WT.
1710918	% Solids	1710918-04	VN-MU3-GC-1-G-17_SED_05-07	Percent Solids	53.4	O-04	53.4	J	HT	% BY WT.
1710918	% Solids	1710918-05	VN-MU3-GC-1-G-17_SED_07-10	Percent Solids	57.4	O-04	57.4	J	HT	% BY WT.
1710918	% Solids	1710918-06	VN-MU3-GC-1-G-17_SED_10-15	Percent Solids	52.5	O-04	52.5	J	HT	% BY WT.
1711046	% Solids	1711046-01	PBR-20-G-17_SED_00-01	Percent Solids	55.2	[1]	55.2	J	HT	% BY WT.
1711046	% Solids	1711046-02	PBR-20-G-17_SED_01-03	Percent Solids	60.1	[2]	60.1	J	HT	% BY WT.

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1711046	% Solids	1711046-03	PBR-20-G-17_SED_03-05	Percent Solids	56.9	[3]	56.9	J	HT	% BY WT.
1711047	% Solids	1711047-01	UPB-MU11-GC-1-E-17_SED_00-01	Percent Solids	31.2	[1]	31.2	J	HT	% BY WT.
1711047	% Solids	1711047-02	UPB-MU11-GC-1-E-17_SED_01-03	Percent Solids	44.6	[2]	44.6	J	HT	% BY WT.
1711047	% Solids	1711047-03	UPB-MU11-GC-1-E-17_SED_03-05	Percent Solids	40.8	[3]	40.8	J	HT	% BY WT.
1711047	% Solids	1711047-04	UPB-MU11-GC-1-E-17_SED_05-07	Percent Solids	44.6	[4]	44.6	J	HT	% BY WT.
1711047	% Solids	1711047-05	UPB-MU11-GC-1-E-17_SED_07-10	Percent Solids	44	[5]	44	J	HT	% BY WT.
1711047	% Solids	1711047-06	UPB-MU11-GC-1-E-17_SED_07-10_DUP	Percent Solids	46.5	[6]	46.5	J	HT	% BY WT.
1711050	% Solids	1711050-01	VE-MU4-GC-1-F-17_SED_00-01	Percent Solids	34.9	[1]	34.9	J	HT	% BY WT.
1711050	% Solids	1711050-02	VE-MU4-GC-1-F-17_SED_01-03	Percent Solids	51	[2]	51	J	HT	% BY WT.
1711050	7474_1631	1711050-03	VE-MU4-GC-1-F-17_SED_03-05	Mercury	859		859	J	FD	NG/G
1711050	% Solids	1711050-03	VE-MU4-GC-1-F-17_SED_03-05	Percent Solids	69.9	[3]	69.9	J	HT	% BY WT.
1711050	7474_1631	1711050-04	VE-MU4-GC-1-F-17_SED_03-05_DUP	Mercury	309		309	J	FD	NG/G
1711050	% Solids	1711050-04	VE-MU4-GC-1-F-17_SED_03-05_DUP	Percent Solids	64.8	[4]	64.8	J	HT	% BY WT.
1711056	% Solids	1711056-01	OR-T3-C5-E-17_SED_00-01	Percent Solids	38.3	[1]	38.3	J	HT	% BY WT.
1711056	% Solids	1711056-02	OR-T3-C5-E-17_SED_01-03	Percent Solids	44.2	[2]	44.2	J	HT	% BY WT.
1711056	% Solids	1711056-03	OR-T3-C5-E-17_SED_03-05	Percent Solids	42.4	[3]	42.4	J	HT	% BY WT.
1711056	% Solids	1711056-04	OR-T3-C5-E-17_SED_05-07	Percent Solids	41.8	[4]	41.8	J	HT	% BY WT.
1711056	% Solids	1711056-05	OR-T3-C5-E-17_SED_07-10	Percent Solids	41.5	[5]	41.5	J	HT	% BY WT.
1711057	% Solids	1711057-01	OR-T3-C4-F-17_SED_00-01	Percent Solids	49.8	[1]	49.8	J	HT	% BY WT.
1711057	% Solids	1711057-02	OR-T3-C4-F-17_SED_01-03	Percent Solids	41	[2]	41	J	HT	% BY WT.
1711057	% Solids	1711057-03	OR-T3-C4-F-17_SED_03-05	Percent Solids	45	[3]	45	J	HT	% BY WT.
1711057	% Solids	1711057-04	OR-T3-C4-F-17_SED_03-05_DUP	Percent Solids	47.4	[4]	47.4	J	HT	% BY WT.
1711057	% Solids	1711057-05	OR-T3-C4-F-17_SED_05-07	Percent Solids	50.7	[5]	50.7	J	HT	% BY WT.
1711057	% Solids	1711057-06	OR-T3-C4-F-17_SED_07-10	Percent Solids	51.1	[6]	51.1	J	HT	% BY WT.
1711058	% Solids	1711058-01	OR-T3-C2-F-17_SED_00-01	Percent Solids	35.4	[1]	35.4	J	HT	% BY WT.
1711058	% Solids	1711058-02	OR-T3-C2-F-17_SED_01-03	Percent Solids	37.9	[2]	37.9	J	HT	% BY WT.
1711058	% Solids	1711058-03	OR-T3-C2-F-17_SED_03-05	Percent Solids	36.9	[3]	36.9	J	HT	% BY WT.
1711058	% Solids	1711058-04	OR-T3-C2-F-17_SED_03-05_DUP	Percent Solids	38.6	[4]	38.6	J	HT	% BY WT.
1711058	% Solids	1711058-05	OR-T3-C2-F-17_SED_05-07	Percent Solids	39.2	[5]	39.2	J	HT	% BY WT.
1711059	% Solids	1711059-01	OR-T3-C1-F-17_SED_00-01	Percent Solids	35.5	[1]	35.5	J	HT	% BY WT.
1711059	% Solids	1711059-02	OR-T3-C1-F-17_SED_01-03	Percent Solids	35.2	[2]	35.2	J	HT	% BY WT.
1711059	% Solids	1711059-03	OR-T3-C1-F-17_SED_03-05	Percent Solids	35.7	[3]	35.7	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1711059	% Solids	1711059-04	OR-T3-C1-F-17_SED_05-07	Percent Solids	36.4	[4]	36.4	J	HT	% BY WT.
1711059	% Solids	1711059-05	OR-T3-C1-F-17_SED_07-10	Percent Solids	38.1	[5]	38.1	J	HT	% BY WT.
1711059	% Solids	1711059-06	OR-T3-C1-F-17_SED_10-15	Percent Solids	26.8	[6]	26.8	J	HT	% BY WT.
1711059	% Solids	1711059-07	OR-T3-C1-F-17_SED_15-20	Percent Solids	30.4	[7]	30.4	J	HT	% BY WT.
1711059	% Solids	1711059-08	OR-T3-C1-F-17_SED_15-20_DUP	Percent Solids	31.4	[8]	31.4	J	HT	% BY WT.
1711060	% Solids	1711060-01	OR-T2-C5-E-17_SED_00-01	Percent Solids	37.6	[1]	37.6	J	HT	% BY WT.
1711060	% Solids	1711060-02	OR-T2-C5-E-17_SED_01-03	Percent Solids	36.2	[2]	36.2	J	HT	% BY WT.
1711060	% Solids	1711060-03	OR-T2-C5-E-17_SED_03-05	Percent Solids	44.5	[3]	44.5	J	HT	% BY WT.
1711060	% Solids	1711060-04	OR-T2-C5-E-17_SED_05-07	Percent Solids	44.8	[4]	44.8	J	HT	% BY WT.
1711060	% Solids	1711060-05	OR-T2-C5-E-17_SED_07-10	Percent Solids	44.7	[5]	44.7	J	HT	% BY WT.
1711061	% Solids	1711061-01	OR-T2-C4-C-17_SED_00-01	Percent Solids	18	[1]	18	J	HT	% BY WT.
1711061	% Solids	1711061-02	OR-T2-C4-C-17_SED_01-03	Percent Solids	40.7	[2]	40.7	J	HT	% BY WT.
1711061	% Solids	1711061-03	OR-T2-C4-C-17_SED_03-05	Percent Solids	40.5	[3]	40.5	J	HT	% BY WT.
1711061	% Solids	1711061-04	OR-T2-C4-C-17_SED_05-07	Percent Solids	44.9	[4]	44.9	J	HT	% BY WT.
1711061	% Solids	1711061-05	OR-T2-C4-C-17_SED_07-10	Percent Solids	35.9	O-04	35.9	J	HT	% BY WT.
1711062	% Solids	1711062-01	PBR-18-I-17_SED_00-01	Percent Solids	36.9	O-04	36.9	J	HT	% BY WT.
1711062	% Solids	1711062-02	PBR-18-I-17_SED_01-03	Percent Solids	36.8	O-04	36.8	J	HT	% BY WT.
1711062	% Solids	1711062-03	PBR-18-I-17_SED_03-05	Percent Solids	37.1	O-04	37.1	J	HT	% BY WT.
1711062	% Solids	1711062-04	PBR-18-I-17_SED_05-07	Percent Solids	40.1	O-04	40.1	J	HT	% BY WT.
1711063	% Solids	1711063-01	OR-T2-C3-C-17_SED_00-01	Percent Solids	42.3	O-04	42.3	J	HT	% BY WT.
1711063	% Solids	1711063-02	OR-T2-C3-C-17_SED_01-03	Percent Solids	47.9	O-04	47.9	J	HT	% BY WT.
1711063	% Solids	1711063-03	OR-T2-C3-C-17_SED_03-05	Percent Solids	50.6	O-04	50.6	J	HT	% BY WT.
1711063	% Solids	1711063-04	OR-T2-C3-C-17_SED_05-07	Percent Solids	48.5	O-04	48.5	J	HT	% BY WT.
1711063	% Solids	1711063-05	OR-T2-C3-C-17_SED_07-10	Percent Solids	47.4	O-04	47.4	J	HT	% BY WT.
1711063	% Solids	1711063-06	OR-T2-C3-C-17_SED_07-10_DUP	Percent Solids	42.8	O-04	42.8	J	HT	% BY WT.
1711064	% Solids	1711064-01	OR-T2-C2-E-17_SED_00-01	Percent Solids	33.3	O-04	33.3	J	HT	% BY WT.
1711064	% Solids	1711064-02	OR-T2-C2-E-17_SED_01-03	Percent Solids	38.6	O-04	38.6	J	HT	% BY WT.
1711064	% Solids	1711064-03	OR-T2-C2-E-17_SED_03-05	Percent Solids	38.8	O-04	38.8	J	HT	% BY WT.
1711064	% Solids	1711064-04	OR-T2-C2-E-17_SED_05-07	Percent Solids	48.4	O-04	48.4	J	HT	% BY WT.
1711064	% Solids	1711064-05	OR-T2-C2-E-17_SED_07-10	Percent Solids	46.9	O-04	46.9	J	HT	% BY WT.
1711065	% Solids	1711065-01	OR-T2-C1-D-17_SED_00-01	Percent Solids	40.3	O-04	40.3	J	HT	% BY WT.
1711065	% Solids	1711065-02	OR-T2-C1-D-17_SED_01-03	Percent Solids	41.7	O-04	41.7	J	HT	% BY WT.

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1711065	% Solids	1711065-03	OR-T2-C1-D-17_SED_03-05	Percent Solids	43	O-04	43	J	HT	% BY WT.
1711065	% Solids	1711065-04	OR-T2-C1-D-17_SED_05-07	Percent Solids	42	O-04	42	J	HT	% BY WT.
1711065	% Solids	1711065-05	OR-T2-C1-D-17_SED_05-07_DUP	Percent Solids	42.6	O-04	42.6	J	HT	% BY WT.
1711065	% Solids	1711065-06	OR-T2-C1-D-17_SED_07-10	Percent Solids	48.1	O-04	48.1	J	HT	% BY WT.
1711065	% Solids	1711065-07	OR-T2-C1-D-17_SED_10-15	Percent Solids	59.3	O-04	59.3	J	HT	% BY WT.
1711065	% Solids	1711065-08	OR-T2-C1-D-17_SED_15-20	Percent Solids	66.2	O-04	66.2	J	HT	% BY WT.
1711066	% Solids	1711066-01	OR-T1-C5-C-17_SED_00-01	Percent Solids	32.2	O-04	32.2	J	HT	% BY WT.
1711066	% Solids	1711066-02	OR-T1-C5-C-17_SED_01-03	Percent Solids	47.2	O-04	47.2	J	HT	% BY WT.
1711066	% Solids	1711066-03	OR-T1-C5-C-17_SED_01-03_DUP	Percent Solids	49.1	O-04	49.1	J	HT	% BY WT.
1711066	% Solids	1711066-04	OR-T1-C5-C-17_SED_03-05	Percent Solids	46.5	O-04	46.5	J	HT	% BY WT.
1711066	% Solids	1711066-05	OR-T1-C5-C-17_SED_05-07	Percent Solids	47.5	O-04	47.5	J	HT	% BY WT.
1711066	% Solids	1711066-06	OR-T1-C5-C-17_SED_07-10	Percent Solids	47.8	O-04	47.8	J	HT	% BY WT.
1711067	% Solids	1711067-01	MM-T4-C2-F-17_SED_00-01	Percent Solids	45.1	O-04	45.1	J	HT	% BY WT.
1711067	% Solids	1711067-02	MM-T4-C2-F-17_SED_01-03	Percent Solids	42.6	O-04	42.6	J	HT	% BY WT.
1711067	% Solids	1711067-03	MM-T4-C2-F-17_SED_01-03_DUP	Percent Solids	44.4	O-04	44.4	J	HT	% BY WT.
1711067	% Solids	1711067-04	MM-T4-C2-F-17_SED_03-05	Percent Solids	45.9	O-04	45.9	J	HT	% BY WT.
1711067	% Solids	1711067-05	MM-T4-C2-F-17_SED_05-07	Percent Solids	47.5	O-04	47.5	J	HT	% BY WT.
1711067	% Solids	1711067-06	MM-T4-C2-F-17_SED_07-10	Percent Solids	38.2	O-04	38.2	J	HT	% BY WT.
1711068	% Solids	1711068-01	OR-T1-C3-C-17_SED_00-01	Percent Solids	53.5	O-04	53.5	J	HT	% BY WT.
1711068	% Solids	1711068-02	OR-T1-C3-C-17_SED_01-03	Percent Solids	43.1	O-04	43.1	J	HT	% BY WT.
1711068	% Solids	1711068-03	OR-T1-C3-C-17_SED_03-05	Percent Solids	42.6	O-04	42.6	J	HT	% BY WT.
1711068	% Solids	1711068-04	OR-T1-C3-C-17_SED_05-07	Percent Solids	44.4	O-04	44.4	J	HT	% BY WT.
1711069	% Solids	1711069-01	OR-T1-C2-C-17_SED_00-01	Percent Solids	45	O-04	45	J	HT	% BY WT.
1711069	% Solids	1711069-02	OR-T1-C2-C-17_SED_01-03	Percent Solids	43.3	O-04	43.3	J	HT	% BY WT.
1711069	% Solids	1711069-03	OR-T1-C2-C-17_SED_03-05	Percent Solids	43.6	O-04	43.6	J	HT	% BY WT.
1711069	% Solids	1711069-04	OR-T1-C2-C-17_SED_05-07	Percent Solids	45.9	O-04	45.9	J	HT	% BY WT.
1711069	% Solids	1711069-05	OR-T1-C2-C-17_SED_07-10	Percent Solids	41.1	O-04	41.1	J	HT	% BY WT.
1711070	% Solids	1711070-01	MM-T3-C4-C-17_SED_00-01	Percent Solids	38.6	O-04	38.6	J	HT	% BY WT.
1711070	% Solids	1711070-02	MM-T3-C4-C-17_SED_01-03	Percent Solids	47.3	O-04	47.3	J	HT	% BY WT.
1711070	% Solids	1711070-03	MM-T3-C4-C-17_SED_03-05	Percent Solids	38.4	O-04	38.4	J	HT	% BY WT.
1711070	% Solids	1711070-04	MM-T3-C4-C-17_SED_05-07	Percent Solids	46.8	O-04	46.8	J	HT	% BY WT.
1711070	% Solids	1711070-05	MM-T3-C4-C-17_SED_07-10	Percent Solids	46.8	O-04	46.8	J	HT	% BY WT.

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1711071	% Solids	1711071-01	MM-T1-C2-D-17_SED_00-01	Percent Solids	43.1	O-04	43.1	J	HT	% BY WT.
1711071	% Solids	1711071-02	MM-T1-C2-D-17_SED_01-03	Percent Solids	38.4	O-04	38.4	J	HT	% BY WT.
1711071	% Solids	1711071-03	MM-T1-C2-D-17_SED_03-05	Percent Solids	43.8	O-04	43.8	J	HT	% BY WT.
1711071	% Solids	1711071-04	MM-T1-C2-D-17_SED_05-07	Percent Solids	39.4	O-04	39.4	J	HT	% BY WT.
1711071	% Solids	1711071-05	MM-T1-C2-D-17_SED_05-07_DUP	Percent Solids	39.2	O-04	39.2	J	HT	% BY WT.
1711071	% Solids	1711071-06	MM-T1-C2-D-17_SED_07-10	Percent Solids	44.9	O-04	44.9	J	HT	% BY WT.
1711073	% Solids	1711073-01	ES-01-F-17_SED_00-01	Percent Solids	45.2	O-04	45.2	J	HT	% BY WT.
1711073	% Solids	1711073-02	ES-01-F-17_SED_01-03	Percent Solids	37.8	O-04	37.8	J	HT	% BY WT.
1711073	% Solids	1711073-03	ES-01-F-17_SED_01-03_DUP	Percent Solids	44	O-04	44	J	HT	% BY WT.
1711073	% Solids	1711073-04	ES-01-F-17_SED_03-05	Percent Solids	35.2	O-04	35.2	J	HT	% BY WT.
1711073	% Solids	1711073-05	ES-01-F-17_SED_05-07	Percent Solids	35.6	O-04	35.6	J	HT	% BY WT.
1711077	% Solids	1711077-01	ES-18-F-17_SED_00-01	Percent Solids	61.6	O-04	61.6	J	HT	% BY WT.
1711077	% Solids	1711077-02	ES-18-F-17_SED_01-03	Percent Solids	56.6	O-04	56.6	J	HT	% BY WT.
1711077	% Solids	1711077-03	ES-18-F-17_SED_03-05	Percent Solids	59	O-04	59	J	HT	% BY WT.
1711077	% Solids	1711077-04	ES-18-F-17_SED_05-07	Percent Solids	57.2	O-04	57.2	J	HT	% BY WT.
1711083	% Solids	1711083-01	MM-T3-C2-F-17_SED_00-01	Percent Solids	38.3	[1]	38.3	J	HT	% BY WT.
1711083	% Solids	1711083-02	MM-T3-C2-F-17_SED_01-03	Percent Solids	39.8	[2]	39.8	J	HT	% BY WT.
1711083	% Solids	1711083-03	MM-T3-C2-F-17_SED_03-05	Percent Solids	30.7	[3]	30.7	J	HT	% BY WT.
1711083	% Solids	1711083-04	MM-T3-C2-F-17_SED_05-07	Percent Solids	29.2	[4]	29.2	J	HT	% BY WT.
1711084	% Solids	1711084-01	MM-T3-C3-C-17_SED_00-01	Percent Solids	81.1	[1]	81.1	J	HT	% BY WT.
1711084	% Solids	1711084-02	MM-T3-C3-C-17_SED_01-03	Percent Solids	61.9	[2]	61.9	J	HT	% BY WT.
1711084	% Solids	1711084-03	MM-T3-C3-C-17_SED_03-05	Percent Solids	55.4	[3]	55.4	J	HT	% BY WT.
1711085	% Solids	1711085-01	MM-T2-C8-B-17_SED_00-01	Percent Solids	25.1	[1]	25.1	J	HT	% BY WT.
1711085	% Solids	1711085-02	MM-T2-C8-B-17_SED_01-03	Percent Solids	24.9	[2]	24.9	J	HT	% BY WT.
1711085	% Solids	1711085-03	MM-T2-C8-B-17_SED_03-05	Percent Solids	30.8	[3]	30.8	J	HT	% BY WT.
1711085	% Solids	1711085-04	MM-T2-C8-B-17_SED_05-07	Percent Solids	25.6	[4]	25.6	J	HT	% BY WT.
1711085	% Solids	1711085-05	MM-T2-C8-B-17_SED_07-10	Percent Solids	23	[5]	23	J	HT	% BY WT.
1711151	% Solids	1711151-01	PBR-28-17_SED_00-01	Percent Solids	39.5	O-04	39.5	J	HT	% BY WT.
1711151	% Solids	1711151-02	PBR-28-17_SED_01-03	Percent Solids	45.4	O-04	45.4	J	HT	% BY WT.
1711151	% Solids	1711151-03	PBR-28-17_SED_03-05	Percent Solids	43.3	O-04	43.3	J	HT	% BY WT.
1711151	% Solids	1711151-04	PBR-28-17_SED_05-07	Percent Solids	47.3	O-04	47.3	J	HT	% BY WT.
1711151	% Solids	1711151-05	PBR-28-17_SED_05-07_DUP	Percent Solids	46.8	O-04	46.8	J	HT	% BY WT.

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1711151	% Solids	1711151-06	PBR-28-17_SED_07-10	Percent Solids	54.5	O-04	54.5	J	HT	% BY WT.
1711156	% Solids	1711156-01	MM-T2-C7-A-17_SED_000-001CM	Percent Solids	45.5	O-04	45.5	J	HT	% BY WT.
1711156	% Solids	1711156-02	MM-T2-C7-A-17_SED_001-002CM	Percent Solids	49	O-04	49	J	HT	% BY WT.
1711156	% Solids	1711156-03	MM-T2-C7-A-17_SED_002-003CM	Percent Solids	47.2	O-04	47.2	J	HT	% BY WT.
1711156	% Solids	1711156-04	MM-T2-C7-A-17_SED_003-004CM	Percent Solids	47	O-04	47	J	HT	% BY WT.
1711156	% Solids	1711156-05	MM-T2-C7-A-17_SED_004-005CM	Percent Solids	46.2	O-04	46.2	J	HT	% BY WT.
1711156	% Solids	1711156-06	MM-T2-C7-A-17_SED_005-006CM	Percent Solids	47.8	O-04	47.8	J	HT	% BY WT.
1711156	% Solids	1711156-07	MM-T2-C7-A-17_SED_006-007CM	Percent Solids	49.1	O-04	49.1	J	HT	% BY WT.
1711156	% Solids	1711156-08	MM-T2-C7-A-17_SED_007-008CM	Percent Solids	49.3	O-04	49.3	J	HT	% BY WT.
1711156	% Solids	1711156-09	MM-T2-C7-A-17_SED_008-009CM	Percent Solids	49	O-04	49	J	HT	% BY WT.
1711156	% Solids	1711156-10	MM-T2-C7-A-17_SED_009-010CM	Percent Solids	46.3	O-04	46.3	J	HT	% BY WT.
1711156	% Solids	1711156-11	MM-T2-C7-A-17_SED_010-011CM	Percent Solids	41.7	O-04	41.7	J	HT	% BY WT.
1711156	% Solids	1711156-12	MM-T2-C7-A-17_SED_011-012CM	Percent Solids	40.2	O-04	40.2	J	HT	% BY WT.
1711156	% Solids	1711156-13	MM-T2-C7-A-17_SED_012-013CM	Percent Solids	43.7	O-04	43.7	J	HT	% BY WT.
1711156	% Solids	1711156-14	MM-T2-C7-A-17_SED_013-014CM	Percent Solids	42	O-04	42	J	HT	% BY WT.
1711156	% Solids	1711156-15	MM-T2-C7-A-17_SED_014-015CM	Percent Solids	43	O-04	43	J	HT	% BY WT.
1711156	% Solids	1711156-16	MM-T2-C7-A-17_SED_015-016CM	Percent Solids	44.4	O-04	44.4	J	HT	% BY WT.
1711156	% Solids	1711156-17	MM-T2-C7-A-17_SED_016-017CM	Percent Solids	41.9	O-04	41.9	J	HT	% BY WT.
1711156	% Solids	1711156-18	MM-T2-C7-A-17_SED_017-018CM	Percent Solids	39.8	O-04	39.8	J	HT	% BY WT.
1711156	% Solids	1711156-19	MM-T2-C7-A-17_SED_018-019CM	Percent Solids	36.8	O-04	36.8	J	HT	% BY WT.
1711156	% Solids	1711156-20	MM-T2-C7-A-17_SED_019-020CM	Percent Solids	38.8	O-04	38.8	J	HT	% BY WT.
1711156	% Solids	1711156-21	MM-T2-C7-A-17_SED_020-022CM	Percent Solids	39.5	O-04	39.5	J	HT	% BY WT.
1711156	% Solids	1711156-22	MM-T2-C7-A-17_SED_022-024CM	Percent Solids	39.9	O-04	39.9	J	HT	% BY WT.
1711156	% Solids	1711156-23	MM-T2-C7-A-17_SED_024-026CM	Percent Solids	37.3	O-04	37.3	J	HT	% BY WT.
1711156	% Solids	1711156-24	MM-T2-C7-A-17_SED_026-028CM	Percent Solids	38	O-04	38	J	HT	% BY WT.
1711156	% Solids	1711156-25	MM-T2-C7-A-17_SED_028-030CM	Percent Solids	38.5	O-04	38.5	J	HT	% BY WT.
1711156	% Solids	1711156-26	MM-T2-C7-A-17_SED_030-032CM	Percent Solids	40.9	O-04	40.9	J	HT	% BY WT.
1711156	% Solids	1711156-27	MM-T2-C7-A-17_SED_032-034CM	Percent Solids	38.7	O-04	38.7	J	HT	% BY WT.
1711156	% Solids	1711156-28	MM-T2-C7-A-17_SED_034-036CM	Percent Solids	34.9	O-04	34.9	J	HT	% BY WT.
1711156	% Solids	1711156-29	MM-T2-C7-A-17_SED_036-038CM	Percent Solids	34.4	O-04	34.4	J	HT	% BY WT.
1711156	% Solids	1711156-30	MM-T2-C7-A-17_SED_038-040CM	Percent Solids	40.7	O-04	40.7	J	HT	% BY WT.
1711156	% Solids	1711156-31	MM-T2-C7-A-17_SED_040-045CM	Percent Solids	39.2	O-04	39.2	J	HT	% BY WT.

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1711156	% Solids	1711156-32	MM-T2-C7-A-17_SED_045-050CM	Percent Solids	42.4	O-04	42.4	J	HT	% BY WT.
1711156	% Solids	1711156-33	MM-T2-C7-A-17_SED_050-055CM	Percent Solids	40.7	O-04	40.7	J	HT	% BY WT.
1711171	% Solids	1711171-01	OR-T3-C1-B-17_SED_000-001CM	Percent Solids	46.5	O-04	46.5	J	HT	% BY WT.
1711171	% Solids	1711171-02	OR-T3-C1-B-17_SED_001-002CM	Percent Solids	48	O-04	48	J	HT	% BY WT.
1711171	% Solids	1711171-03	OR-T3-C1-B-17_SED_002-003CM	Percent Solids	48.6	O-04	48.6	J	HT	% BY WT.
1711171	% Solids	1711171-04	OR-T3-C1-B-17_SED_003-004CM	Percent Solids	48.5	O-04	48.5	J	HT	% BY WT.
1711171	% Solids	1711171-05	OR-T3-C1-B-17_SED_004-005CM	Percent Solids	46	O-04	46	J	HT	% BY WT.
1711171	% Solids	1711171-06	OR-T3-C1-B-17_SED_005-006CM	Percent Solids	41.7	O-04	41.7	J	HT	% BY WT.
1711171	% Solids	1711171-07	OR-T3-C1-B-17_SED_006-007CM	Percent Solids	39.7	O-04	39.7	J	HT	% BY WT.
1711171	% Solids	1711171-08	OR-T3-C1-B-17_SED_007-008CM	Percent Solids	39.1	O-04	39.1	J	HT	% BY WT.
1711171	% Solids	1711171-09	OR-T3-C1-B-17_SED_008-009CM	Percent Solids	39.2	O-04	39.2	J	HT	% BY WT.
1711171	% Solids	1711171-10	OR-T3-C1-B-17_SED_009-010CM	Percent Solids	35.7	O-04	35.7	J	HT	% BY WT.
1711171	% Solids	1711171-11	OR-T3-C1-B-17_SED_010-011CM	Percent Solids	35.6	O-04	35.6	J	HT	% BY WT.
1711171	% Solids	1711171-12	OR-T3-C1-B-17_SED_011-012CM	Percent Solids	34.2	O-04	34.2	J	HT	% BY WT.
1711171	% Solids	1711171-13	OR-T3-C1-B-17_SED_012-013CM	Percent Solids	35.2	O-04	35.2	J	HT	% BY WT.
1711171	% Solids	1711171-14	OR-T3-C1-B-17_SED_013-014CM	Percent Solids	34.2	O-04	34.2	J	HT	% BY WT.
1711171	% Solids	1711171-15	OR-T3-C1-B-17_SED_014-015CM	Percent Solids	37	O-04	37	J	HT	% BY WT.
1711171	% Solids	1711171-16	OR-T3-C1-B-17_SED_015-016CM	Percent Solids	37.7	O-04	37.7	J	HT	% BY WT.
1711171	% Solids	1711171-17	OR-T3-C1-B-17_SED_016-017CM	Percent Solids	38.2	O-04	38.2	J	HT	% BY WT.
1711171	% Solids	1711171-18	OR-T3-C1-B-17_SED_017-018CM	Percent Solids	39.3	O-04	39.3	J	HT	% BY WT.
1711171	% Solids	1711171-19	OR-T3-C1-B-17_SED_018-019CM	Percent Solids	38.2	O-04	38.2	J	HT	% BY WT.
1711171	% Solids	1711171-20	OR-T3-C1-B-17_SED_019-020CM	Percent Solids	39.4	O-04	39.4	J	HT	% BY WT.
1711171	% Solids	1711171-21	OR-T3-C1-B-17_SED_020-022CM	Percent Solids	40.9	O-04	40.9	J	HT	% BY WT.
1711171	% Solids	1711171-22	OR-T3-C1-B-17_SED_022-024CM	Percent Solids	41.7	O-04	41.7	J	HT	% BY WT.
1711171	% Solids	1711171-23	OR-T3-C1-B-17_SED_024-026CM	Percent Solids	41.7	O-04	41.7	J	HT	% BY WT.
1711171	% Solids	1711171-24	OR-T3-C1-B-17_SED_026-028CM	Percent Solids	41.8	O-04	41.8	J	HT	% BY WT.
1711171	% Solids	1711171-25	OR-T3-C1-B-17_SED_028-030CM	Percent Solids	42	O-04	42	J	HT	% BY WT.
1711171	% Solids	1711171-26	OR-T3-C1-B-17_SED_030-032CM	Percent Solids	41.8	O-04	41.8	J	HT	% BY WT.
1711171	% Solids	1711171-27	OR-T3-C1-B-17_SED_032-034CM	Percent Solids	42.2	O-04	42.2	J	HT	% BY WT.
1711171	% Solids	1711171-28	OR-T3-C1-B-17_SED_034-036CM	Percent Solids	40.6	O-04	40.6	J	HT	% BY WT.
1711171	% Solids	1711171-29	OR-T3-C1-B-17_SED_036-038CM	Percent Solids	44.3	O-04	44.3	J	HT	% BY WT.
1711171	% Solids	1711171-30	OR-T3-C1-B-17_SED_038-040CM	Percent Solids	44	O-04	44	J	HT	% BY WT.

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
1711171	% Solids	1711171-31	OR-T3-C1-B-17_SED_040-045CM	Percent Solids	44.1	O-04	44.1	J	HT	% BY WT.
1711171	% Solids	1711171-32	OR-T3-C1-B-17_SED_045-050CM	Percent Solids	45.1	O-04	45.1	J	HT	% BY WT.
1711171	% Solids	1711171-33	OR-T3-C1-B-17_SED_050-055CM	Percent Solids	47	O-04	47	J	HT	% BY WT.
1711171	% Solids	1711171-34	OR-T3-C1-B-17_SED_055-060CM	Percent Solids	47.8	O-04	47.8	J	HT	% BY WT.
1711171	% Solids	1711171-35	OR-T3-C1-B-17_SED_060-065CM	Percent Solids	48.8	O-04	48.8	J	HT	% BY WT.
1711171	% Solids	1711171-36	OR-T3-C1-B-17_SED_065-070CM	Percent Solids	49.8	O-04	49.8	J	HT	% BY WT.
1711171	% Solids	1711171-37	OR-T3-C1-B-17_SED_070-075CM	Percent Solids	53.7	O-04	53.7	J	HT	% BY WT.
1711171	% Solids	1711171-38	OR-T3-C1-B-17_SED_075-080CM	Percent Solids	54.6	O-04	54.6	J	HT	% BY WT.
1711171	% Solids	1711171-39	OR-T3-C1-B-17_SED_080-085CM	Percent Solids	54.2	O-04	54.2	J	HT	% BY WT.
1711171	% Solids	1711171-40	OR-T3-C1-B-17_SED_085-090CM	Percent Solids	54.5	O-04	54.5	J	HT	% BY WT.
1711173	% Solids	1711173-01	OR-T1-C1-D-17_SED_00-01	Percent Solids	46.9	O-04	46.9	J	HT	% BY WT.
1711173	% Solids	1711173-02	OR-T1-C1-D-17_SED_01-03	Percent Solids	37.2	O-04	37.2	J	HT	% BY WT.
1711173	% Solids	1711173-03	OR-T1-C1-D-17_SED_03-05	Percent Solids	42.2	O-04	42.2	J	HT	% BY WT.
1711173	% Solids	1711173-04	OR-T1-C1-D-17_SED_05-07	Percent Solids	43.1	O-04	43.1	J	HT	% BY WT.
1711173	% Solids	1711173-05	OR-T1-C1-D-17_SED_07-10	Percent Solids	42.5	O-04	42.5	J	HT	% BY WT.
1711174	% Solids	1711174-01	MM-T3-C1-17_SED_000-001CM	Percent Solids	44.7	O-04	44.7	J	HT	% BY WT.
1711174	% Solids	1711174-02	MM-T3-C1-17_SED_000-001CM_DUP	Percent Solids	43.4	O-04	43.4	J	HT	% BY WT.
1711174	% Solids	1711174-03	MM-T3-C1-17_SED_001-002CM	Percent Solids	43.8	O-04	43.8	J	HT	% BY WT.
1711174	% Solids	1711174-04	MM-T3-C1-17_SED_001-002CM_DUP	Percent Solids	46.1	O-04	46.1	J	HT	% BY WT.
1711174	% Solids	1711174-05	MM-T3-C1-17_SED_002-003CM	Percent Solids	57.1	O-04	57.1	J	HT	% BY WT.
1711174	% Solids	1711174-06	MM-T3-C1-17_SED_003-004CM	Percent Solids	61.6	O-04	61.6	J	HT	% BY WT.
1711174	% Solids	1711174-07	MM-T3-C1-17_SED_003-004CM_DUP	Percent Solids	61.7	O-04	61.7	J	HT	% BY WT.
1711174	% Solids	1711174-08	MM-T3-C1-17_SED_004-005CM	Percent Solids	68.7	O-04	68.7	J	HT	% BY WT.
1711174	% Solids	1711174-09	MM-T3-C1-17_SED_004-005CM_DUP	Percent Solids	67.6	O-04	67.6	J	HT	% BY WT.
1711174	% Solids	1711174-10	MM-T3-C1-17_SED_005-006CM	Percent Solids	75.1	O-04	75.1	J	HT	% BY WT.
1711174	% Solids	1711174-11	MM-T3-C1-17_SED_005-006CM_DUP	Percent Solids	76	O-04	76	J	HT	% BY WT.
1711174	% Solids	1711174-12	MM-T3-C1-17_SED_006-007CM	Percent Solids	80.7	O-04	80.7	J	HT	% BY WT.
1711174	% Solids	1711174-13	MM-T3-C1-17_SED_006-007CM_DUP	Percent Solids	80.8	O-04	80.8	J	HT	% BY WT.
1711174	% Solids	1711174-14	MM-T3-C1-17_SED_007-008CM	Percent Solids	80.7	O-04	80.7	J	HT	% BY WT.
1711174	% Solids	1711174-15	MM-T3-C1-17_SED_007-008CM_DUP	Percent Solids	81.3	O-04	81.3	J	HT	% BY WT.
1711174	% Solids	1711174-16	MM-T3-C1-17_SED_008-009CM	Percent Solids	81.2	O-04	81.2	J	HT	% BY WT.
1711174	% Solids	1711174-17	MM-T3-C1-17_SED_008-009CM_DUP	Percent Solids	81.5	O-04	81.5	J	HT	% BY WT.

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1711174	% Solids	1711174-18	MM-T3-C1-17_SED_009-010CM	Percent Solids	81.9	O-04	81.9	J	HT	% BY WT.
1711174	% Solids	1711174-19	MM-T3-C1-17_SED_009-010CM_DUP	Percent Solids	82.2	O-04	82.2	J	HT	% BY WT.
1711174	% Solids	1711174-20	MM-T3-C1-17_SED_010-011CM	Percent Solids	77.3	O-04	77.3	J	HT	% BY WT.
1711174	% Solids	1711174-21	MM-T3-C1-17_SED_010-011CM_DUP	Percent Solids	77.7	O-04	77.7	J	HT	% BY WT.
1711174	% Solids	1711174-22	MM-T3-C1-17_SED_011-012CM	Percent Solids	76.5	O-04	76.5	J	HT	% BY WT.
1711174	% Solids	1711174-23	MM-T3-C1-17_SED_011-012CM_DUP	Percent Solids	77.1	O-04	77.1	J	HT	% BY WT.
1711174	% Solids	1711174-24	MM-T3-C1-17_SED_012-013CM	Percent Solids	76	O-04	76	J	HT	% BY WT.
1711174	% Solids	1711174-25	MM-T3-C1-17_SED_012-013CM_DUP	Percent Solids	75.8	O-04	75.8	J	HT	% BY WT.
1711174	% Solids	1711174-26	MM-T3-C1-17_SED_013-014CM	Percent Solids	75.9	O-04	75.9	J	HT	% BY WT.
1711174	% Solids	1711174-27	MM-T3-C1-17_SED_013-014CM_DUP	Percent Solids	76.7	O-04	76.7	J	HT	% BY WT.
1711174	% Solids	1711174-28	MM-T3-C1-17_SED_014-015CM	Percent Solids	79	O-04	79	J	HT	% BY WT.
1711174	% Solids	1711174-29	MM-T3-C1-17_SED_014-015CM_DUP	Percent Solids	78.3	O-04	78.3	J	HT	% BY WT.
1711174	7474_1631	1711174-30	MM-T3-C1-17_SED_015-016CM	Mercury	8.73		8.73	J	MS-L	NG/G
1711174	% Solids	1711174-30	MM-T3-C1-17_SED_015-016CM	Percent Solids	79.9	O-04	79.9	J	HT	% BY WT.
1711174	7474_1631	1711174-31	MM-T3-C1-17_SED_015-016CM_DUP	Mercury	7.58		7.58	J	MS-L	NG/G
1711174	% Solids	1711174-31	MM-T3-C1-17_SED_015-016CM_DUP	Percent Solids	79.3	O-04	79.3	J	HT	% BY WT.
1711174	% Solids	1711174-32	MM-T3-C1-17_SED_016-017CM	Percent Solids	76.3	O-04	76.3	J	HT	% BY WT.
1711174	% Solids	1711174-33	MM-T3-C1-17_SED_016-017CM_DUP	Percent Solids	77.2	O-04	77.2	J	HT	% BY WT.
1711174	% Solids	1711174-34	MM-T3-C1-17_SED_017-018CM	Percent Solids	78.5	O-04	78.5	J	HT	% BY WT.
1711174	% Solids	1711174-35	MM-T3-C1-17_SED_017-018CM_DUP	Percent Solids	79	O-04	79	J	HT	% BY WT.
1711174	% Solids	1711174-36	MM-T3-C1-17_SED_018-019CM	Percent Solids	80.4	O-04	80.4	J	HT	% BY WT.
1711174	% Solids	1711174-37	MM-T3-C1-17_SED_018-019CM_DUP	Percent Solids	79.8	O-04	79.8	J	HT	% BY WT.
1711174	% Solids	1711174-38	MM-T3-C1-17_SED_019-020CM	Percent Solids	79.9	O-04	79.9	J	HT	% BY WT.
1711174	% Solids	1711174-39	MM-T3-C1-17_SED_019-020CM_DUP	Percent Solids	80.3	O-04	80.3	J	HT	% BY WT.
1711174	% Solids	1711174-40	MM-T3-C1-17_SED_020-022CM	Percent Solids	79.4	O-04	79.4	J	HT	% BY WT.
1711174	% Solids	1711174-41	MM-T3-C1-17_SED_020-022CM_DUP	Percent Solids	79.4	O-04	79.4	J	HT	% BY WT.
1711174	% Solids	1711174-42	MM-T3-C1-17_SED_022-024CM	Percent Solids	80.1	O-04	80.1	J	HT	% BY WT.
1711174	% Solids	1711174-43	MM-T3-C1-17_SED_022-024CM_DUP	Percent Solids	79.6	O-04	79.6	J	HT	% BY WT.
1711174	% Solids	1711174-44	MM-T3-C1-17_SED_024-026CM	Percent Solids	81.9	O-04	81.9	J	HT	% BY WT.
1711174	% Solids	1711174-45	MM-T3-C1-17_SED_024-026CM_DUP	Percent Solids	81.6	O-04	81.6	J	HT	% BY WT.
1711328	% Solids	1711328-01	MM-T1-C1-B-17_SED_00-01	Percent Solids	41.1	[1]	41.1	J	HT	% BY WT.
1711328	% Solids	1711328-02	MM-T1-C1-B-17_SED_01-03	Percent Solids	34.2	[2]	34.2	J	HT	% BY WT.

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1711328	% Solids	1711328-03	MM-T1-C1-B-17_SED_03-05	Percent Solids	37.7	[3]	37.7	J	HT	% BY WT.
1711328	% Solids	1711328-04	MM-T1-C1-B-17_SED_03-05-Dup	Percent Solids	36.3	[4]	36.3	J	HT	% BY WT.
1711328	% Solids	1711328-05	MM-T1-C1-B-17_SED_05-07	Percent Solids	37.5	O-04	37.5	J	HT	% BY WT.
1711328	% Solids	1711328-06	MM-T1-C1-B-17_SED_07-10	Percent Solids	44.9	O-04	44.9	J	HT	% BY WT.
1712044	% Solids	1712044-01	MM-T3-C4-D-17_SED_022-024CM	Percent Solids	43.4	O-04	43.4	J	HT	% BY WT.
1712044	% Solids	1712044-02	MM-T3-C4-D-17_SED_022-024CM_DUP	Percent Solids	43.3	O-04	43.3	J	HT	% BY WT.
1712045	% Solids	1712045-01	MM-T4-C7-17_SED_045-050CM	Percent Solids	70.8	O-04	70.8	J	HT	% BY WT.
1712045	% Solids	1712045-02	MM-T4-C7-17_SED_045-050CM_DUP	Percent Solids	70.9	O-04	70.9	J	HT	% BY WT.
1712045	% Solids	1712045-03	MM-T4-C7-17_SED_055-060CM	Percent Solids	76.4	O-04	76.4	J	HT	% BY WT.
1712045	% Solids	1712045-04	MM-T4-C7-17_SED_055-060CM_DUP	Percent Solids	76.3	O-04	76.3	J	HT	% BY WT.
1712047	% Solids	1712047-01	OR-T3-C4-A-17_SED_050-055CM	Percent Solids	67.5	O-04	67.5	J	HT	% BY WT.
L1732774	LLOYD_KAHN	L1732774-24	MM-T3-C2-C-17_SED_026-028CM	Total Organic Carbon	0.1565		0.1565	J	LD	PERCENT
L1732774	LLOYD_KAHN	L1732774-28	MM-T3-C2-C-17_SED_034-036CM	Total Organic Carbon	0.104		0.104	J	LD	PERCENT
L1732774	LLOYD_KAHN	L1732774-32	MM-T3-C2-C-17_SED_045-050CM	Total Organic Carbon	0.082		0.082	J	LD	PERCENT
L1732774	LLOYD_KAHN	L1732774-34	MM-T3-C2-C-17_SED_055-060CM	Total Organic Carbon	0.1025		0.1025	J	LD	PERCENT
L1733612	LLOYD_KAHN	L1733612-20	OR-T1-C4-C-17_SED_019-020CM	Total Organic Carbon	2.305		2.305	J	LD	PERCENT
L1733612	LLOYD_KAHN	L1733612-27	OR-T1-C4-C-17_SED_032-034CM	Total Organic Carbon	2.605		2.605	J	LD	PERCENT
L1733618	2540G	L1733618-01	MM-T1-C3-B-17_SED_000-001CM	Percent Solids, Residual	33.3		33.3	J	LD	PERCENT
L1733618	LLOYD_KAHN	L1733618-13	MM-T1-C3-B-17_SED_012-013CM	Total Organic Carbon	0.1825		0.1825	J	LD	PERCENT
L1733618	LLOYD_KAHN	L1733618-15	MM-T1-C3-B-17_SED_014-015CM	Total Organic Carbon	0.1145		0.1145	J	LD	PERCENT
L1733618	LLOYD_KAHN	L1733618-20	MM-T1-C3-B-17_SED_019-020CM	Total Organic Carbon	0.1565		0.1565	J	LD	PERCENT
L1733618	LLOYD_KAHN	L1733618-22	MM-T1-C3-B-17_SED_022-024CM	Total Organic Carbon	0.164		0.164	J	LD	PERCENT
L1733618	LLOYD_KAHN	L1733618-28	MM-T1-C3-B-17_SED_034-036CM	Total Organic Carbon	0.1715		0.1715	J	LD	PERCENT
L1733618	LLOYD_KAHN	L1733618-35	MM-T1-C3-B-17_SED_060-065CM	Total Organic Carbon	0.1265		0.1265	J	LD	PERCENT
L1733618	LLOYD_KAHN	L1733618-37	MM-T1-C3-B-17_SED_070-075CM	Total Organic Carbon	0.152		0.152	J	LD	PERCENT
L1733619	LLOYD_KAHN	L1733619-08	MM-T2-C4-B-17_SED_007-008CM	Total Organic Carbon	2.455		2.455	J	MS-H	PERCENT
L1733619	LLOYD_KAHN	L1733619-22	MM-T2-C4-B-17_SED_022-024CM	Total Organic Carbon	0.7385		0.7385	J	LD	PERCENT
L1733619	LLOYD_KAHN	L1733619-36	MM-T2-C4-B-17_SED_065-070CM	Total Organic Carbon	0.4575		0.4575	J	LD	PERCENT
L1733620	LLOYD_KAHN	L1733620-09	MM-T2-C5-A-17_SED_008-009CM	Total Organic Carbon	2.89		2.89	J	LD	PERCENT
L1733620	LLOYD_KAHN	L1733620-14	MM-T2-C5-A-17_SED_013-014CM	Total Organic Carbon	6.045		6.045	J	LD	PERCENT
L1733620	LLOYD_KAHN	L1733620-29	MM-T2-C5-A-17_SED_036-038CM	Total Organic Carbon	1.435		1.435	J	MS-H	PERCENT
L1733621	2540G	L1733621-01	MM-T2-C6-A-17_SED_000-001CM	Percent Solids, Residual	46.8		46.8	J	LD	PERCENT

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L1736451	LLOYD_KAHN	L1736451-31	MM-T1-C2-B-17_SED_040-045CM	Total Organic Carbon	2.915		2.915	J	MS-H	PERCENT
L1736453	2540G	L1736453-01	OR-T1-C2-B-17_SED_000-001CM	Percent Solids, Residual	35		35	J	LD	PERCENT
L1736454	LLOYD_KAHN	L1736454-02	OR-T1-C5-A-17_SED_001-002CM	Total Organic Carbon	4.975		4.975	J	LD	PERCENT
L1736454	LLOYD_KAHN	L1736454-18	OR-T1-C5-A-17_SED_017-018CM	Total Organic Carbon	4.355		4.355	J	MS-H	PERCENT
L1736454	LLOYD_KAHN	L1736454-38	OR-T1-C5-A-17_SED_075-080CM	Total Organic Carbon	8.29		8.29	J	LD	PERCENT
L1736455	2540G	L1736455-01	OR-T2-C1-C-17_SED_000-001CM	Percent Solids, Residual	40.7		40.7	J	LD	PERCENT
L1736455	LLOYD_KAHN	L1736455-19	OR-T2-C1-C-17_SED_018-019CM	Total Organic Carbon	8.285		8.285	J	LD	PERCENT
L1736456	2540G	L1736456-01	OR-T2-C4-A-17_SED_000-001CM	Percent Solids, Residual	18.6		18.6	J	LD	PERCENT
L1736458	2540G	L1736458-21	OR-T3-C3-B-17_SED_020-022CM	Percent Solids, Residual	22		22	J	LD	PERCENT
L1737045	2540G	L1737045-01	MM-T3-C3-B2-17_SED_000-001CM	Percent Solids, Residual	46.5		46.5	J	LD	PERCENT
L1737045	LLOYD_KAHN	L1737045-01	MM-T3-C3-B2-17_SED_000-001CM	Total Organic Carbon	4.775		4.775	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-02	MM-T3-C3-B2-17_SED_001-002CM	Total Organic Carbon	3.8		3.8	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-03	MM-T3-C3-B2-17_SED_002-003CM	Total Organic Carbon	3.705		3.705	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-04	MM-T3-C3-B2-17_SED_003-004CM	Total Organic Carbon	2.92		2.92	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-05	MM-T3-C3-B2-17_SED_004-005CM	Total Organic Carbon	3.28		3.28	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-06	MM-T3-C3-B2-17_SED_005-006CM	Total Organic Carbon	3.045		3.045	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-07	MM-T3-C3-B2-17_SED_006-007CM	Total Organic Carbon	3.185		3.185	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-08	MM-T3-C3-B2-17_SED_007-008CM	Total Organic Carbon	3.48		3.48	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-09	MM-T3-C3-B2-17_SED_008-009CM	Total Organic Carbon	2.76		2.76	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-10	MM-T3-C3-B2-17_SED_009-010CM	Total Organic Carbon	3.08		3.08	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-11	MM-T3-C3-B2-17_SED_010-011CM	Total Organic Carbon	3.52		3.52	J	LD,HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-12	MM-T3-C3-B2-17_SED_011-012CM	Total Organic Carbon	3.39		3.39	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-13	MM-T3-C3-B2-17_SED_012-013CM	Total Organic Carbon	4.095		4.095	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-14	MM-T3-C3-B2-17_SED_013-014CM	Total Organic Carbon	4.84		4.84	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-15	MM-T3-C3-B2-17_SED_014-015CM	Total Organic Carbon	5.905		5.905	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-16	MM-T3-C3-B2-17_SED_015-016CM	Total Organic Carbon	4.41		4.41	J	MS-H,HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-17	MM-T3-C3-B2-17_SED_016-017CM	Total Organic Carbon	3.135		3.135	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-18	MM-T3-C3-B2-17_SED_017-018CM	Total Organic Carbon	3.27		3.27	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-19	MM-T3-C3-B2-17_SED_018-019CM	Total Organic Carbon	3.32		3.32	J	LD,HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-20	MM-T3-C3-B2-17_SED_019-020CM	Total Organic Carbon	3.18		3.18	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-21	MM-T3-C3-B2-17_SED_020-022CM	Total Organic Carbon	4.21		4.21	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-22	MM-T3-C3-B2-17_SED_022-024CM	Total Organic Carbon	2.025		2.025	J	HT	PERCENT

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
L1737045	LLOYD_KAHN	L1737045-23	MM-T3-C3-B2-17_SED_024-026CM	Total Organic Carbon	0.594		0.594	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-24	MM-T3-C3-B2-17_SED_026-028CM	Total Organic Carbon	0.409		0.409	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-25	MM-T3-C3-B2-17_SED_028-030CM	Total Organic Carbon	0.4735		0.4735	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-26	MM-T3-C3-B2-17_SED_030-032CM	Total Organic Carbon	0.688		0.688	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-27	MM-T3-C3-B2-17_SED_032-034CM	Total Organic Carbon	1.365		1.365	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-28	MM-T3-C3-B2-17_SED_034-036CM	Total Organic Carbon	0.7425		0.7425	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-29	MM-T3-C3-B2-17_SED_036-038CM	Total Organic Carbon	0.4015		0.4015	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-30	MM-T3-C3-B2-17_SED_038-040CM	Total Organic Carbon	0.376		0.376	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-31	MM-T3-C3-B2-17_SED_040-045CM	Total Organic Carbon	0.3565		0.3565	J	LD,HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-32	MM-T3-C3-B2-17_SED_045-050CM	Total Organic Carbon	0.362		0.362	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-33	MM-T3-C3-B2-17_SED_050-055CM	Total Organic Carbon	0.7885		0.7885	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-34	MM-T3-C3-B2-17_SED_055-060CM	Total Organic Carbon	0.754		0.754	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-35	MM-T3-C3-B2-17_SED_060-065CM	Total Organic Carbon	0.7745		0.7745	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-36	MM-T3-C3-B2-17_SED_065-070CM	Total Organic Carbon	0.3145		0.3145	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-37	MM-T3-C3-B2-17_SED_070-075CM	Total Organic Carbon	0.1645		0.1645	J	HT	PERCENT
L1737045	LLOYD_KAHN	L1737045-38	MM-T3-C3-B2-17_SED_075-080CM	Total Organic Carbon	0.1025		0.1025	J	LD,HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-01	OR-T1-C3-A-17_SED_000-001CM	Total Organic Carbon	4.42		4.42	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-02	OR-T1-C3-A-17_SED_001-002CM	Total Organic Carbon	4.705		4.705	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-03	OR-T1-C3-A-17_SED_002-003CM	Total Organic Carbon	4.825		4.825	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-04	OR-T1-C3-A-17_SED_003-004CM	Total Organic Carbon	5.38		5.38	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-05	OR-T1-C3-A-17_SED_004-005CM	Total Organic Carbon	5.34		5.34	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-06	OR-T1-C3-A-17_SED_005-006CM	Total Organic Carbon	5.37		5.37	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-07	OR-T1-C3-A-17_SED_006-007CM	Total Organic Carbon	6.005		6.005	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-08	OR-T1-C3-A-17_SED_007-008CM	Total Organic Carbon	5.615		5.615	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-09	OR-T1-C3-A-17_SED_008-009CM	Total Organic Carbon	5.935		5.935	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-10	OR-T1-C3-A-17_SED_009-010CM	Total Organic Carbon	5.74		5.74	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-11	OR-T1-C3-A-17_SED_010-011CM	Total Organic Carbon	5.845		5.845	J	MS-H,HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-12	OR-T1-C3-A-17_SED_011-012CM	Total Organic Carbon	5.085		5.085	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-13	OR-T1-C3-A-17_SED_012-013CM	Total Organic Carbon	6.665		6.665	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-14	OR-T1-C3-A-17_SED_013-014CM	Total Organic Carbon	5.735		5.735	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-15	OR-T1-C3-A-17_SED_014-015CM	Total Organic Carbon	5.625		5.625	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-16	OR-T1-C3-A-17_SED_015-016CM	Total Organic Carbon	6.3		6.3	J	HT	PERCENT

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
L1737046	LLOYD_KAHN	L1737046-17	OR-T1-C3-A-17_SED_016-017CM	Total Organic Carbon	6.04		6.04	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-18	OR-T1-C3-A-17_SED_017-018CM	Total Organic Carbon	6.245		6.245	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-19	OR-T1-C3-A-17_SED_018-019CM	Total Organic Carbon	7.75		7.75	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-20	OR-T1-C3-A-17_SED_019-020CM	Total Organic Carbon	8.015		8.015	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-21	OR-T1-C3-A-17_SED_020-022CM	Total Organic Carbon	6.35		6.35	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-22	OR-T1-C3-A-17_SED_022-024CM	Total Organic Carbon	5.845		5.845	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-23	OR-T1-C3-A-17_SED_024-026CM	Total Organic Carbon	7.88		7.88	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-24	OR-T1-C3-A-17_SED_026-028CM	Total Organic Carbon	6.89		6.89	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-25	OR-T1-C3-A-17_SED_028-030CM	Total Organic Carbon	6.87		6.87	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-26	OR-T1-C3-A-17_SED_030-032CM	Total Organic Carbon	6.595		6.595	J	LD,HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-27	OR-T1-C3-A-17_SED_032-034CM	Total Organic Carbon	7.57		7.57	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-28	OR-T1-C3-A-17_SED_034-036CM	Total Organic Carbon	7.515		7.515	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-29	OR-T1-C3-A-17_SED_036-038CM	Total Organic Carbon	8.185		8.185	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-30	OR-T1-C3-A-17_SED_038-040CM	Total Organic Carbon	8.24		8.24	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-31	OR-T1-C3-A-17_SED_040-045CM	Total Organic Carbon	9.38		9.38	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-32	OR-T1-C3-A-17_SED_045-050CM	Total Organic Carbon	8.785		8.785	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-33	OR-T1-C3-A-17_SED_050-055CM	Total Organic Carbon	9.545		9.545	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-34	OR-T1-C3-A-17_SED_055-060CM	Total Organic Carbon	5.86		5.86	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-35	OR-T1-C3-A-17_SED_060-065CM	Total Organic Carbon	6.805		6.805	J	LD,HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-36	OR-T1-C3-A-17_SED_065-070CM	Total Organic Carbon	7.585		7.585	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-37	OR-T1-C3-A-17_SED_070-075CM	Total Organic Carbon	7.515		7.515	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-38	OR-T1-C3-A-17_SED_075-080CM	Total Organic Carbon	6.695		6.695	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-39	OR-T1-C3-A-17_SED_080-085CM	Total Organic Carbon	6.525		6.525	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-40	OR-T1-C3-A-17_SED_085-090CM	Total Organic Carbon	5.62		5.62	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-41	OR-T1-C3-A-17_SED_090-095CM	Total Organic Carbon	2.97		2.97	J	HT	PERCENT
L1737046	LLOYD_KAHN	L1737046-42	OR-T1-C3-A-17_SED_095-101CM	Total Organic Carbon	2.31		2.31	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-01	OR-T2-C3-B-17_SED_000-001CM	Total Organic Carbon	24.7		24.7	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-02	OR-T2-C3-B-17_SED_001-002CM	Total Organic Carbon	3.66		3.66	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-03	OR-T2-C3-B-17_SED_002-003CM	Total Organic Carbon	7.07		7.07	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-04	OR-T2-C3-B-17_SED_003-004CM	Total Organic Carbon	4.68		4.68	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-05	OR-T2-C3-B-17_SED_004-005CM	Total Organic Carbon	3.2		3.2	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-06	OR-T2-C3-B-17_SED_005-006CM	Total Organic Carbon	5.525		5.525	J	HT	PERCENT

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DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
L1737047	LLOYD_KAHN	L1737047-07	OR-T2-C3-B-17_SED_006-007CM	Total Organic Carbon	3.895		3.895	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-08	OR-T2-C3-B-17_SED_007-008CM	Total Organic Carbon	2.68		2.68	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-09	OR-T2-C3-B-17_SED_008-009CM	Total Organic Carbon	3.34		3.34	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-10	OR-T2-C3-B-17_SED_009-010CM	Total Organic Carbon	3.06		3.06	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-11	OR-T2-C3-B-17_SED_010-011CM	Total Organic Carbon	3.305		3.305	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-12	OR-T2-C3-B-17_SED_011-012CM	Total Organic Carbon	3.335		3.335	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-13	OR-T2-C3-B-17_SED_012-013CM	Total Organic Carbon	3.295		3.295	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-14	OR-T2-C3-B-17_SED_013-014CM	Total Organic Carbon	2.275		2.275	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-15	OR-T2-C3-B-17_SED_014-015CM	Total Organic Carbon	2.16		2.16	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-16	OR-T2-C3-B-17_SED_015-016CM	Total Organic Carbon	2.085		2.085	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-17	OR-T2-C3-B-17_SED_016-017CM	Total Organic Carbon	2.025		2.025	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-18	OR-T2-C3-B-17_SED_017-018CM	Total Organic Carbon	1.72		1.72	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-19	OR-T2-C3-B-17_SED_018-019CM	Total Organic Carbon	1.73		1.73	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-20	OR-T2-C3-B-17_SED_019-020CM	Total Organic Carbon	1.61		1.61	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-21	OR-T2-C3-B-17_SED_020-022CM	Total Organic Carbon	1.845		1.845	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-22	OR-T2-C3-B-17_SED_022-024CM	Total Organic Carbon	1.945		1.945	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-23	OR-T2-C3-B-17_SED_024-026CM	Total Organic Carbon	1.915		1.915	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-24	OR-T2-C3-B-17_SED_026-028CM	Total Organic Carbon	2.125		2.125	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-25	OR-T2-C3-B-17_SED_028-030CM	Total Organic Carbon	1.92		1.92	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-26	OR-T2-C3-B-17_SED_030-032CM	Total Organic Carbon	2.16		2.16	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-27	OR-T2-C3-B-17_SED_032-034CM	Total Organic Carbon	1.875		1.875	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-28	OR-T2-C3-B-17_SED_034-036CM	Total Organic Carbon	1.875		1.875	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-29	OR-T2-C3-B-17_SED_036-038CM	Total Organic Carbon	1.645		1.645	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-30	OR-T2-C3-B-17_SED_038-040CM	Total Organic Carbon	1.85		1.85	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-31	OR-T2-C3-B-17_SED_040-045CM	Total Organic Carbon	1.74		1.74	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-32	OR-T2-C3-B-17_SED_045-050CM	Total Organic Carbon	1.9		1.9	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-33	OR-T2-C3-B-17_SED_050-055CM	Total Organic Carbon	1.97		1.97	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-34	OR-T2-C3-B-17_SED_055-060CM	Total Organic Carbon	1.635		1.635	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-35	OR-T2-C3-B-17_SED_060-065CM	Total Organic Carbon	2.285		2.285	J	HT	PERCENT
L1737047	LLOYD_KAHN	L1737047-36	OR-T2-C3-B-17_SED_065-070CM	Total Organic Carbon	2.31		2.31	J	HT	PERCENT
L1738093	2540G	L1738093-01	MM-T3-C6-17_SED_000-001CM	Percent Solids, Residual	30		30	J	LD	PERCENT
L1738093	LLOYD_KAHN	L1738093-01	MM-T3-C6-17_SED_000-001CM	Total Organic Carbon	15.85		15.85	J	HT	PERCENT

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
L1738093	LLOYD_KAHN	L1738093-02	MM-T3-C6-17_SED_001-002CM	Total Organic Carbon	16.15		16.15	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-03	MM-T3-C6-17_SED_002-003CM	Total Organic Carbon	18.25		18.25	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-04	MM-T3-C6-17_SED_003-004CM	Total Organic Carbon	20		20	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-05	MM-T3-C6-17_SED_004-005CM	Total Organic Carbon	21.25		21.25	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-06	MM-T3-C6-17_SED_005-006CM	Total Organic Carbon	20.25		20.25	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-07	MM-T3-C6-17_SED_006-007CM	Total Organic Carbon	19.15		19.15	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-08	MM-T3-C6-17_SED_007-008CM	Total Organic Carbon	12.45		12.45	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-09	MM-T3-C6-17_SED_008-009CM	Total Organic Carbon	10.8		10.8	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-10	MM-T3-C6-17_SED_010-011CM	Total Organic Carbon	14.95		14.95	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-11	MM-T3-C6-17_SED_011-012CM	Total Organic Carbon	19.65		19.65	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-12	MM-T3-C6-17_SED_012-013CM	Total Organic Carbon	20.4		20.4	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-13	MM-T3-C6-17_SED_013-014CM	Total Organic Carbon	18.75		18.75	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-14	MM-T3-C6-17_SED_014-015CM	Total Organic Carbon	14.85		14.85	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-15	MM-T3-C6-17_SED_015-016CM	Total Organic Carbon	12.75		12.75	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-16	MM-T3-C6-17_SED_016-017CM	Total Organic Carbon	10.59		10.59	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-17	MM-T3-C6-17_SED_017-018CM	Total Organic Carbon	11.3		11.3	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-18	MM-T3-C6-17_SED_018-019CM	Total Organic Carbon	12.7		12.7	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-19	MM-T3-C6-17_SED_019-020CM	Total Organic Carbon	12		12	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-20	MM-T3-C6-17_SED_020-022CM	Total Organic Carbon	12.15		12.15	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-21	MM-T3-C6-17_SED_022-024CM	Total Organic Carbon	11.1		11.1	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-22	MM-T3-C6-17_SED_024-026CM	Total Organic Carbon	8.23		8.23	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-23	MM-T3-C6-17_SED_026-028CM	Total Organic Carbon	7.77		7.77	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-24	MM-T3-C6-17_SED_028-030CM	Total Organic Carbon	6.72		6.72	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-25	MM-T3-C6-17_SED_030-032CM	Total Organic Carbon	6.655		6.655	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-26	MM-T3-C6-17_SED_032-034CM	Total Organic Carbon	7.275		7.275	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-27	MM-T3-C6-17_SED_034-036CM	Total Organic Carbon	7.195		7.195	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-28	MM-T3-C6-17_SED_036-038CM	Total Organic Carbon	6.285		6.285	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-29	MM-T3-C6-17_SED_038-040CM	Total Organic Carbon	5.965		5.965	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-30	MM-T3-C6-17_SED_040-045CM	Total Organic Carbon	5.66		5.66	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-31	MM-T3-C6-17_SED_045-050CM	Total Organic Carbon	5.88		5.88	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-32	MM-T3-C6-17_SED_050-055CM	Total Organic Carbon	5.92		5.92	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-33	MM-T3-C6-17_SED_055-060CM	Total Organic Carbon	12.2		12.2	J	HT	PERCENT

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
L1738093	LLOYD_KAHN	L1738093-34	MM-T3-C6-17_SED_060-065CM	Total Organic Carbon	11.45		11.45	J	HT	PERCENT
L1738093	LLOYD_KAHN	L1738093-35	MM-T3-C6-17_SED_065-070CM	Total Organic Carbon	14.2		14.2	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-01	MM-T4-C1-17_SED_000-001CM	Total Organic Carbon	8.14		8.14	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-02	MM-T4-C1-17_SED_001-002CM	Total Organic Carbon	9.485		9.485	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-03	MM-T4-C1-17_SED_002-003CM	Total Organic Carbon	9.675		9.675	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-04	MM-T4-C1-17_SED_003-004CM	Total Organic Carbon	7.98		7.98	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-05	MM-T4-C1-17_SED_004-005CM	Total Organic Carbon	8.35		8.35	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-06	MM-T4-C1-17_SED_005-006CM	Total Organic Carbon	9.14		9.14	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-07	MM-T4-C1-17_SED_006-007CM	Total Organic Carbon	11.75		11.75	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-08	MM-T4-C1-17_SED_007-008CM	Total Organic Carbon	10.9		10.9	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-09	MM-T4-C1-17_SED_008-009CM	Total Organic Carbon	9.675		9.675	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-10	MM-T4-C1-17_SED_009-010CM	Total Organic Carbon	9.885		9.885	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-11	MM-T4-C1-17_SED_010-011CM	Total Organic Carbon	10.02		10.02	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-12	MM-T4-C1-17_SED_011-012CM	Total Organic Carbon	12.4		12.4	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-13	MM-T4-C1-17_SED_012-013CM	Total Organic Carbon	12.15		12.15	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-14	MM-T4-C1-17_SED_013-014CM	Total Organic Carbon	12		12	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-15	MM-T4-C1-17_SED_014-015CM	Total Organic Carbon	10.35		10.35	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-16	MM-T4-C1-17_SED_015-016CM	Total Organic Carbon	10.59		10.59	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-17	MM-T4-C1-17_SED_016-017CM	Total Organic Carbon	11.05		11.05	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-18	MM-T4-C1-17_SED_017-018CM	Total Organic Carbon	11.15		11.15	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-19	MM-T4-C1-17_SED_018-019CM	Total Organic Carbon	11.4		11.4	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-20	MM-T4-C1-17_SED_019-020CM	Total Organic Carbon	10.9		10.9	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-21	MM-T4-C1-17_SED_020-022CM	Total Organic Carbon	12.65		12.65	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-22	MM-T4-C1-17_SED_022-024CM	Total Organic Carbon	13.45		13.45	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-23	MM-T4-C1-17_SED_024-026CM	Total Organic Carbon	14.8		14.8	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-24	MM-T4-C1-17_SED_026-028CM	Total Organic Carbon	11.05		11.05	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-25	MM-T4-C1-17_SED_028-030CM	Total Organic Carbon	10.55		10.55	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-26	MM-T4-C1-17_SED_030-032CM	Total Organic Carbon	8.11		8.11	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-27	MM-T4-C1-17_SED_032-034CM	Total Organic Carbon	9.02		9.02	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-28	MM-T4-C1-17_SED_034-036CM	Total Organic Carbon	5.57		5.57	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-29	MM-T4-C1-17_SED_036-038CM	Total Organic Carbon	7.06		7.06	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-30	MM-T4-C1-17_SED_038-040CM	Total Organic Carbon	8.815		8.815	J	HT	PERCENT

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
L1738103	LLOYD_KAHN	L1738103-31	MM-T4-C1-17_SED_040-045CM	Total Organic Carbon	11.85		11.85	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-32	MM-T4-C1-17_SED_045-050CM	Total Organic Carbon	12.95		12.95	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-33	MM-T4-C1-17_SED_050-055CM	Total Organic Carbon	12.1		12.1	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-34	MM-T4-C1-17_SED_055-060CM	Total Organic Carbon	14.35		14.35	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-35	MM-T4-C1-17_SED_060-065CM	Total Organic Carbon	18.85		18.85	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-36	MM-T4-C1-17_SED_065-070CM	Total Organic Carbon	17.65		17.65	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-37	MM-T4-C1-17_SED_070-075CM	Total Organic Carbon	21.3		21.3	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-38	MM-T4-C1-17_SED_075-080CM	Total Organic Carbon	23.15		23.15	J	HT	PERCENT
L1738103	LLOYD_KAHN	L1738103-39	MM-T4-C1-17_SED_080-085CM	Total Organic Carbon	21.6		21.6	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-01	MM-T4-C5-17_SED_000-001CM	Total Organic Carbon	16.25		16.25	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-02	MM-T4-C5-17_SED_001-002CM	Total Organic Carbon	15.15		15.15	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-03	MM-T4-C5-17_SED_002-003CM	Total Organic Carbon	17.6		17.6	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-04	MM-T4-C5-17_SED_003-004CM	Total Organic Carbon	18.65		18.65	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-05	MM-T4-C5-17_SED_004-005CM	Total Organic Carbon	15.6		15.6	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-06	MM-T4-C5-17_SED_005-006CM	Total Organic Carbon	17.75		17.75	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-07	MM-T4-C5-17_SED_006-007CM	Total Organic Carbon	16.6		16.6	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-08	MM-T4-C5-17_SED_007-008CM	Total Organic Carbon	15.85		15.85	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-09	MM-T4-C5-17_SED_008-009CM	Total Organic Carbon	10.6		10.6	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-10	MM-T4-C5-17_SED_009-010CM	Total Organic Carbon	10.215		10.215	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-11	MM-T4-C5-17_SED_010-011CM	Total Organic Carbon	13.9		13.9	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-12	MM-T4-C5-17_SED_011-012CM	Total Organic Carbon	13.35		13.35	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-13	MM-T4-C5-17_SED_012-013CM	Total Organic Carbon	13.05		13.05	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-14	MM-T4-C5-17_SED_013-014CM	Total Organic Carbon	14.1		14.1	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-15	MM-T4-C5-17_SED_014-015CM	Total Organic Carbon	13.9		13.9	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-16	MM-T4-C5-17_SED_015-016CM	Total Organic Carbon	14.2		14.2	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-17	MM-T4-C5-17_SED_016-017CM	Total Organic Carbon	13.2		13.2	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-18	MM-T4-C5-17_SED_017-018CM	Total Organic Carbon	11.65		11.65	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-19	MM-T4-C5-17_SED_018-019CM	Total Organic Carbon	9.975		9.975	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-20	MM-T4-C5-17_SED_019-020CM	Total Organic Carbon	9.355		9.355	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-21	MM-T4-C5-17_SED_020-022CM	Total Organic Carbon	7.635		7.635	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-22	MM-T4-C5-17_SED_022-024CM	Total Organic Carbon	11.65		11.65	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-23	MM-T4-C5-17_SED_024-026CM	Total Organic Carbon	8.725		8.725	J	HT	PERCENT

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SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
L1738104	LLOYD_KAHN	L1738104-24	MM-T4-C5-17_SED_026-028CM	Total Organic Carbon	8.11		8.11	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-25	MM-T4-C5-17_SED_028-030CM	Total Organic Carbon	7.14		7.14	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-26	MM-T4-C5-17_SED_030-032CM	Total Organic Carbon	8.505		8.505	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-27	MM-T4-C5-17_SED_032-034CM	Total Organic Carbon	8.415		8.415	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-28	MM-T4-C5-17_SED_034-036CM	Total Organic Carbon	9.73		9.73	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-29	MM-T4-C5-17_SED_036-038CM	Total Organic Carbon	10.7		10.7	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-30	MM-T4-C5-17_SED_038-040CM	Total Organic Carbon	8.92		8.92	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-31	MM-T4-C5-17_SED_040-045CM	Total Organic Carbon	7.44		7.44	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-32	MM-T4-C5-17_SED_045-050CM	Total Organic Carbon	8.155		8.155	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-33	MM-T4-C5-17_SED_050-055CM	Total Organic Carbon	5.32		5.32	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-34	MM-T4-C5-17_SED_055-060CM	Total Organic Carbon	4.795		4.795	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-35	MM-T4-C5-17_SED_060-065CM	Total Organic Carbon	4.96		4.96	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-36	MM-T4-C5-17_SED_065-070CM	Total Organic Carbon	5.805		5.805	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-37	MM-T4-C5-17_SED_070-075CM	Total Organic Carbon	2.33		2.33	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-38	MM-T4-C5-17_SED_075-080CM	Total Organic Carbon	3.93		3.93	J	HT	PERCENT
L1738104	LLOYD_KAHN	L1738104-39	MM-T4-C5-17_SED_080-085CM	Total Organic Carbon	4.035		4.035	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-01	MM-T4-C6-17_SED_000-001CM	Total Organic Carbon	7.36		7.36	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-02	MM-T4-C6-17_SED_001-002CM	Total Organic Carbon	7.7		7.7	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-03	MM-T4-C6-17_SED_002-003CM	Total Organic Carbon	7.505		7.505	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-04	MM-T4-C6-17_SED_003-004CM	Total Organic Carbon	7.34		7.34	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-05	MM-T4-C6-17_SED_004-005CM	Total Organic Carbon	7.405		7.405	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-06	MM-T4-C6-17_SED_005-006CM	Total Organic Carbon	6.895		6.895	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-07	MM-T4-C6-17_SED_006-007CM	Total Organic Carbon	6.295		6.295	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-08	MM-T4-C6-17_SED_007-008CM	Total Organic Carbon	6.72		6.72	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-09	MM-T4-C6-17_SED_008-009CM	Total Organic Carbon	6.745		6.745	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-10	MM-T4-C6-17_SED_009-010CM	Total Organic Carbon	6.545		6.545	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-11	MM-T4-C6-17_SED_010-011CM	Total Organic Carbon	6.6		6.6	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-12	MM-T4-C6-17_SED_011-012CM	Total Organic Carbon	6.62		6.62	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-13	MM-T4-C6-17_SED_012-013CM	Total Organic Carbon	6.82		6.82	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-14	MM-T4-C6-17_SED_013-014CM	Total Organic Carbon	7.22		7.22	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-15	MM-T4-C6-17_SED_014-015CM	Total Organic Carbon	7.99		7.99	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-16	MM-T4-C6-17_SED_015-016CM	Total Organic Carbon	9.015		9.015	J	HT	PERCENT

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
L1738105	LLOYD_KAHN	L1738105-17	MM-T4-C6-17_SED_016-017CM	Total Organic Carbon	8.99		8.99	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-18	MM-T4-C6-17_SED_017-018CM	Total Organic Carbon	9.085		9.085	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-19	MM-T4-C6-17_SED_018-019CM	Total Organic Carbon	9.59		9.59	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-20	MM-T4-C6-17_SED_019-020CM	Total Organic Carbon	9.49		9.49	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-21	MM-T4-C6-17_SED_020-022CM	Total Organic Carbon	9.09		9.09	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-22	MM-T4-C6-17_SED_022-024CM	Total Organic Carbon	10.85		10.85	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-23	MM-T4-C6-17_SED_024-026CM	Total Organic Carbon	10.4		10.4	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-24	MM-T4-C6-17_SED_026-028CM	Total Organic Carbon	10.95		10.95	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-25	MM-T4-C6-17_SED_028-030CM	Total Organic Carbon	12.2		12.2	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-26	MM-T4-C6-17_SED_030-032CM	Total Organic Carbon	12.45		12.45	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-27	MM-T4-C6-17_SED_032-034CM	Total Organic Carbon	11.9		11.9	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-28	MM-T4-C6-17_SED_034-036CM	Total Organic Carbon	11.3		11.3	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-29	MM-T4-C6-17_SED_036-038CM	Total Organic Carbon	9.77		9.77	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-30	MM-T4-C6-17_SED_038-040CM	Total Organic Carbon	7.815		7.815	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-31	MM-T4-C6-17_SED_040-045CM	Total Organic Carbon	6.615		6.615	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-32	MM-T4-C6-17_SED_045-050CM	Total Organic Carbon	6.1		6.1	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-33	MM-T4-C6-17_SED_050-055CM	Total Organic Carbon	6.13		6.13	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-34	MM-T4-C6-17_SED_055-060CM	Total Organic Carbon	6.225		6.225	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-35	MM-T4-C6-17_SED_060-065CM	Total Organic Carbon	5.65		5.65	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-36	MM-T4-C6-17_SED_065-070CM	Total Organic Carbon	5.075		5.075	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-37	MM-T4-C6-17_SED_070-075CM	Total Organic Carbon	4.895		4.895	J	HT	PERCENT
L1738105	LLOYD_KAHN	L1738105-38	MM-T4-C6-17_SED_075-080CM	Total Organic Carbon	4.585		4.585	J	HT	PERCENT
L1738128	2540G	L1738128-02	MM-T5-C2-17_SED_001-002CM	Percent Solids, Residual	40.2		40.2	J	LD	PERCENT
L1738128	LLOYD_KAHN	L1738128-30	MM-T5-C2-17_SED_038-040CM	Total Organic Carbon	4.405		4.405	J	MS-H	PERCENT
L1739122	LLOYD_KAHN	L1739122-01	MM-T4-C7-17_SED_000-001CM	Total Organic Carbon	6.295		6.295	J	MS-H	PERCENT
L1739122	LLOYD_KAHN	L1739122-23	MM-T4-C7-17_SED_024-026CM	Total Organic Carbon	0.2005		0.2005	J	LD	PERCENT
L1739122	LLOYD_KAHN	L1739122-26	MM-T4-C7-17_SED_030-032CM	Total Organic Carbon	0.208		0.208	J	LD	PERCENT
L1739127	LLOYD_KAHN	L1739127-21	OR-T3-C4-A-17_SED_020-022CM	Total Organic Carbon	5.13		5.13	J	MS-H	PERCENT
L1739537	LLOYD_KAHN	L1739537-03	ES-18-F-17_SED_03-05	Total Organic Carbon	3.495		3.495	J	LD	PERCENT
L1739540	LLOYD_KAHN	L1739540-04	MM-T1-C2-D-17_SED_05-07	Total Organic Carbon	6.91		6.91	J	MS-H	PERCENT
L1739573	LLOYD_KAHN	L1739573-02	MM-T4-C2-F-17_SED_01-03	Total Organic Carbon	6.97		6.97	J	MS-H	PERCENT
L1739656	LLOYD_KAHN	L1739656-03	VE-MU4-GC-1-F-17_SED_03-05	Total Organic Carbon	1.53		1.53	J	LD	PERCENT

TABLE 2
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Analysis Method	Lab Sample ID	Field Sample Id	Parameter Name	Lab Result	Lab Qualifier	Validated Result	Validated Qualifier	Validation Reason Code	Result Units
L1740284	LLOYD_KAHN	L1740284-16	MM-T2-C7-A-17_SED_015-016CM	Total Organic Carbon	6.045		6.045	J	MS-H	PERCENT
L1740285	LLOYD_KAHN	L1740285-01	MM-T3-C1-17_SED_000-001CM	Total Organic Carbon	4.97		4.97	J	MS-H	PERCENT
L1740285	LLOYD_KAHN	L1740285-08	MM-T3-C1-17_SED_007-008CM	Total Organic Carbon	0.073		0.073	J	LD	PERCENT
L1740285	LLOYD_KAHN	L1740285-18	MM-T3-C1-17_SED_017-018CM	Total Organic Carbon	0.102		0.102	J	LD	PERCENT
L1741133	LLOYD_KAHN	L1741133-04	MM-T1-C1-B-17_SED_05-07	Total Organic Carbon	7.845		7.845	J	LD	PERCENT

Units

NG/G = Nanogram per gram

Validation Qualifier:

J = Value is estimated

Validation Reason Codes:

FD = Field duplicate RPD limit exceeded

HT = Hold time exceeded

LCS-RPD = LCS/LCSD RPD limit exceeded

LD = Lab duplicate limit exceeded

MS-H = MS and/or MSD recovery high

MS-L = MS and/or MSD recovery low

MS-RPD = MS/MSD RPD limit exceeded

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDGs 1709432, 1709552, 1709555, 1709558, 1709562, 1709563, 1709564, 1709565, 1709566, 1709567, 1709568, 1709569, 1709570, 1709571, 1709572, 1709574, 1710289, 1710294, 1710307, 1710310, 1710313, 1710315, 1710633, 1710634, 1710637, 1710639, 1710641, 1710682, 1710684, 1710685, 1710728, 1710729, 1710730, 1710731, 1710732, 1710733, 1710907, 1710910, 1710913, 1710916, 1710917, 1710918, 1711046, 1711047, 1711050, 1711056, 1711057, 1711058, 1711059, 1711060, 1711061, 1711062, 1711063, 1711064, 1711065, 1711066, 1711067, 1711068, 1711069, 1711070, 1711071, 1711073, 1711077, 1711083, 1711084, 1711085, 1711151, 1711156, 1711171, 1711173, 1711174, 1711328, 1712044, 1712045, 1712047, L1732774, L1733612, L1733618, L1733619, L1733620, L1733621, L1736451, L1736453, L1736454, L1736455, L1736456, L1736458, L1737040, L1737041, L1737042, L1737043, L1737044, L1737045, L1737046, L1737047, L1738093, L1738103, L1738104, L1738105, L1738106, L1738128, L1739120, L1739121, L1739122, L1739123, L1739124, L1739127, L1739536, L1739537, L1739540, L1739541, L1739542, L1739572, L1739573, L1739577, L1739578, L1739579, L1739580, L1739581, L1739593, L1739594, L1739595, L1739596, L1739597, L1739598, L1739599, L1739601, L1739602, L1739653, L1739656, L1739691, L1740283, L1740284, L1740285, L1740287, L1740289 and L1741133

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1709432	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_000-001CM	FS	51.1	J	604			
1709432	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_001-002CM	FS	58.3	J	442			
1709432	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_002-003CM	FS	54.3	J	512			
1709432	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_003-004CM	FS	50	J	571			
1709432	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_004-005CM	FS	42.8	J	718			
1709432	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_005-006CM	FS	41.3	J	720			
1709432	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_006-007CM	FS	43	J	633			
1709432	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_007-008CM	FS	45.3	J	590			
1709432	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_008-009CM	FS	49	J	475			
1709432	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_009-010CM	FS	46.1	J	522			
1709432	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_010-011CM	FS	49.7	J	478			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_011-012CM	FS	42.5	J	811			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_012-013CM	FS	40.8	J	825			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_013-014CM	FS	50.8	J	467			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_014-015CM	FS	58.4	J	246			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_015-016CM	FS	59.3	J	292			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_016-017CM	FS	41.6	J	565			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_017-018CM	FS	57	J	167			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_018-019CM	FS	83	J	54.9			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_019-020CM	FS	81.9	J	5.23			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_020-022CM	FS	82.5	J	5.42			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_022-024CM	FS	82.2	J	4.69			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_024-026CM	FS	81.7	J	3.1	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_026-028CM	FS	82.4	J	2.45	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_028-030CM	FS	78.3	J	2.71	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_030-032CM	FS	79.8	J	2.52	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_032-034CM	FS	81.9	J	2.43	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_034-036CM	FS	81.8	J	2.86	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_036-038CM	FS	81.5	J	2.64	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_038-040CM	FS	82.6	J	2.46	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_040-045CM	FS	82.5	J	3.36	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_045-050CM	FS	81.9	J	2.83	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_050-055CM	FS	83.6	J	5.11			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_055-060CM	FS	82.3	J	4.62			
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_060-065CM	FS	81.8	J	3.51	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_065-070CM	FS	82.8	J	1.97	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_070-075CM	FS	82.3	J	2.71	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_075-080CM	FS	82.6	J	3.41	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_080-085CM	FS	81.5	J	4.35	J		
1709432	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_085-090CM	FS	83.2	J	2.25	J		

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
					Final	Final	Final	Final	Final	Final		
					Result	Qualifier	Result	Qualifier	Result	Qualifier		
1709552	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_040-045CM	FS	59.8	J	14.8					
1709552	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_045-050CM	FS	60.8	J	16.5					
1709552	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_050-055CM	FS	56.2	J	14.8					
1709552	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_055-060CM	FS	56.4	J	18.1					
1709552	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_060-065CM	FS	56.6	J	18.4					
1709552	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_065-070CM	FS	56.1	J	17.7					
1709552	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_070-075CM	FS	55.6	J	15.8					
1709552	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_075-080CM	FS	55.7	J	12.4					
1709552	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_080-085CM	FS	57	J	16					
1709552	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_085-090CM	FS	55.8	J	16.2					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_015-016CM	FS	62.4	J	16.4					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_016-017CM	FS	64.5	J	17.8					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_017-018CM	FS	62.5	J	16.3					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_018-019CM	FS	61.6	J	18.3					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_019-020CM	FS	61	J	20.4					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_020-022CM	FS	59.4	J	20.1					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_022-024CM	FS	59.8	J	20.6					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_024-026CM	FS	62.4	J	17.4					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_026-028CM	FS	60.5	J	16.5					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_028-030CM	FS	54.7	J	28.2					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_030-032CM	FS	53.2	J	19.5					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_032-034CM	FS	55.6	J	19.6					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_034-036CM	FS	56.1	J	18.9					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_036-038CM	FS	57.8	J	16.8					
1709555	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_038-040CM	FS	59.4	J	16.2					

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
					Final	Final	Final	Final	Final	Final		
					Result	Qualifier	Result	Qualifier	Result	Qualifier		
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_000-001CM	FS	50.8	J	86.4					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_001-002CM	FS	50.2	J	68.8					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_002-003CM	FS	49.6	J	53					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_003-004CM	FS	49.4	J	47.7					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_004-005CM	FS	50.4	J	37.4					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_005-006CM	FS	54.5	J	39.4					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_006-007CM	FS	56.3	J	35.2					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_007-008CM	FS	56.3	J	32.7					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_008-009CM	FS	59.5	J	30.3					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_009-010CM	FS	59.5	J	27.9					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_010-011CM	FS	58	J	24					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_011-012CM	FS	59.2	J	23.7					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_012-013CM	FS	58.6	J	21.9					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_013-014CM	FS	58.5	J	25.3					
1709558	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_014-015CM	FS	63.2	J	20.2					
1709562	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_040-045CM	FS	45	J	565					
1709562	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_045-050CM	FS	48.8	J	589					
1709562	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_050-055CM	FS	54.8	J	662					
1709562	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_055-060CM	FS	45	J	2,250					
1709562	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_060-065CM	FS	42.2	J	2,820					
1709562	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_065-070CM	FS	43.6	J	3,280					
1709562	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_070-075CM	FS	49	J	1,870					
1709562	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_075-080CM	FS	46.1	J	1,990					
1709562	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_080-085CM	FS	54.2	J	504					
1709562	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_085-090CM	FS	63	J	78					

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_015-016CM	FS	40.1	J	826			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_016-017CM	FS	39.6	J	764			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_017-018CM	FS	41.6	J	720			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_018-019CM	FS	42.6	J	714			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_019-020CM	FS	39.7	J	823			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_020-022CM	FS	43.1	J	708			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_022-024CM	FS	47.9	J	697			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_024-026CM	FS	42.9	J	743			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_026-028CM	FS	46.2	J	642			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_028-030CM	FS	45.6	J	709			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_030-032CM	FS	43.2	J	1,010			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_032-034CM	FS	41.8	J	785			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_034-036CM	FS	44.2	J	903			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_036-038CM	FS	43.2	J	803			
1709563	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_038-040CM	FS	38.2	J	739			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_000-001CM	FS	37.2	J	960			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_001-002CM	FS	43.8	J	642			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_002-003CM	FS	39.8	J	593			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_003-004CM	FS	38	J	718			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_004-005CM	FS	40.5	J	642			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_005-006CM	FS	37.8	J	691			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_006-007CM	FS	39.8	J	736			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_007-008CM	FS	42.1	J	720			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_008-009CM	FS	38.5	J	882			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_009-010CM	FS	41.3	J	698			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_010-011CM	FS	40.3	J	843			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_011-012CM	FS	40.6	J	748			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_012-013CM	FS	42.6	J	736			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_013-014CM	FS	42.6	J	733			
1709564	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_014-015CM	FS	44.1	J	651			
1709565	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_040-045CM	FS	63.6	J	28.5			
1709565	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_045-050CM	FS	63.1	J	25.5			
1709565	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_050-055CM	FS	67.5	J	17			
1709565	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_055-060CM	FS	66	J	19			
1709565	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_060-065CM	FS	64.8	J	16.7			
1709565	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_065-070CM	FS	67.1	J	18			
1709565	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_070-075CM	FS	63	J	23.1			
1709565	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_075-080CM	FS	58.4	J	25.6			
1709565	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_080-085CM	FS	55.8	J	22.7			
1709565	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_085-090CM	FS	59	J	21.8			
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_015-016CM	FS	63.8	J	171			
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_016-017CM	FS	60.3	J	181			
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_017-018CM	FS	62.9	J	266			
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_018-019CM	FS	64.1	J	224			
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_019-020CM	FS	67.4	J	276			
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_020-022CM	FS	67.8	J	109			
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_022-024CM	FS	65.9	J	151			
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_024-026CM	FS	62.8	J	123			
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_026-028CM	FS	64.9	J	83.2			
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_028-030CM	FS	63.6	J	96.3			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
Final	Final	Final	Final	Final	Final	Final	Final	Final	Final			
Result	Qualifier	Result	Qualifier	Result	Qualifier	Result	Qualifier	Result	Qualifier			
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_030-032CM	FS	67.1	J	60.3					
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_032-034CM	FS	63	J	47.9					
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_034-036CM	FS	65.8	J	45.5					
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_036-038CM	FS	64.7	J	39.7					
1709566	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_038-040CM	FS	64.6	J	28.3					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_000-001CM	FS	36.1	J	544					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_001-002CM	FS	33.4	J	446					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_002-003CM	FS	35.8	J	525					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_003-004CM	FS	39.6	J	342					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_004-005CM	FS	44	J	287					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_005-006CM	FS	45.2	J	282					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_006-007CM	FS	46.1	J	301					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_007-008CM	FS	51.4	J	253					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_008-009CM	FS	41.3	J	408					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_009-010CM	FS	53.6	J	257					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_010-011CM	FS	59.3	J	236					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_011-012CM	FS	53.1	J	183					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_012-013CM	FS	55.5	J	195					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_013-014CM	FS	56	J	193					
1709567	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_014-015CM	FS	56.5	J	176					
1709568	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_040-045CM	FS	84.5	J	4.03	J				
1709568	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_045-050CM	FS	81.5	J	5.11					
1709568	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_050-055CM	FS	83.7	J	4.25	J				
1709568	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_055-060CM	FS	82.5	J	5.41					
1709568	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_060-065CM	FS	80.6	J	5.56					

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total	Final	Final	Total	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1709568	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_065-070CM	FS	81.9	J	4.73			
1709568	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_070-075CM	FS	80.1	J	4.32	J		
1709568	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_075-080CM	FS	81.5	J	4.47	J		
1709568	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_080-085CM	FS	81.1	J	4.68	J		
1709568	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_085-090CM	FS	80.9	J	5.12			
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_015-016CM	FS	74.4	J	13.7			
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_016-017CM	FS	76.4	J	12.4			
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_017-018CM	FS	75.6	J	12.1			
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_018-019CM	FS	73.1	J	10.8			
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_019-020CM	FS	74.1	J	11.1			
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_020-022CM	FS	71.4	J	8.41			
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_022-024CM	FS	84.7	J	5.09			
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_024-026CM	FS	85.6	J	4.89			
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_026-028CM	FS	87.1	J	3.36	J		
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_028-030CM	FS	85.4	J	4	J		
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_030-032CM	FS	85.1	J	3.84	J		
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_032-034CM	FS	82.5	J	3.27	J		
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_034-036CM	FS	83.5	J	4.11	J		
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_036-038CM	FS	82.8	J	7.03			
1709569	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_038-040CM	FS	84.2	J	4.18	J		
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_000-001CM	FS	40	J	116			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_001-002CM	FS	47.2	J	88.5			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_002-003CM	FS	43.8	J	77.8			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_003-004CM	FS	45	J	69			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_004-005CM	FS	48.6	J	64.6			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_005-006CM	FS	50.1	J	64.9			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_006-007CM	FS	54.9	J	53.9			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_007-008CM	FS	56.7	J	48.4			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_008-009CM	FS	56.9	J	45.4			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_009-010CM	FS	60	J	34.2			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_010-011CM	FS	60.6	J	34.4			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_011-012CM	FS	63.8	J	28.3			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_012-013CM	FS	64.7	J	23.4			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_013-014CM	FS	66.9	J	19.9			
1709570	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_014-015CM	FS	68.8	J	17.3			
1709571	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_040-045CM	FS	92.3	J	24.4			
1709571	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_045-050CM	FS	93.2	J	24.1			
1709571	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_050-055CM	FS	92	J	23.1			
1709571	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_055-060CM	FS	91.5	J	16.7			
1709571	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_060-065CM	FS	91.9	J	8.29			
1709571	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_065-070CM	FS	90.7	J	7.03			
1709571	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_070-075CM	FS	92.8	J	4.79			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_015-016CM	FS	89.1	J	10.4			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_016-017CM	FS	93.4	J	9.77			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_017-018CM	FS	86.9	J	16.1			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_018-019CM	FS	90.4	J	11.2			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_019-020CM	FS	91.8	J	12.2			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_020-022CM	FS	93.6	J	12.7			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_022-024CM	FS	88	J	20.1			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_024-026CM	FS	90.5	J	12.6			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_026-028CM	FS	89.8	J	11.6			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_028-030CM	FS	88.4	J	16.7			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_030-032CM	FS	94.4	J	12.8			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_032-034CM	FS	92.1	J	13.2			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_034-036CM	FS	93.3	J	22			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_036-038CM	FS	93.6	J	17.2			
1709572	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_038-040CM	FS	91	J	24.3			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_000-001CM	FS	40.4	J	565			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_001-002CM	FS	42.3	J	488			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_002-003CM	FS	42.7	J	439			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_003-004CM	FS	45.6	J	391			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_004-005CM	FS	63.7	J	182			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_005-006CM	FS	53.5	J	174			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_006-007CM	FS	53.6	J	110			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_007-008CM	FS	58.7	J	67.5			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_008-009CM	FS	73.1	J	45.6			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_009-010CM	FS	72.5	J	26.8			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_010-011CM	FS	82.8	J	25.5			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_011-012CM	FS	78.8	J	18.6			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_012-013CM	FS	86.1	J	13.1			
1709574	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_013-014CM	FS	90.1	J	12.1			
1709574	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_014-015CM	FS	88.5	J	7.47			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_000-001CM	FS	34.7	J	779			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_001-002CM	FS	30.5	J	790			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_002-003CM	FS	29.6	J	819			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_003-004CM	FS	35.5	J	782			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_004-005CM	FS	34.6	J	833			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_005-006CM	FS	37.1	J	751			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_006-007CM	FS	36.5	J	768			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_007-008CM	FS	37.4	J	821			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_008-009CM	FS	37.7	J	726			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_009-010CM	FS	36.3	J	812			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_010-011CM	FS	34.4	J	870			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_011-012CM	FS	36	J	780			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_012-013CM	FS	34.3	J	952			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_013-014CM	FS	37.6	J	861			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_014-015CM	FS	36.9	J	865			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_015-016CM	FS	38.1	J	773			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_016-017CM	FS	38.6	J	798			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_017-018CM	FS	37.3	J	900			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_018-019CM	FS	36.3	J	966			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_019-020CM	FS	36.7	J	988			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_020-022CM	FS	39.2	J	919			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_022-024CM	FS	39.8	J	1,040			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_024-026CM	FS	42.8	J	635			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_026-028CM	FS	45.9	J	274			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_028-030CM	FS	45.6	J	192			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_030-032CM	FS	45.8	J	138			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_032-034CM	FS	47	J	105			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_034-036CM	FS	47.3	J	87.6			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_036-038CM	FS	58	J	38.2			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_038-040CM	FS	56.7	J	41.1			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_040-045CM	FS	60.9	J	29.3			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_045-050CM	FS	61.3	J	25.6			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_050-055CM	FS	59.7	J	26.2			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_055-060CM	FS	62.7	J	21.8			
1710289	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_060-065CM	FS	61.7	J	45.1			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_000-001CM	FS	40.1	J	637			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_001-002CM	FS	40.9	J	749			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_002-003CM	FS	39.7	J	736			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_003-004CM	FS	40.2	J	774			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_004-005CM	FS	46.6	J	783			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_005-006CM	FS	43.1	J	794			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_006-007CM	FS	41.8	J	711			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_007-008CM	FS	41.9	J	759			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_008-009CM	FS	42	J	723			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_009-010CM	FS	43.6	J	685			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_010-011CM	FS	42.6	J	753			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_011-012CM	FS	43	J	810			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_012-013CM	FS	42.3	J	793			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_013-014CM	FS	44.1	J	769			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_014-015CM	FS	44.6	J	800			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_015-016CM	FS	45.1	J	919			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_016-017CM	FS	44.3	J	876			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_017-018CM	FS	44.5	J	936			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_018-019CM	FS	44.6	J	926			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_019-020CM	FS	44.5	J	940			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_020-022CM	FS	43.8	J	1,080			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_022-024CM	FS	44.6	J	1,060			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_024-026CM	FS	44.9	J	1,280			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_026-028CM	FS	44.8	J	1,390			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_028-030CM	FS	45.6	J	1,490			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_030-032CM	FS	44.2	J	1,660			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_032-034CM	FS	44.4	J	1,830			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_034-036CM	FS	44	J	1,970			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_036-038CM	FS	43.2	J	2,090			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_038-040CM	FS	40.7	J	2,570			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_040-045CM	FS	39.7	J	3,530			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_045-050CM	FS	39.6	J	3,370			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_050-055CM	FS	39.4	J	3,130			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_055-060CM	FS	43.7	J	2,010			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_060-065CM	FS	41.5	J	1,620			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_065-070CM	FS	41.3	J	680			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_070-075CM	FS	39.3	J	464			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_075-080CM	FS	40.5	J	345			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_080-085CM	FS	62.4	J	71.1			
1710294	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_085-090CM	FS	63.4	J	126			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_000-001CM	FS	40	J	638			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_001-002CM	FS	42.5	J	764			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_002-003CM	FS	47.3	J	785			

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_003-004CM	FS	42.6	J	764			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_004-005CM	FS	44.1	J	704			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_005-006CM	FS	45.2	J	738			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_006-007CM	FS	42.6	J	828			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_007-008CM	FS	40.6	J	838			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_008-009CM	FS	41.8	J	809			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_009-010CM	FS	42.3	J	790			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_010-011CM	FS	43.6	J	764			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_011-012CM	FS	46.9	J	723			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_012-013CM	FS	48.7	J	701			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_013-014CM	FS	50.5	J	664			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_014-015CM	FS	50.8	J	677			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_015-016CM	FS	49.4	J	738			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_016-017CM	FS	48.9	J	793			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_017-018CM	FS	46.2	J	888			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_018-019CM	FS	45.5	J	1,040			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_019-020CM	FS	46.7	J	1,020			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_020-022CM	FS	46	J	1,020			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_022-024CM	FS	48.1	J	1,060			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_024-026CM	FS	49.1	J	855			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_026-028CM	FS	47.3	J	1,020			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_028-030CM	FS	45.9	J	1,120			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_030-032CM	FS	43.1	J	1,300			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_032-034CM	FS	49.6	J	1,210			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_034-036CM	FS	49.1	J	1,440			

TABLE 3
DATA VALIDATION SUMMARY
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_036-038CM	FS	48.6	J	1,670			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_038-040CM	FS	48.3	J	1,860			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_040-045CM	FS	47.4	J	2,060			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_045-050CM	FS	52.9	J	1,660			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_050-055CM	FS	50.9	J	1,240			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_055-060CM	FS	46.5	J	616			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_060-065CM	FS	42.4	J	252	J		
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_065-070CM	FS	44.7	J	2,250			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_070-075CM	FS	47.5	J	230			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_075-080CM	FS	43.4	J	249			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_080-085CM	FS	42.6	J	262			
1710307	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_085-090CM	FS	45.8	J	249			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_000-001CM	FS	40.6	J	721			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_001-002CM	FS	38.5	J	894			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_002-003CM	FS	37.6	J	812			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_003-004CM	FS	36	J	1,030			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_004-005CM	FS	40.5	J	822			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_005-006CM	FS	38.6	J	862			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_006-007CM	FS	41.7	J	854			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_007-008CM	FS	42.4	J	816			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_008-009CM	FS	43.9	J	917			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_009-010CM	FS	43.7	J	1,180			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_010-011CM	FS	42.8	J	1,340			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_011-012CM	FS	42	J	1,720			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_012-013CM	FS	41.8	J	1,950			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_013-014CM	FS	42.7	J	2,250			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_014-015CM	FS	39	J	2,310			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_015-016CM	FS	40.4	J	1,790			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_016-017CM	FS	43.6	J	1,670			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_017-018CM	FS	42.9	J	1,630			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_018-019CM	FS	42.6	J	1,360			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_019-020CM	FS	41.4	J	827			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_020-022CM	FS	43.1	J	400			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_022-024CM	FS	43.2	J	320			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_024-026CM	FS	41.2	J	300			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_026-028CM	FS	45.8	J	289			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_028-030CM	FS	46.2	J	311			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_030-032CM	FS	47.6	J	386			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_032-034CM	FS	48.6	J	285			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_034-036CM	FS	48.2	J	293			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_036-038CM	FS	49.1	J	270			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_038-040CM	FS	53.9	J	204			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_040-045CM	FS	57.2	J	146			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_045-050CM	FS	68.8	J	43.4			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_050-055CM	FS	70.8	J	21.7			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_055-060CM	FS	68.5	J	19.7			
1710310	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_060-065CM	FS	64.9	J	24.3			
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_000-001CM	FS	47.2	J	771			
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_001-002CM	FS	48	J	820			
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_002-003CM	FS	47.4	J	805			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier		
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_003-004CM	FS	49.1	J	731					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_004-005CM	FS	49.1	J	763					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_005-006CM	FS	46.7	J	834					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_006-007CM	FS	44.7	J	965					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_007-008CM	FS	42.4	J	1,060					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_008-009CM	FS	42.6	J	1,190					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_009-010CM	FS	40.9	J	1,260					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_010-011CM	FS	42.3	J	1,230					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_011-012CM	FS	44.9	J	1,150					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_012-013CM	FS	42	J	1,260					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_013-014CM	FS	43.8	J	1,240					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_014-015CM	FS	45.2	J	1,230					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_015-016CM	FS	45.5	J	1,140					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_016-017CM	FS	46.8	J	1,140					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_017-018CM	FS	46	J	1,180					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_018-019CM	FS	41.1	J	1,440					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_019-020CM	FS	42	J	1,370					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_020-022CM	FS	40.7	J	1,450					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_022-024CM	FS	40	J	1,710					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_024-026CM	FS	39	J	2,900					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_026-028CM	FS	35.3	J	3,400					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_028-030CM	FS	37.3	J	3,680					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_030-032CM	FS	39	J	2,830					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_032-034CM	FS	42.4	J	2,210					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_034-036CM	FS	40.7	J	2,180					

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier		
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_036-038CM	FS	40.2	J	2,460					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_038-040CM	FS	43.4	J	1,620					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_040-045CM	FS	42.8	J	1,230					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_045-050CM	FS	41.5	J	867					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_050-055CM	FS	33.1	J	489					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_055-060CM	FS	39.8	J	354					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_060-065CM	FS	37.8	J	291					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_065-070CM	FS	31.5	J	309					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_070-075CM	FS	34.2	J	298					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_075-080CM	FS	35.5	J	273					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_080-085CM	FS	37.4	J	274					
1710313	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_085-090CM	FS	43	J	241					
1710315	OR-T3-C3-B	9/29/2017	OR-T3-C3-B-17_SED_000-001CM	FS	28.3	J	1,110					
1710315	OR-T3-C3-B	9/29/2017	OR-T3-C3-B-17_SED_001-002CM	FS	26.7	J	994					
1710315	OR-T3-C3-B	9/29/2017	OR-T3-C3-B-17_SED_002-003CM	FS	23.5	J	1,340					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_003-004CM	FS	23.3	J	1,270					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_004-005CM	FS	26.7	J	1,290					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_005-006CM	FS	32	J	1,040					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_006-007CM	FS	29.7	J	1,160					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_007-008CM	FS	27.3	J	1,310					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_008-009CM	FS	27.2	J	1,250					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_009-010CM	FS	26.3	J	1,240					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_010-011CM	FS	22.3	J	1,440					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_011-012CM	FS	19.3	J	1,610					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_012-013CM	FS	20.3	J	1,540					

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
					Final	Final	Final	Final	Final	Final		
					Result	Qualifier	Result	Qualifier	Result	Qualifier		
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_013-014CM	FS	19.1	J	1,880					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_014-015CM	FS	17.1	J	1,800					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_015-016CM	FS	16.1	J	1,540					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_016-017CM	FS	18.1	J	1,730					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_017-018CM	FS	19.7	J	1,510					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_018-019CM	FS	18.7	J	1,410					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_019-020CM	FS	18.2	J	1,540					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_020-022CM	FS	24.1	J	1,390					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_022-024CM	FS	30.5	J	1,270					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_024-026CM	FS	28.1	J	1,470					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_026-028CM	FS	36	J	1,240					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_028-030CM	FS	34.4	J	1,470					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_030-032CM	FS	36	J	1,280					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_032-034CM	FS	40.4	J	1,150					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_034-036CM	FS	32.4	J	1,560					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_036-038CM	FS	30.7	J	1,800					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_038-040CM	FS	31.3	J	1,790					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_040-045CM	FS	35.4	J	1,410					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_045-050CM	FS	47	J	1,100					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_050-055CM	FS	34.7	J	1,930					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_055-060CM	FS	39.8	J	1,720					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_060-065CM	FS	37.2	J	1,970					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_065-070CM	FS	30.2	J	2,160					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_070-075CM	FS	33	J	2,250					
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_075-080CM	FS	29.1	J	2,330					

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_080-085CM	FS	34	J	2,180			
1710315	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_085-090CM	FS	37.3	J	2,030			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_000-001CM	FS	17.9	J	136			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_001-002CM	FS	14.4	J	117			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_002-003CM	FS	16.5	J	133			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_003-004CM	FS	16	J	160			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_004-005CM	FS	18.2	J	365			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_005-006CM	FS	17.5	J	464			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_006-007CM	FS	17	J	449			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_007-008CM	FS	14	J	231			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_008-009CM	FS	16.1	J	132			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_009-010CM	FS	16.6	J	78.3			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_010-011CM	FS	16.2	J	74.7			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_011-012CM	FS	19.9	J	46.1			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_012-013CM	FS	19.2	J	33.6			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_013-014CM	FS	17.3	J	37			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_014-015CM	FS	15.8	J	30.8			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_015-016CM	FS	16.3	J	40.8			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_016-017CM	FS	16.8	J	22.3	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_017-018CM	FS	15.8	J	20.8	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_018-019CM	FS	15.6	J	27.9			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_019-020CM	FS	15	J	19.6	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_020-022CM	FS	16.5	J	20.2	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_022-024CM	FS	17.6	J	16	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_024-026CM	FS	17	J	15	J		

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_026-028CM	FS	18.9	J	14.1	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_028-030CM	FS	17.7	J	19.6	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_030-032CM	FS	18.9	J	19.8			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_032-034CM	FS	23.3	J	16	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_034-036CM	FS	21.8	J	17.6			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_036-038CM	FS	20.5	J	16.3	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_038-040CM	FS	22.7	J	15.7	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_040-045CM	FS	23.8	J	10.4	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_045-050CM	FS	19.7	J	23			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_050-055CM	FS	20.9	J	12.9	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_055-060CM	FS	19.3	J	12.8	J		
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_060-065CM	FS	23.3	J	20.5			
1710633	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_065-070CM	FS	23	J	18.8			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_000-001CM	FS	41	J	804			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_001-002CM	FS	41.4	J	873			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_002-003CM	FS	38.6	J	846			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_003-004CM	FS	39.8	J	804			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_004-005CM	FS	37.2	J	792			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_005-006CM	FS	39.7	J	848			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_006-007CM	FS	38.9	J	816			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_007-008CM	FS	39.7	J	794			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_008-009CM	FS	42	J	659			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_009-010CM	FS	31.9	J	781			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_010-011CM	FS	28	J	797			
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_011-012CM	FS	40.3	J	667			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
					Final	Final	Final	Final	Final	Final		
					Result	Qualifier	Result	Qualifier	Result	Qualifier		
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_012-013CM	FS	43.3	J	705					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_013-014CM	FS	42.7	J	688					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_014-015CM	FS	42.1	J	745					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_015-016CM	FS	40	J	709					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_016-017CM	FS	32.6	J	828					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_017-018CM	FS	40.4	J	746					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_018-019CM	FS	39.5	J	713					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_019-020CM	FS	39.8	J	771					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_020-022CM	FS	42.2	J	711					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_022-024CM	FS	43.6	J	723					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_024-026CM	FS	45.6	J	754					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_026-028CM	FS	45	J	594					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_028-030CM	FS	41.4	J	671					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_030-032CM	FS	41.1	J	777					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_032-034CM	FS	38.2	J	811					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_034-036CM	FS	40.4	J	757					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_036-038CM	FS	41.9	J	740					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_038-040CM	FS	41.2	J	712					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_040-045CM	FS	40.2	J	709					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_045-050CM	FS	44.9	J	690					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_050-055CM	FS	42.5	J	858					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_055-060CM	FS	43.5	J	737					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_060-065CM	FS	43.8	J	853					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_065-070CM	FS	42	J	944					
1710634	MM-C1-C	10/6/2017	MM-C1-C-17_SED_070-075CM	FS	44	J	982					

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_000-001CM	FS	36.9	J	608	J		
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_001-002CM	FS	32.4	J	791	J		
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_002-003CM	FS	35.7	J	735	J		
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_003-004CM	FS	39.4	J	726	J		
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_004-005CM	FS	37.9	J	773	J		
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_005-006CM	FS	29.2	J	714	J		
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_006-007CM	FS	37.4	J	769	J		
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_007-008CM	FS	36.7	J	780	J		
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_008-009CM	FS	33.9	J	816	J		
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_009-010CM	FS	35.6	J	702	J		
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_010-011CM	FS	35.9	J	775	J		
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_011-012CM	FS	36.7	J	801			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_012-013CM	FS	38.1	J	801			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_013-014CM	FS	40.6	J	641			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_014-015CM	FS	42.1	J	698			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_015-016CM	FS	38	J	626			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_016-017CM	FS	37.7	J	848			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_017-018CM	FS	37.2	J	850			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_018-019CM	FS	38.4	J	936			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_019-020CM	FS	41.1	J	932			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_020-022CM	FS	40	J	847			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_022-024CM	FS	41.8	J	750			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_024-026CM	FS	37.4	J	403			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_026-028CM	FS	50.1	J	482			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_028-030CM	FS	48.2	J	342			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_030-032CM	FS	51.6	J	113			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_032-034CM	FS	51.6	J	70.9			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_034-036CM	FS	46.7	J	74.1			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_036-038CM	FS	51.1	J	65.5			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_038-040CM	FS	42	J	85.6			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_040-045CM	FS	51.1	J	62.7			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_045-050CM	FS	56.4	J	41.2			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_050-055CM	FS	56	J	35.3			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_055-060CM	FS	57.7	J	38			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_060-065CM	FS	57.1	J	30.1			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_065-070CM	FS	56.9	J	33.5			
1710637	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_070-075CM	FS	59.1	J	30.1			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_000-001CM	FS	18.4	J	1,820			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_001-002CM	FS	52.5	J	650			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_002-003CM	FS	40	J	788			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_003-004CM	FS	41.8	J	739			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_004-005CM	FS	17.1	J	1,060			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_005-006CM	FS	49.9	J	631			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_006-007CM	FS	51.2	J	598			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_007-008CM	FS	53	J	353			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_008-009CM	FS	52.4	J	187			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_009-010CM	FS	51.7	J	106			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_010-011CM	FS	55.1	J	57.2			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_011-012CM	FS	55.7	J	63.5			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_012-013CM	FS	51.4	J	72.1			

**TABLE 3
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_013-014CM	FS	58.7	J	41.2			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_014-015CM	FS	61.3	J	30.7			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_015-016CM	FS	62.6	J	29			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_016-017CM	FS	63.4	J	28.1			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_017-018CM	FS	63.8	J	22			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_018-019CM	FS	64.5	J	22.8			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_019-020CM	FS	63.8	J	27.8			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_020-022CM	FS	63.6	J	26.1			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_022-024CM	FS	7.1	J	151			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_024-026CM	FS	64.6	J	21.9			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_026-028CM	FS	65.8	J	23.5			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_028-030CM	FS	65.5	J	24			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_030-032CM	FS	67	J	20.1			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_032-034CM	FS	65.3	J	21.5			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_034-036CM	FS	65.8	J	18.8			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_036-038CM	FS	70.6	J	16.7			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_038-040CM	FS	66.8	J	18.5			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_040-045CM	FS	66.5	J	17.8			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_045-050CM	FS	66.4	J	18.8			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_050-055CM	FS	67	J	18.8			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_055-060CM	FS	66.6	J	16.4			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_060-065CM	FS	65.2	J	21.8			
1710639	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_065-070CM	FS	63.7	J	24.1			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_000-001CM	FS	29.5	J	494			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_001-002CM	FS	29.4	J	452			

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SDG	Location ID	Sample Date	Sample ID	Analysis Method	% Solids		EPA 1631		LLOYD KAHN	
				Parameter	PERCENT		Mercury		TOC	
				Unit	Total		NG/G		PERCENT	
QC Code	Final	Final	Final	Final	Final	Final				
				Fraction	Result	Qualifier	Result	Qualifier	Result	Qualifier
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_002-003CM	FS	27.2	J	452			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_003-004CM	FS	26.1	J	483			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_004-005CM	FS	26.3	J	592			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_005-006CM	FS	24.9	J	581			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_006-007CM	FS	26.1	J	624			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_007-008CM	FS	28.2	J	822			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_008-009CM	FS	27.9	J	949			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_009-010CM	FS	28	J	957			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_010-011CM	FS	27.7	J	970			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_011-012CM	FS	25.4	J	1,210			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_012-013CM	FS	26.3	J	1,090			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_013-014CM	FS	29	J	1,330			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_014-015CM	FS	29.8	J	1,820			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_015-016CM	FS	30.9	J	2,780			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_016-017CM	FS	30.7	J	2,520			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_017-018CM	FS	30.3	J	2,720			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_018-019CM	FS	30.6	J	4,110			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_019-020CM	FS	30.2	J	4,430			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_020-022CM	FS	26.7	J	3,180			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_022-024CM	FS	30.9	J	3,000			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_024-026CM	FS	32	J	2,300			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_026-028CM	FS	31.9	J	1,490			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_028-030CM	FS	28	J	426			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_030-032CM	FS	28.8	J	355			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_032-034CM	FS	26	J	320			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_034-036CM	FS	23.9	J	343			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_036-038CM	FS	28.5	J	286			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_038-040CM	FS	29.3	J	286			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_040-045CM	FS	34.4	J	182			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_045-050CM	FS	36.3	J	149			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_050-055CM	FS	41.4	J	56.9			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_055-060CM	FS	41.8	J	43.7			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_060-065CM	FS	45.3	J	38.7			
1710641	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_065-070CM	FS	44.6	J	43.1			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_000-001CM	FS	37.5	J	882			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_000-001CM_DUP	FD	38.3	J	826			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_001-002CM	FS	37.3	J	955			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_001-002CM_DUP	FD	38.2	J	919			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_002-003CM	FS	35.9	J	1,040			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_002-003CM_DUP	FD	35.7	J	1,100			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_003-004CM	FS	36.4	J	967			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_003-004CM_DUP	FD	36.8	J	1,020			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_004-005CM	FS	35.8	J	1,090			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_005-006CM	FS	39.7	J	971			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_005-006CM_DUP	FD	39.6	J	921			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_006-007CM	FS	40.4	J	942			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_006-007CM_DUP	FD	39	J	989			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_007-008CM	FS	40.7	J	916			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_007-008CM_DUP	FD	39.8	J	976			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_008-009CM	FS	40.7	J	1,020			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_008-009CM_DUP	FD	40.9	J	1,040			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_009-010CM	FS	41.2	J	874			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_009-010CM_DUP	FD	43.2	J	797			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_010-011CM	FS	40.1	J	944			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_010-011CM_DUP	FD	40.3	J	866			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_011-012CM	FS	5.9	J	1,930			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_011-012CM_DUP	FD	6.1	J	2,520			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_012-013CM	FS	36.8	J	907			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_012-013CM_DUP	FD	37.4	J	857			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_013-014CM	FS	37.4	J	929			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_013-014CM_DUP	FD	37.3	J	917			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_014-015CM	FS	38	J	1,060			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_014-015CM_DUP	FD	38.3	J	947			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_015-016CM	FS	36	J	1,040			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_015-016CM_DUP	FD	35.7	J	1,040			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_016-017CM	FS	36.7	J	1,190			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_016-017CM_DUP	FD	36.5	J	1,150			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_017-018CM	FS	35.9	J	1,260			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_017-018CM_DUP	FD	37.3	J	1,310			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_018-019CM	FS	37	J	1,030			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_018-019CM_DUP	FD	36.9	J	1,070			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_019-020CM	FS	36.8	J	1,020			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_019-020CM_DUP	FD	37.8	J	1,010			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_020-022CM	FS	36.6	J	1,080			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_020-022CM_DUP	FD	37.2	J	928			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_022-024CM	FS	36.2	J	756			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_022-024CM_DUP	FD	37.6	J	783			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_024-026CM	FS	36.7	J	545			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_024-026CM_DUP	FD	37.3	J	474			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_026-028CM	FS	39.4	J	349			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_026-028CM_DUP	FD	39.2	J	367			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_028-030CM	FS	39.2	J	275			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_028-030CM_DUP	FD	38.6	J	317			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_030-032CM	FS	39.9	J	224			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_030-032CM_DUP	FD	40	J	254			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_032-034CM	FS	38.1	J	355			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_032-034CM_DUP	FD	39.1	J	258			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_034-036CM	FS	37.7	J	215			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_034-036CM_DUP	FD	39.2	J	227			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_036-038CM	FS	42.7	J	165			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_036-038CM_DUP	FD	42.3	J	180			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_038-040CM	FS	36.7	J	223			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_038-040CM_DUP	FD	38	J	206			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_040-045CM	FS	38.9	J	212			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_040-045CM_DUP	FD	38.7	J	141			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_045-050CM	FS	33.2	J	136	J		
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_045-050CM_DUP	FD	34.9	J	295	J		
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_050-055CM	FS	43.2	J	107			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_050-055CM_DUP	FD	43.4	J	105			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_055-060CM	FS	44.5	J	86			

**TABLE 3
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_055-060CM_DUP	FD	44.7	J	89.9			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_060-065CM	FS	45	J	66.2			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_060-065CM_DUP	FD	46.1	J	65.3			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_065-070CM	FS	48.2	J	68.5			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_065-070CM_DUP	FD	48.1	J	62.9			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_070-075CM	FS	47.2	J	58.6			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_070-075CM_DUP	FD	45.7	J	61.4			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_075-080CM	FS	55.9	J	55.3			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_075-080CM_DUP	FD	51.4	J	52.5			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_080-085CM	FS	55.2	J	44.8			
1710682	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_080-085CM_DUP	FD	54.9	J	41.3			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_000-001CM	FS	43.3	J	225			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_000-001CM_DUP	FD	41.8	J	278			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_001-002CM	FS	42.8	J	218			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_001-002CM_DUP	FD	44.2	J	203			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_002-003CM	FS	45.3	J	171			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_002-003CM_DUP	FD	46.4	J	177			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_003-004CM	FS	54.2	J	158			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_003-004CM_DUP	FD	53.3	J	159			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_004-005CM	FS	51.6	J	232			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_004-005CM_DUP	FD	52.9	J	244			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_005-006CM	FS	50.1	J	246			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_005-006CM_DUP	FD	49.2	J	248			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_006-007CM	FS	54.3	J	290			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_006-007CM_DUP	FD	54.6	J	286			

**TABLE 3
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_007-008CM	FS	49.9	J	326			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_007-008CM_DUP	FD	49.7	J	305			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_008-009CM	FS	55.8	J	303			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_008-009CM_DUP	FD	56.4	J	290			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_009-010CM	FS	48.3	J	366			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_009-010CM_DUP	FD	48.4	J	380			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_010-011CM	FS	53.7	J	325			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_010-011CM_DUP	FD	54	J	316			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_011-012CM	FS	50.3	J	407			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_011-012CM_DUP	FD	51.3	J	398			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_012-013CM	FS	44.8	J	467			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_012-013CM_DUP	FD	45.8	J	458			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_013-014CM	FS	43	J	615			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_013-014CM_DUP	FD	43.7	J	569			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_014-015CM	FS	44.9	J	520			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_014-015CM_DUP	FD	43.6	J	557			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_015-016CM	FS	46.2	J	519			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_015-016CM_DUP	FD	46.3	J	498			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_016-017CM	FS	59.8	J	299			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_016-017CM_DUP	FD	59	J	299			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_017-018CM	FS	52.4	J	352			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_017-018CM_DUP	FD	52.6	J	365			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_018-019CM	FS	38.9	J	409			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_018-019CM_DUP	FD	37.3	J	490			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_019-020CM	FS	50.7	J	313			

**TABLE 3
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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_019-020CM_DUP	FD	48.7	J	303			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_020-022CM	FS	49	J	424			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_020-022CM_DUP	FD	48.4	J	454			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_022-024CM	FS	60.9	J	176			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_022-024CM_DUP	FD	61.4	J	190			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_024-026CM	FS	77.3	J	36.8			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_024-026CM_DUP	FD	77.5	J	30.8			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_026-028CM	FS	80.3	J	24.9			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_026-028CM_DUP	FD	81	J	23.7			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_028-030CM	FS	79.5	J	20.8			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_028-030CM_DUP	FD	79.2	J	21			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_030-032CM	FS	77.8	J	69.5			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_030-032CM_DUP	FD	77.5	J	64.8			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_032-034CM	FS	69.4	J	192			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_032-034CM_DUP	FD	69.6	J	221			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_034-036CM	FS	79.6	J	94.3			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_034-036CM_DUP	FD	80.1	J	92.8			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_036-038CM	FS	81.6	J	20.6			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_036-038CM_DUP	FD	81.5	J	19.8			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_038-040CM	FS	82.6	J	17			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_038-040CM_DUP	FD	82.2	J	17.2			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_040-045CM	FS	84.6	J	16.9			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_040-045CM_DUP	FD	84.9	J	16			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_045-050CM	FS	85.3	J	27.6			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_045-050CM_DUP	FD	85.2	J	29.1			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_050-055CM	FS	81	J	77			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_050-055CM_DUP	FD	80.7	J	47.1			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_055-060CM	FS	74	J	30.5			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_055-060CM_DUP	FD	77.6	J	18.8			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_060-065CM	FS	80	J	11.9			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_060-065CM_DUP	FD	79.7	J	12.9			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_065-070CM	FS	85.9	J	11.4			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_065-070CM_DUP	FD	86.2	J	12.9			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_070-075CM	FS	85.5	J	6.88			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_070-075CM_DUP	FD	84.7	J	9.86			
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_075-080CM	FS	83.6	J	4.17	J		
1710684	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_075-080CM_DUP	FD	87.1	J	4.23			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_000-001CM	FS	47.4	J	647			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_000-001CM_DUP	FD	47	J	676			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_001-002CM	FS	43.2	J	703			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_001-002CM_DUP	FD	42.4	J	738			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_002-003CM	FS	43.9	J	726			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_003-004CM	FS	40.2	J	862			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_003-004CM_DUP	FD	40.4	J	832			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_004-005CM	FS	38.8	J	832			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_004-005CM_DUP	FD	38.8	J	845			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_005-006CM	FS	38.9	J	886			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_005-006CM_DUP	FD	39	J	1,200			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_006-007CM	FS	38.1	J	879			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_006-007CM_DUP	FD	38.4	J	935			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_007-008CM	FS	40	J	742			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_008-009CM	FS	38	J	858			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_008-009CM_DUP	FD	37.7	J	832			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_009-010CM	FS	39	J	911			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_009-010CM_DUP	FD	38.9	J	911			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_010-011CM	FS	40.2	J	887			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_010-011CM_DUP	FD	40.4	J	886			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_011-012CM	FS	42.3	J	896			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_011-012CM_DUP	FD	42.8	J	1,070			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_012-013CM	FS	42.1	J	845			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_012-013CM_DUP	FD	42.4	J	852			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_013-014CM	FS	42.6	J	921			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_013-014CM_DUP	FD	43.6	J	869			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_014-015CM	FS	42.2	J	966			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_014-015CM_DUP	FD	41.9	J	885			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_015-016CM	FS	42.2	J	969			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_015-016CM_DUP	FD	41.8	J	929			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_016-017CM	FS	40.6	J	999			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_016-017CM_DUP	FD	41.1	J	1,130			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_017-018CM	FS	41.3	J	1,220			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_017-018CM_DUP	FD	42.5	J	1,060			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_018-019CM	FS	24.1	J	800	J		
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_018-019CM_DUP	FD	12.3	J	1,570	J		
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_019-020CM	FS	40.9	J	1,220			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_019-020CM_DUP	FD	41	J	1,130			

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_020-022CM	FS	40.7	J	1,250			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_020-022CM_DUP	FD	41	J	1,210			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_022-024CM	FS	43.5	J	1,200			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_022-024CM_DUP	FD	43.3	J	1,050			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_024-026CM	FS	42.7	J	1,250			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_024-026CM_DUP	FD	42.6	J	1,360			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_026-028CM	FS	41.2	J	1,430			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_026-028CM_DUP	FD	41	J	1,440			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_028-030CM	FS	41.6	J	1,350			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_028-030CM_DUP	FD	41.4	J	1,350			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_030-032CM	FS	40.9	J	1,440			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_030-032CM_DUP	FD	41.4	J	1,390			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_032-034CM	FS	41.3	J	1,630			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_032-034CM_DUP	FD	41.5	J	1,690			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_034-036CM	FS	32.4	J	1,880			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_034-036CM_DUP	FD	32.8	J	1,820			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_036-038CM	FS	40.2	J	2,300			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_036-038CM_DUP	FD	40.3	J	2,030			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_038-040CM	FS	39.7	J	3,020			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_038-040CM_DUP	FD	39.6	J	3,010			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_040-045CM	FS	39.4	J	3,510			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_040-045CM_DUP	FD	39.7	J	3,560			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_045-050CM	FS	42.2	J	2,420			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_045-050CM_DUP	FD	42.1	J	2,490			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_050-055CM	FS	42.6	J	2,190			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_050-055CM_DUP	FD	42.7	J	2,260			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_055-060CM	FS	50.2	J	1,170			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_055-060CM_DUP	FD	50.1	J	1,340			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_060-065CM	FS	42.9	J	874			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_060-065CM_DUP	FD	41.9	J	882			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_065-070CM	FS	44	J	449			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_065-070CM_DUP	FD	44.5	J	453			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_070-075CM	FS	45.3	J	258			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_070-075CM_DUP	FD	44.9	J	237			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_075-080CM	FS	42	J	267			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_075-080CM_DUP	FD	43.1	J	258			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_080-085CM	FS	44.2	J	312			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_080-085CM_DUP	FD	44.5	J	287			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_085-090CM	FS	47.7	J	185			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_085-090CM_DUP	FD	48.8	J	162			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_090-095CM	FS	51	J	49.4			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_090-095CM_DUP	FD	51.6	J	48.2			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_095-101CM	FS	55.2	J	22.9			
1710685	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_095-101CM_DUP	FD	51.4	J	24.3			
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_000-001CM	FS	23.2	J	232			
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_001-002CM	FS	22.4	J	221			
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_002-003CM	FS	23.9	J	188			
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_003-004CM	FS	19.4	J	205			
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_004-005CM	FS	19.8	J	203			
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_005-006CM	FS	20	J	322			

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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
Final	Final	Final	Final	Final	Final	Final	Final	Final	Final			
Result	Qualifier	Result	Qualifier	Result	Qualifier	Result	Qualifier	Result	Qualifier			
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_006-007CM	FS	31.2	J	885					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_007-008CM	FS	24.5	J	520					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_008-009CM	FS	30.5	J	581					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_009-010CM	FS	31.5	J	915					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_010-011CM	FS	22.5	J	728					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_011-012CM	FS	21.6	J	535					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_012-013CM	FS	20.6	J	699					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_013-014CM	FS	22.5	J	296					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_014-015CM	FS	25.6	J	143					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_015-016CM	FS	27.9	J	34.5					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_016-017CM	FS	28.5	J	33.3					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_017-018CM	FS	30.1	J	25.7					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_018-019CM	FS	28.6	J	15.1					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_019-020CM	FS	28.6	J	9.52	J				
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_020-022CM	FS	28.7	J	9.62	J				
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_022-024CM	FS	31.8	J	12					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_024-026CM	FS	34.7	J	14.4					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_026-028CM	FS	32.5	J	20.1					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_028-030CM	FS	38.5	J	26.6					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_030-032CM	FS	38.3	J	77.1					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_032-034CM	FS	37.2	J	17.6					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_034-036CM	FS	34.4	J	28					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_036-038CM	FS	41.6	J	47.8					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_038-040CM	FS	40.6	J	24.6					
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_040-045CM	FS	37.6	J	28.6					

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	% Solids		EPA 1631		LLOYD KAHN		
					Parameter	PERCENT	Mercury	TOC				
					Unit	Total	Final	Final	Final	Final	Final	
					Fraction		Result	Qualifier	Result	Qualifier	Result	Qualifier
									NG/G		PERCENT	
									Total		Total	
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_045-050CM	FS		37.8	J		19.1			
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_050-055CM	FS		37.9	J		25.4			
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_055-060CM	FS		28.5	J		19.8			
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_060-065CM	FS		28.2	J		20.2			
1710728	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_065-070CM	FS		27.8	J		18.5			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_000-001CM	FS		41	J		293			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_001-002CM	FS		43.9	J		232			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_002-003CM	FS		45.9	J		162			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_003-004CM	FS		47.2	J		185			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_004-005CM	FS		47.6	J		80.9			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_005-006CM	FS		48.7	J		56.7			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_006-007CM	FS		48	J		38.1			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_007-008CM	FS		50.1	J		31			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_008-009CM	FS		47.7	J		26.9			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_009-010CM	FS		44.7	J		20.6			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_010-011CM	FS		45.1	J		20.1			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_011-012CM	FS		42.5	J		19.4			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_012-013CM	FS		40.4	J		26.2			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_013-014CM	FS		38	J		25			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_014-015CM	FS		38.8	J		28.6			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_015-016CM	FS		40.5	J		26			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_016-017CM	FS		49.7	J		26.1			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_017-018CM	FS		50.7	J		26.5			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_018-019CM	FS		48.1	J		27.5			
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_019-020CM	FS		45.9	J		27.8			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
					Final	Final	Final	Final	Final	Final		
					Result	Qualifier	Result	Qualifier	Result	Qualifier		
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_020-022CM	FS	48.1	J	31					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_022-024CM	FS	53	J	30.7					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_024-026CM	FS	51.1	J	27.5					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_026-028CM	FS	48.9	J	27.7					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_028-030CM	FS	47.5	J	32.5					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_030-032CM	FS	46.7	J	28					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_032-034CM	FS	47.6	J	29.2					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_034-036CM	FS	48.3	J	27.5					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_036-038CM	FS	47.6	J	32.4					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_038-040CM	FS	49.7	J	36					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_040-045CM	FS	52.3	J	29					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_045-050CM	FS	56.8	J	25.7					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_050-055CM	FS	64	J	23.3					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_055-060CM	FS	69.5	J	17.7					
1710729	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_060-065CM	FS	66.6	J	19.5					
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_000-001CM	FS	40.2	J	690					
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_001-002CM	FS	42	J	799					
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_002-003CM	FS	41.2	J	857					
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_003-004CM	FS	41.9	J	858					
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_004-005CM	FS	42.7	J	765					
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_005-006CM	FS	43.7	J	913					
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_006-007CM	FS	43.8	J	994					
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_007-008CM	FS	42.3	J	916					
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_008-009CM	FS	42.5	J	998					
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_009-010CM	FS	45.3	J	992					

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method	% Solids		EPA 1631		LLOYD KAHN	
				Parameter	PERCENT		Mercury		TOC	
				Unit	Total		NG/G		PERCENT	
QC Code	Final	Final	Final	Final	Final	Final				
				Fraction	Result	Qualifier	Total	Qualifier	Total	Qualifier
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_010-011CM	FS	45.3	J	1,050			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_011-012CM	FS	45.8	J	1,240			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_012-013CM	FS	45.9	J	1,570			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_013-014CM	FS	45.5	J	2,350			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_014-015CM	FS	42	J	2,890			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_015-016CM	FS	42.2	J	2,580			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_016-017CM	FS	42	J	2,820			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_017-018CM	FS	42.5	J	2,960	J		
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_018-019CM	FS	43.5	J	2,710			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_019-020CM	FS	42.5	J	2,900			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_020-022CM	FS	42.5	J	2,810			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_022-024CM	FS	40.1	J	2,870			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_024-026CM	FS	42.3	J	2,160			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_026-028CM	FS	41.3	J	1,370			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_028-030CM	FS	39.8	J	1,170			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_030-032CM	FS	35.8	J	653			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_032-034CM	FS	41	J	514			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_034-036CM	FS	39.4	J	453			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_036-038CM	FS	41.7	J	397			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_038-040CM	FS	42.3	J	350			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_040-045CM	FS	45.8	J	222			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_045-050CM	FS	50.1	J	135			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_050-055CM	FS	48.9	J	113			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_055-060CM	FS	48.7	J	121			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_060-065CM	FS	48.3	J	103			

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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_065-070CM	FS	51.1	J	83.1			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_070-075CM	FS	54.8	J	68.7			
1710730	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_075-080CM	FS	56.6	J	66.5			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_000-001CM	FS	26.5	J	282			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_001-002CM	FS	26.1	J	310			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_002-003CM	FS	24.5	J	362			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_003-004CM	FS	22	J	432			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_004-005CM	FS	24.1	J	580			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_005-006CM	FS	22.8	J	749			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_006-007CM	FS	23.4	J	843			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_007-008CM	FS	24.7	J	1,240			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_008-009CM	FS	30.1	J	1,380			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_009-010CM	FS	29.4	J	1,760			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_010-011CM	FS	27	J	2,050			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_011-012CM	FS	27.4	J	1,630			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_012-013CM	FS	27.2	J	1,180			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_013-014CM	FS	27.6	J	805			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_014-015CM	FS	26.6	J	632			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_015-016CM	FS	26.1	J	458			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_016-017CM	FS	27.7	J	379			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_017-018CM	FS	29.1	J	305			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_018-019CM	FS	32.5	J	261			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_019-020CM	FS	33.1	J	240			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_020-022CM	FS	36.7	J	160			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_022-024CM	FS	31.3	J	107			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_024-026CM	FS	33.9	J	78.1			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_026-028CM	FS	37.5	J	64.4			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_028-030CM	FS	39.5	J	39.5			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_030-032CM	FS	37.3	J	22.8			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_032-034CM	FS	38.4	J	27			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_034-036CM	FS	34.5	J	26.3			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_036-038CM	FS	33.7	J	26.5			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_038-040CM	FS	39.2	J	27.4			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_040-045CM	FS	43.8	J	27.2			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_045-050CM	FS	42.6	J	20.2			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_050-055CM	FS	49.1	J	19			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_055-060CM	FS	53.7	J	18.9			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_060-065CM	FS	51.7	J	20.1			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_065-070CM	FS	51.1	J	17			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_070-075CM	FS	65	J	22.6			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_075-080CM	FS	57.1	J	23.7			
1710731	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_080-085CM	FS	52	J	24			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_000-001CM	FS	34.4	J	482			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_001-002CM	FS	31.1	J	531			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_002-003CM	FS	33.8	J	614			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_003-004CM	FS	35.7	J	706			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_004-005CM	FS	34.1	J	688			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_005-006CM	FS	31.8	J	616			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_006-007CM	FS	29.3	J	537			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_007-008CM	FS	29.5	J	749			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_008-009CM	FS	32.8	J	899			

**TABLE 3
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_009-010CM	FS	33.5	J	984			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_010-011CM	FS	29.5	J	1,180			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_011-012CM	FS	31.4	J	989			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_012-013CM	FS	32	J	1,140			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_013-014CM	FS	34.4	J	1,540			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_014-015CM	FS	37.9	J	1,820			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_015-016CM	FS	35.9	J	1,880			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_016-017CM	FS	35.4	J	2,620			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_017-018CM	FS	34.7	J	2,120			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_018-019CM	FS	33.9	J	1,750			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_019-020CM	FS	35.7	J	1,500			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_020-022CM	FS	34.7	J	606			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_022-024CM	FS	27.9	J	330			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_024-026CM	FS	33	J	278			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_026-028CM	FS	37.3	J	184			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_028-030CM	FS	36.4	J	133			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_030-032CM	FS	43.7	J	96.3			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_032-034CM	FS	38.7	J	68.8			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_034-036CM	FS	45.1	J	47.5			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_036-038CM	FS	44.3	J	32.7			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_038-040CM	FS	41.1	J	24.3			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_040-045CM	FS	31.1	J	25.7			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_045-050CM	FS	31.5	J	35.5			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_050-055CM	FS	35.4	J	24.4			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_055-060CM	FS	30.9	J	21.3			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_060-065CM	FS	24.4	J	20.9			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	% Solids		EPA 1631		LLOYD KAHN		
					Parameter	PERCENT	Mercury	TOC				
					Unit	Total	Final	Final	Final	Final		
					Fraction		Result	Qualifier	Result	Qualifier	Result	Qualifier
									NG/G	PERCENT		
									Total	Total		
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_065-070CM	FS		25.3	J		16.3			
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_070-075CM	FS		20.8	J		12.2	J		
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_075-080CM	FS		18.5	J		11	J		
1710732	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_080-085CM	FS		19.3	J		11.2	J		
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_000-001CM	FS		26.7	J		502			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_001-002CM	FS		27.2	J		482			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_002-003CM	FS		27.5	J		432			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_003-004CM	FS		27.5	J		396			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_004-005CM	FS		28.5	J		578			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_005-006CM	FS		25.9	J		828			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_006-007CM	FS		26.5	J		735			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_007-008CM	FS		23.7	J		885			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_008-009CM	FS		26	J		1,300			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_009-010CM	FS		26.7	J		1,610			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_010-011CM	FS		27.8	J		1,600			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_011-012CM	FS		26.5	J		1,380			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_012-013CM	FS		22	J		1,450			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_013-014CM	FS		21.3	J		1,430			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_014-015CM	FS		18.2	J		1,530			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_015-016CM	FS		18.9	J		914			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_016-017CM	FS		18.6	J		740			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_017-018CM	FS		18.4	J		503			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_018-019CM	FS		21	J		381			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_019-020CM	FS		22.4	J		371			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_020-022CM	FS		20.6	J		197			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_022-024CM	FS		24.6	J		133			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_024-026CM	FS	25.6	J	91.7			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_026-028CM	FS	23.7	J	59.1	J		
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_028-030CM	FS	23.8	J	102			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_030-032CM	FS	26.6	J	93.7			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_032-034CM	FS	34.6	J	66.7			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_034-036CM	FS	33.6	J	27.3			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_036-038CM	FS	28.4	J	29.2			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_038-040CM	FS	31.8	J	24			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_040-045CM	FS	31.7	J	18			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_045-050CM	FS	46	J	20			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_050-055CM	FS	51.4	J	15.5			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_055-060CM	FS	36.2	J	8.95	J		
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_060-065CM	FS	35.8	J	11.2			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_065-070CM	FS	39.6	J	12.4			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_070-075CM	FS	35.5	J	18.9			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_075-080CM	FS	34.2	J	20.4			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_080-085CM	FS	29.1	J	15.1			
1710733	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_085-090CM	FS	34.3	J	36.9			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_000-001CM	FS	46.8	J	729			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_000-001CM_DUP	FD	46	J	728			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_001-002CM	FS	45.7	J	651			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_001-002CM_DUP	FD	46.1	J	738			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_002-003CM	FS	42.1	J	875			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_002-003CM_DUP	FD	44.1	J	842			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_003-004CM	FS	44	J	826			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_003-004CM_DUP	FD	44.1	J	891			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_004-005CM	FS	45.6	J	823			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_004-005CM_DUP	FD	45.8	J	853			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_005-006CM	FS	47.2	J	775			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_005-006CM_DUP	FD	47.2	J	903			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_006-007CM	FS	46.5	J	854			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_006-007CM_DUP	FD	46.4	J	768			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_007-008CM	FS	44	J	793			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_007-008CM_DUP	FD	44.6	J	854			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_008-009CM	FS	44.1	J	777			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_008-009CM_DUP	FD	44	J	805			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_009-010CM	FS	46.1	J	707			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_009-010CM_DUP	FD	46.9	J	710			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_010-011CM	FS	45.8	J	719			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_010-011CM_DUP	FD	45.5	J	715			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_011-012CM	FS	44	J	840			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_011-012CM_DUP	FD	43	J	855			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_012-013CM	FS	41.3	J	866			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_012-013CM_DUP	FD	40.8	J	935			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_013-014CM	FS	44.7	J	768			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_013-014CM_DUP	FD	44.9	J	785			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_014-015CM	FS	42.4	J	872			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_014-015CM_DUP	FD	43.3	J	893			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_015-016CM	FS	43	J	745			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_015-016CM_DUP	FD	42.8	J	737			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_016-017CM	FS	47.5	J	712			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_016-017CM_DUP	FD	44.7	J	763			

**TABLE 3
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method Parameter Unit Fraction		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_017-018CM	FS	47.5	J	701			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_017-018CM_DUP	FD	46.1	J	759			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_018-019CM	FS	44.8	J	886			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_018-019CM_DUP	FD	44.2	J	746			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_019-020CM	FS	46	J	784			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_019-020CM_DUP	FD	45.7	J	789			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_020-022CM	FS	45.3	J	786			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_020-022CM_DUP	FD	46.3	J	736			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_024-026CM	FS	44.8	J	1,040			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_024-026CM_DUP	FD	46.1	J	998			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_026-028CM	FS	47.7	J	997			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_026-028CM_DUP	FD	47.4	J	933			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_028-030CM	FS	45.7	J	1,010			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_028-030CM_DUP	FD	45.4	J	993			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_030-032CM	FS	44.3	J	1,050			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_030-032CM_DUP	FD	42.8	J	1,050			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_032-034CM	FS	45.6	J	1,030			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_032-034CM_DUP	FD	46.5	J	1,150			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_034-036CM	FS	44.9	J	1,080			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_034-036CM_DUP	FD	44.9	J	1,140			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_036-038CM	FS	42.9	J	1,010			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_036-038CM_DUP	FD	43.7	J	675			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_038-040CM	FS	42.6	J	434			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_038-040CM_DUP	FD	42.7	J	471			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_040-045CM	FS	41.5	J	397			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_040-045CM_DUP	FD	42.1	J	415			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
Final	Final	Final	Final	Final	Final	Final	Final	Final	Final			
Result	Qualifier	Result	Qualifier	Result	Qualifier	Result	Qualifier	Result	Qualifier			
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_045-050CM	FS	39.6	J	221					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_045-050CM_DUP	FD	40.5	J	242					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_050-055CM	FS	43.4	J	152					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_050-055CM_DUP	FD	44	J	155					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_055-060CM	FS	46.7	J	143					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_055-060CM_DUP	FD	46.6	J	140					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_060-065CM	FS	48.9	J	135					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_060-065CM_DUP	FD	47.9	J	142					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_065-070CM	FS	43.7	J	140					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_065-070CM_DUP	FD	43.6	J	121					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_070-075CM	FS	39.4	J	118					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_070-075CM_DUP	FD	39.5	J	110					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_075-080CM	FS	21.6	J	168					
1710907	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_075-080CM_DUP	FD	22	J	158					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_000-001CM	FS	20.6	J	184					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_001-002CM	FS	20.2	J	102					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_002-003CM	FS	18.9	J	200					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_003-004CM	FS	19.9	J	255					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_004-005CM	FS	22.1	J	416					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_005-006CM	FS	21.9	J	529					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_006-007CM	FS	19.4	J	439					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_007-008CM	FS	19.8	J	377					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_008-009CM	FS	20.5	J	301					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_009-010CM	FS	20.6	J	268					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_010-011CM	FS	21.3	J	270					
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_011-012CM	FS	23.8	J	158					

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_012-013CM	FS	23.5	J	167			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_013-014CM	FS	24	J	118			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_014-015CM	FS	22.7	J	97.7			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_015-016CM	FS	22.4	J	71.4			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_016-017CM	FS	24.2	J	65			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_017-018CM	FS	27.7	J	49.7			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_018-019CM	FS	27.6	J	40.4			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_019-020CM	FS	27.9	J	34.3			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_020-022CM	FS	29.6	J	310			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_022-024CM	FS	30.7	J	29.6			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_024-026CM	FS	26.8	J	27.3			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_026-028CM	FS	22.1	J	41.1			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_028-030CM	FS	21.5	J	35.1			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_030-032CM	FS	23.4	J	29.3			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_032-034CM	FS	25.1	J	20.8			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_034-036CM	FS	25	J	24.2			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_036-038CM	FS	21.4	J	22.9			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_038-040CM	FS	23.2	J	19.3			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_040-045CM	FS	26.5	J	14.1			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_045-050CM	FS	26.6	J	13.2			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_050-055CM	FS	27.6	J	29.1			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_055-060CM	FS	30.7	J	15.4			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_060-065CM	FS	32.8	J	17.9			
1710910	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_065-070CM	FS	35	J	34.3			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_000-001CM	FS	35.2	J	681			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_000-001CM_DUP	FD	36.5	J	645			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
Final	Final	Final	Final	Final	Final							
Result	Qualifier	Result	Qualifier	Result	Qualifier							
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_001-002CM	FS	37.5	J	844					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_001-002CM_DUP	FD	37.7	J	872					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_002-003CM	FS	40	J	803					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_002-003CM_DUP	FD	40	J	785					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_003-004CM	FS	43.7	J	476					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_003-004CM_DUP	FD	41.5	J	516					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_004-005CM	FS	44.6	J	364					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_004-005CM_DUP	FD	45.1	J	284					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_005-006CM	FS	46.8	J	130					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_005-006CM_DUP	FD	46.8	J	110					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_006-007CM	FS	48.7	J	63.9					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_006-007CM_DUP	FD	49	J	47.4					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_007-008CM	FS	48	J	97.6					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_007-008CM_DUP	FD	48.4	J	108					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_008-009CM	FS	41.9	J	578					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_008-009CM_DUP	FD	33	J	771					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_009-010CM	FS	42.5	J	643					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_009-010CM_DUP	FD	39	J	680					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_010-011CM	FS	40.8	J	631					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_010-011CM_DUP	FD	37.1	J	713					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_011-012CM	FS	37.6	J	733					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_011-012CM_DUP	FD	38.4	J	746					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_012-013CM	FS	39.1	J	653					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_012-013CM_DUP	FD	39.1	J	632					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_013-014CM	FS	37.7	J	703					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_013-014CM_DUP	FD	37.4	J	665					

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_014-015CM	FS	33.9	J	659			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_014-015CM_DUP	FD	36.7	J	651			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_015-016CM	FS	40.5	J	576			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_015-016CM_DUP	FD	42.9	J	487			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_016-017CM	FS	39.7	J	577			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_016-017CM_DUP	FD	37.7	J	609			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_017-018CM	FS	46.7	J	414			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_017-018CM_DUP	FD	46.9	J	441			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_018-019CM	FS	43.4	J	515			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_018-019CM_DUP	FD	42.7	J	508			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_019-020CM	FS	46.9	J	300			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_019-020CM_DUP	FD	53.9	J	343			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_020-022CM	FS	74.8	J	34.4			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_020-022CM_DUP	FD	72.9	J	34.9			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_022-024CM	FS	76.6	J	10			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_022-024CM_DUP	FD	78.1	J	9.35			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_024-026CM	FS	76	J	8.4			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_024-026CM_DUP	FD	76.3	J	8.22			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_026-028CM	FS	69.8	J	11.2			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_026-028CM_DUP	FD	72	J	11.2			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_028-030CM	FS	73.3	J	9.76			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_028-030CM_DUP	FD	74	J	9.79			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_030-032CM	FS	74.1	J	12.1			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_030-032CM_DUP	FD	72.9	J	12.6			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_032-034CM	FS	78.1	J	9.26			
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_032-034CM_DUP	FD	78.5	J	8.44			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
Final	Final	Final	Final	Final	Final	Final	Final					
Result	Qualifier	Result	Qualifier	Result	Qualifier	Result	Qualifier					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_034-036CM	FS	75.8	J	9.39					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_034-036CM_DUP	FD	75.4	J	9.16					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_036-038CM	FS	78.6	J	10.3					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_036-038CM_DUP	FD	79.7	J	9.35					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_038-040CM	FS	78.6	J	9.41					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_038-040CM_DUP	FD	78.7	J	9.5					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_040-045CM	FS	76.1	J	10.2					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_040-045CM_DUP	FD	77.9	J	9.15					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_050-055CM	FS	73.9	J	10.7					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_050-055CM_DUP	FD	75	J	12.9					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_060-065CM	FS	73.5	J	9.87					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_060-065CM_DUP	FD	73.5	J	10.5					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_065-070CM	FS	70	J	9.79					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_065-070CM_DUP	FD	72.3	J	9.84					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_070-075CM	FS	74.8	J	10.3					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_070-075CM_DUP	FD	76	J	9.14					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_075-080CM	FS	74.6	J	8.97					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_075-080CM_DUP	FD	73	J	10.8					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_080-085CM	FS	74.9	J	8.52					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_080-085CM_DUP	FD	75	J	8.18					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_085-090CM	FS	76.1	J	8.98					
1710913	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_085-090CM_DUP	FD	76.9	J	8.59					
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_000-001CM	FS	29	J	669					
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_001-002CM	FS	26.7	J	568					
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_002-003CM	FS	31.1	J	553					
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_003-004CM	FS	29.9	J	581					

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	% Solids		EPA 1631		LLOYD KAHN	
					Parameter	PERCENT	Mercury	TOC	Unit	Total	PERCENT
					Fraction	Final	Final	Final	Final	Final	Final
						Result	Qualifier	Result	Qualifier	Result	Qualifier
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_004-005CM	FS		28.3	J	574			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_005-006CM	FS		27.9	J	560			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_006-007CM	FS		28.6	J	840	J		
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_007-008CM	FS		33.9	J	945			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_008-009CM	FS		35.1	J	833			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_009-010CM	FS		31.7	J	894			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_010-011CM	FS		29.6	J	790			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_011-012CM	FS		30.3	J	830			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_012-013CM	FS		30.3	J	1,430			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_013-014CM	FS		30.6	J	1,740			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_014-015CM	FS		29.7	J	2,060			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_015-016CM	FS		26.6	J	2,320			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_016-017CM	FS		28.1	J	2,790			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_017-018CM	FS		27.5	J	3,770			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_018-019CM	FS		26.1	J	3,340			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_019-020CM	FS		26	J	2,780			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_020-022CM	FS		29.3	J	2,490			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_022-024CM	FS		29.1	J	2,110			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_024-026CM	FS		27.7	J	1,120			
1710916	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_026-028CM	FS		29.3	J	414			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_028-030CM	FS		28.9	J	290			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_030-032CM	FS		26.2	J	228			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_032-034CM	FS		25.2	J	305			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_034-036CM	FS		27.5	J	352			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_036-038CM	FS		28.3	J	291			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_038-040CM	FS		32.4	J	215			

**TABLE 3
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	% Solids		EPA 1631		LLOYD KAHN		
					Parameter	PERCENT	Mercury	TOC				
					Unit	Total	Final	Final	Final	Final	Final	
					Fraction	Total	Result	Qualifier	Result	Qualifier	Result	Qualifier
									NG/G	PERCENT		
									Total	Total		
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_040-045CM	FS		34.9	J		131			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_045-050CM	FS		39.8	J		63.6			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_050-055CM	FS		44.1	J		31.6			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_055-060CM	FS		45.9	J		28.8			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_060-065CM	FS		52.3	J		30.5			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_065-070CM	FS		42.1	J		29.1			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_070-075CM	FS		43.9	J		25.4			
1710916	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_075-080CM	FS		43.5	J		19.7			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_000-001CM	FS		45.7	J		740			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_001-002CM	FS		42	J		680			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_002-003CM	FS		43	J		723			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_003-004CM	FS		42.2	J		670			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_004-005CM	FS		42.1	J		721			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_005-006CM	FS		41.6	J		812			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_006-007CM	FS		41.5	J		826			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_007-008CM	FS		43.3	J		937			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_008-009CM	FS		40.9	J		829			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_009-010CM	FS		43.2	J		889			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_010-011CM	FS		41.5	J		851			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_011-012CM	FS		43.2	J		831			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_012-013CM	FS		45.7	J		637			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_013-014CM	FS		44.7	J		510			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_014-015CM	FS		47.9	J		400			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_015-016CM	FS		50.2	J		333			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_016-017CM	FS		49.8	J		227			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_017-018CM	FS		49.5	J		190			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_018-019CM	FS	52.7	J	155			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_019-020CM	FS	51	J	150			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_020-022CM	FS	50	J	166			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_022-024CM	FS	52	J	124			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_024-026CM	FS	54	J	116			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_026-028CM	FS	52.9	J	106			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_028-030CM	FS	54.1	J	103			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_030-032CM	FS	54.2	J	89.4			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_032-034CM	FS	50.8	J	106			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_034-036CM	FS	56.3	J	79.5			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_036-038CM	FS	61.5	J	53.2			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_038-040CM	FS	62.4	J	40.4			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_040-045CM	FS	64	J	28.1			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_045-050CM	FS	66.7	J	24.1			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_055-060CM	FS	66	J	22.1			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_060-065CM	FS	62.7	J	24.1			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_065-070CM	FS	65.6	J	22.3			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_070-075CM	FS	41.1	J	17.8			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_075-080CM	FS	49	J	30.7			
1710917	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_080-085CM	FS	63.4	J	22.3			
1710918	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_00-01	FS	50.6	J	686			
1710918	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_01-03	FS	49.4	J	778			
1710918	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_03-05	FS	49.2	J	852			
1710918	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_05-07	FS	53.4	J	904			
1710918	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_07-10	FS	57.4	J	1,250			
1710918	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_10-15	FS	52.5	J	1,700			

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DATA VALIDATION SUMMARY
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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
					Final	Final	Final	Final	Final	Final		
					Result	Qualifier	Result	Qualifier	Result	Qualifier		
1711046	PBR-20-G	10/23/2017	PBR-20-G-17_SED_00-01	FS	55.2	J	380					
1711046	PBR-20-G	10/23/2017	PBR-20-G-17_SED_01-03	FS	60.1	J	353					
1711046	PBR-20-G	10/23/2017	PBR-20-G-17_SED_03-05	FS	56.9	J	509					
1711047	UPB-MU11-GC-1-E	10/23/2017	UPB-MU11-GC-1-E-17_SED_00-01	FS	31.2	J	684					
1711047	UPB-MU11-GC-1-E	10/23/2017	UPB-MU11-GC-1-E-17_SED_01-03	FS	44.6	J	636					
1711047	UPB-MU11-GC-1-E	10/23/2017	UPB-MU11-GC-1-E-17_SED_03-05	FS	40.8	J	664					
1711047	UPB-MU11-GC-1-E	10/23/2017	UPB-MU11-GC-1-E-17_SED_05-07	FS	44.6	J	647					
1711047	UPB-MU11-GC-1-E	10/23/2017	UPB-MU11-GC-1-E-17_SED_07-10	FS	44	J	834					
1711047	UPB-MU11-GC-1-E	10/23/2017	UPB-MU11-GC-1-E-17_SED_07-10_DUP	FD	46.5	J	602					
1711050	VE-MU4-GC-1-F	10/19/2017	VE-MU4-GC-1-F-17_SED_00-01	FS	34.9	J	648					
1711050	VE-MU4-GC-1-F	10/19/2017	VE-MU4-GC-1-F-17_SED_01-03	FS	51	J	496					
1711050	VE-MU4-GC-1-F	10/19/2017	VE-MU4-GC-1-F-17_SED_03-05	FS	69.9	J	859	J				
1711050	VE-MU4-GC-1-F	10/19/2017	VE-MU4-GC-1-F-17_SED_03-05_DUP	FD	64.8	J	309	J				
1711056	OR-T3-C5-E	10/24/2017	OR-T3-C5-E-17_SED_00-01	FS	38.3	J	774					
1711056	OR-T3-C5-E	10/24/2017	OR-T3-C5-E-17_SED_01-03	FS	44.2	J	701					
1711056	OR-T3-C5-E	10/24/2017	OR-T3-C5-E-17_SED_03-05	FS	42.4	J	852					
1711056	OR-T3-C5-E	10/24/2017	OR-T3-C5-E-17_SED_05-07	FS	41.8	J	963					
1711056	OR-T3-C5-E	10/24/2017	OR-T3-C5-E-17_SED_07-10	FS	41.5	J	1,210					
1711057	OR-T3-C4-F	10/23/2017	OR-T3-C4-F-17_SED_00-01	FS	49.8	J	898					
1711057	OR-T3-C4-F	10/23/2017	OR-T3-C4-F-17_SED_01-03	FS	41	J	935					
1711057	OR-T3-C4-F	10/23/2017	OR-T3-C4-F-17_SED_03-05	FS	45	J	427					
1711057	OR-T3-C4-F	10/23/2017	OR-T3-C4-F-17_SED_03-05_DUP	FD	47.4	J	361					
1711057	OR-T3-C4-F	10/23/2017	OR-T3-C4-F-17_SED_05-07	FS	50.7	J	132					
1711057	OR-T3-C4-F	10/23/2017	OR-T3-C4-F-17_SED_07-10	FS	51.1	J	228					
1711058	OR-T3-C2-F	10/23/2017	OR-T3-C2-F-17_SED_00-01	FS	35.4	J	964					
1711058	OR-T3-C2-F	10/23/2017	OR-T3-C2-F-17_SED_01-03	FS	37.9	J	1,020					

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1711058	OR-T3-C2-F	10/23/2017	OR-T3-C2-F-17_SED_03-05	FS	36.9	J	1,200			
1711058	OR-T3-C2-F	10/23/2017	OR-T3-C2-F-17_SED_03-05_DUP	FD	38.6	J	1,270			
1711058	OR-T3-C2-F	10/23/2017	OR-T3-C2-F-17_SED_05-07	FS	39.2	J	1,630			
1711059	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_00-01	FS	35.5	J	567			
1711059	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_01-03	FS	35.2	J	564			
1711059	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_03-05	FS	35.7	J	858			
1711059	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_05-07	FS	36.4	J	931			
1711059	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_07-10	FS	38.1	J	1,180			
1711059	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_10-15	FS	26.8	J	1,010			
1711059	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_15-20	FS	30.4	J	318			
1711059	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_15-20_DUP	FD	31.4	J	289			
1711060	OR-T2-C5-E	10/24/2017	OR-T2-C5-E-17_SED_00-01	FS	37.6	J	725			
1711060	OR-T2-C5-E	10/24/2017	OR-T2-C5-E-17_SED_01-03	FS	36.2	J	826			
1711060	OR-T2-C5-E	10/24/2017	OR-T2-C5-E-17_SED_03-05	FS	44.5	J	902			
1711060	OR-T2-C5-E	10/24/2017	OR-T2-C5-E-17_SED_05-07	FS	44.8	J	801			
1711060	OR-T2-C5-E	10/24/2017	OR-T2-C5-E-17_SED_07-10	FS	44.7	J	1,100			
1711061	OR-T2-C4-C	10/23/2017	OR-T2-C4-C-17_SED_00-01	FS	18	J	1,730			
1711061	OR-T2-C4-C	10/23/2017	OR-T2-C4-C-17_SED_01-03	FS	40.7	J	830			
1711061	OR-T2-C4-C	10/23/2017	OR-T2-C4-C-17_SED_03-05	FS	40.5	J	962			
1711061	OR-T2-C4-C	10/23/2017	OR-T2-C4-C-17_SED_05-07	FS	44.9	J	1,220			
1711061	OR-T2-C4-C	10/23/2017	OR-T2-C4-C-17_SED_07-10	FS	35.9	J	1,150			
1711062	PBR-18-I	10/20/2017	PBR-18-I-17_SED_00-01	FS	36.9	J	698			
1711062	PBR-18-I	10/20/2017	PBR-18-I-17_SED_01-03	FS	36.8	J	763			
1711062	PBR-18-I	10/20/2017	PBR-18-I-17_SED_03-05	FS	37.1	J	852			
1711062	PBR-18-I	10/20/2017	PBR-18-I-17_SED_05-07	FS	40.1	J	854			
1711063	OR-T2-C3-C	10/20/2017	OR-T2-C3-C-17_SED_00-01	FS	42.3	J	792			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1711063	OR-T2-C3-C	10/20/2017	OR-T2-C3-C-17_SED_01-03	FS	47.9	J	245			
1711063	OR-T2-C3-C	10/20/2017	OR-T2-C3-C-17_SED_03-05	FS	50.6	J	79.8			
1711063	OR-T2-C3-C	10/20/2017	OR-T2-C3-C-17_SED_05-07	FS	48.5	J	80.2			
1711063	OR-T2-C3-C	10/20/2017	OR-T2-C3-C-17_SED_07-10	FS	47.4	J	82.9			
1711063	OR-T2-C3-C	10/20/2017	OR-T2-C3-C-17_SED_07-10_DUP	FD	42.8	J	79.7			
1711064	OR-T2-C2-E	10/20/2017	OR-T2-C2-E-17_SED_00-01	FS	33.3	J	767			
1711064	OR-T2-C2-E	10/20/2017	OR-T2-C2-E-17_SED_01-03	FS	38.6	J	840			
1711064	OR-T2-C2-E	10/20/2017	OR-T2-C2-E-17_SED_03-05	FS	38.8	J	996			
1711064	OR-T2-C2-E	10/20/2017	OR-T2-C2-E-17_SED_05-07	FS	48.4	J	996			
1711064	OR-T2-C2-E	10/20/2017	OR-T2-C2-E-17_SED_07-10	FS	46.9	J	956			
1711065	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_00-01	FS	40.3	J	836			
1711065	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_01-03	FS	41.7	J	1,560			
1711065	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_03-05	FS	43	J	1,460			
1711065	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_05-07	FS	42	J	361			
1711065	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_05-07_DUP	FD	42.6	J	360			
1711065	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_07-10	FS	48.1	J	269			
1711065	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_10-15	FS	59.3	J	160			
1711065	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_15-20	FS	66.2	J	40.3			
1711066	OR-T1-C5-C	10/23/2017	OR-T1-C5-C-17_SED_00-01	FS	32.2	J	571			
1711066	OR-T1-C5-C	10/23/2017	OR-T1-C5-C-17_SED_01-03	FS	47.2	J	644			
1711066	OR-T1-C5-C	10/23/2017	OR-T1-C5-C-17_SED_01-03_DUP	FD	49.1	J	785			
1711066	OR-T1-C5-C	10/23/2017	OR-T1-C5-C-17_SED_03-05	FS	46.5	J	682			
1711066	OR-T1-C5-C	10/23/2017	OR-T1-C5-C-17_SED_05-07	FS	47.5	J	830			
1711066	OR-T1-C5-C	10/23/2017	OR-T1-C5-C-17_SED_07-10	FS	47.8	J	913			
1711067	MM-T4-C2-F	10/24/2017	MM-T4-C2-F-17_SED_00-01	FS	45.1	J	635			
1711067	MM-T4-C2-F	10/24/2017	MM-T4-C2-F-17_SED_01-03	FS	42.6	J	693			

**TABLE 3
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SDG	Location ID	Sample Date	Sample ID	Analysis Method	% Solids		EPA 1631		LLOYD KAHN	
				Parameter	PERCENT		Mercury		TOC	
				Unit	Total		NG/G		PERCENT	
QC Code	Final	Final	Final	Final	Final	Final				
				Fraction	Result	Qualifier	Total	Qualifier	Total	Qualifier
1711067	MM-T4-C2-F	10/24/2017	MM-T4-C2-F-17_SED_01-03_DUP	FD	44.4	J	725			
1711067	MM-T4-C2-F	10/24/2017	MM-T4-C2-F-17_SED_03-05	FS	45.9	J	570			
1711067	MM-T4-C2-F	10/24/2017	MM-T4-C2-F-17_SED_05-07	FS	47.5	J	533			
1711067	MM-T4-C2-F	10/24/2017	MM-T4-C2-F-17_SED_07-10	FS	38.2	J	939			
1711068	OR-T1-C3-C	10/19/2017	OR-T1-C3-C-17_SED_00-01	FS	53.5	J	672			
1711068	OR-T1-C3-C	10/19/2017	OR-T1-C3-C-17_SED_01-03	FS	43.1	J	815			
1711068	OR-T1-C3-C	10/19/2017	OR-T1-C3-C-17_SED_03-05	FS	42.6	J	749			
1711068	OR-T1-C3-C	10/19/2017	OR-T1-C3-C-17_SED_05-07	FS	44.4	J	1,060			
1711069	OR-T1-C2-C	10/19/2017	OR-T1-C2-C-17_SED_00-01	FS	45	J	647			
1711069	OR-T1-C2-C	10/19/2017	OR-T1-C2-C-17_SED_01-03	FS	43.3	J	638			
1711069	OR-T1-C2-C	10/19/2017	OR-T1-C2-C-17_SED_03-05	FS	43.6	J	818			
1711069	OR-T1-C2-C	10/19/2017	OR-T1-C2-C-17_SED_05-07	FS	45.9	J	867			
1711069	OR-T1-C2-C	10/19/2017	OR-T1-C2-C-17_SED_07-10	FS	41.1	J	1,110			
1711070	MM-T3-C4-C	10/24/2017	MM-T3-C4-C-17_SED_00-01	FS	38.6	J	728			
1711070	MM-T3-C4-C	10/24/2017	MM-T3-C4-C-17_SED_01-03	FS	47.3	J	840			
1711070	MM-T3-C4-C	10/24/2017	MM-T3-C4-C-17_SED_03-05	FS	38.4	J	964			
1711070	MM-T3-C4-C	10/24/2017	MM-T3-C4-C-17_SED_05-07	FS	46.8	J	781			
1711070	MM-T3-C4-C	10/24/2017	MM-T3-C4-C-17_SED_07-10	FS	46.8	J	770			
1711071	MM-T1-C2-D	10/20/2017	MM-T1-C2-D-17_SED_00-01	FS	43.1	J	783			
1711071	MM-T1-C2-D	10/20/2017	MM-T1-C2-D-17_SED_01-03	FS	38.4	J	778			
1711071	MM-T1-C2-D	10/20/2017	MM-T1-C2-D-17_SED_03-05	FS	43.8	J	812			
1711071	MM-T1-C2-D	10/20/2017	MM-T1-C2-D-17_SED_05-07	FS	39.4	J	919			
1711071	MM-T1-C2-D	10/20/2017	MM-T1-C2-D-17_SED_05-07_DUP	FD	39.2	J	848			
1711071	MM-T1-C2-D	10/20/2017	MM-T1-C2-D-17_SED_07-10	FS	44.9	J	227			
1711073	ES-01-F	10/20/2017	ES-01-F-17_SED_00-01	FS	45.2	J	512			
1711073	ES-01-F	10/20/2017	ES-01-F-17_SED_01-03	FS	37.8	J	699			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1711073	ES-01-F	10/20/2017	ES-01-F-17_SED_01-03_DUP	FD	44	J	600			
1711073	ES-01-F	10/20/2017	ES-01-F-17_SED_03-05	FS	35.2	J	632			
1711073	ES-01-F	10/20/2017	ES-01-F-17_SED_05-07	FS	35.6	J	637			
1711077	ES-18-F	10/23/2017	ES-18-F-17_SED_00-01	FS	61.6	J	298			
1711077	ES-18-F	10/23/2017	ES-18-F-17_SED_01-03	FS	56.6	J	780			
1711077	ES-18-F	10/23/2017	ES-18-F-17_SED_03-05	FS	59	J	857			
1711077	ES-18-F	10/23/2017	ES-18-F-17_SED_05-07	FS	57.2	J	648			
1711083	MM-T3-C2-F	10/20/2017	MM-T3-C2-F-17_SED_00-01	FS	38.3	J	647			
1711083	MM-T3-C2-F	10/20/2017	MM-T3-C2-F-17_SED_01-03	FS	39.8	J	823			
1711083	MM-T3-C2-F	10/20/2017	MM-T3-C2-F-17_SED_03-05	FS	30.7	J	966			
1711083	MM-T3-C2-F	10/20/2017	MM-T3-C2-F-17_SED_05-07	FS	29.2	J	1,010			
1711084	MM-T3-C3-C	10/19/2017	MM-T3-C3-C-17_SED_00-01	FS	81.1	J	60			
1711084	MM-T3-C3-C	10/19/2017	MM-T3-C3-C-17_SED_01-03	FS	61.9	J	359			
1711084	MM-T3-C3-C	10/19/2017	MM-T3-C3-C-17_SED_03-05	FS	55.4	J	436			
1711085	MM-T2-C8-B	10/24/2017	MM-T2-C8-B-17_SED_00-01	FS	25.1	J	206			
1711085	MM-T2-C8-B	10/24/2017	MM-T2-C8-B-17_SED_01-03	FS	24.9	J	325			
1711085	MM-T2-C8-B	10/24/2017	MM-T2-C8-B-17_SED_03-05	FS	30.8	J	1,180			
1711085	MM-T2-C8-B	10/24/2017	MM-T2-C8-B-17_SED_05-07	FS	25.6	J	625			
1711085	MM-T2-C8-B	10/24/2017	MM-T2-C8-B-17_SED_07-10	FS	23	J	201			
1711151	PBR-28	11/1/2017	PBR-28-17_SED_00-01	FS	39.5	J	608			
1711151	PBR-28	11/1/2017	PBR-28-17_SED_01-03	FS	45.4	J	631			
1711151	PBR-28	11/1/2017	PBR-28-17_SED_03-05	FS	43.3	J	897			
1711151	PBR-28	11/1/2017	PBR-28-17_SED_05-07	FS	47.3	J	900			
1711151	PBR-28	11/1/2017	PBR-28-17_SED_05-07_DUP	FD	46.8	J	824			
1711151	PBR-28	11/1/2017	PBR-28-17_SED_07-10	FS	54.5	J	115			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_000-001CM	FS	45.5	J	33.3			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_001-002CM	FS	49	J	36.1			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_002-003CM	FS	47.2	J	34.9			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_003-004CM	FS	47	J	42.3			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_004-005CM	FS	46.2	J	51.3			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_005-006CM	FS	47.8	J	54.8			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_006-007CM	FS	49.1	J	59			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_007-008CM	FS	49.3	J	68			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_008-009CM	FS	49	J	81.8			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_009-010CM	FS	46.3	J	62.9			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_010-011CM	FS	41.7	J	127			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_011-012CM	FS	40.2	J	133			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_012-013CM	FS	43.7	J	87			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_013-014CM	FS	42	J	128			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_014-015CM	FS	43	J	132			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_015-016CM	FS	44.4	J	147			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_016-017CM	FS	41.9	J	153			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_017-018CM	FS	39.8	J	172			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_018-019CM	FS	36.8	J	210			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_019-020CM	FS	38.8	J	201			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_020-022CM	FS	39.5	J	230			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_022-024CM	FS	39.9	J	243			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_024-026CM	FS	37.3	J	258			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_026-028CM	FS	38	J	240			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_028-030CM	FS	38.5	J	270			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_030-032CM	FS	40.9	J	306			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_032-034CM	FS	38.7	J	601			

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_034-036CM	FS	34.9	J	1,980			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_036-038CM	FS	34.4	J	2,350			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_038-040CM	FS	40.7	J	2,810			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_040-045CM	FS	39.2	J	2,400			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_045-050CM	FS	42.4	J	910			
1711156	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_050-055CM	FS	40.7	J	386			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_000-001CM	FS	46.5	J	621			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_001-002CM	FS	48	J	584			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_002-003CM	FS	48.6	J	654			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_003-004CM	FS	48.5	J	684			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_004-005CM	FS	46	J	1,060			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_005-006CM	FS	41.7	J	1,020			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_006-007CM	FS	39.7	J	1,100			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_007-008CM	FS	39.1	J	1,220			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_008-009CM	FS	39.2	J	799			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_009-010CM	FS	35.7	J	731			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_010-011CM	FS	35.6	J	630			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_011-012CM	FS	34.2	J	578			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_012-013CM	FS	35.2	J	442			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_013-014CM	FS	34.2	J	364			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_014-015CM	FS	37	J	297			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_015-016CM	FS	37.7	J	281			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_016-017CM	FS	38.2	J	297			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_017-018CM	FS	39.3	J	314			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_018-019CM	FS	38.2	J	314			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_019-020CM	FS	39.4	J	306			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_020-022CM	FS	40.9	J	325			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_022-024CM	FS	41.7	J	285			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_024-026CM	FS	41.7	J	310			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_026-028CM	FS	41.8	J	285			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_028-030CM	FS	42	J	289			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_030-032CM	FS	41.8	J	277			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_032-034CM	FS	42.2	J	292			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_034-036CM	FS	40.6	J	335			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_036-038CM	FS	44.3	J	326			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_038-040CM	FS	44	J	308			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_040-045CM	FS	44.1	J	291			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_045-050CM	FS	45.1	J	259			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_050-055CM	FS	47	J	238			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_055-060CM	FS	47.8	J	262			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_060-065CM	FS	48.8	J	182			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_065-070CM	FS	49.8	J	160			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_070-075CM	FS	53.7	J	118			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_075-080CM	FS	54.6	J	96.7			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_080-085CM	FS	54.2	J	77.3			
1711171	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_085-090CM	FS	54.5	J	80.2			
1711173	OR-T1-C1-D	11/1/2017	OR-T1-C1-D-17_SED_00-01	FS	46.9	J	351			
1711173	OR-T1-C1-D	11/1/2017	OR-T1-C1-D-17_SED_01-03	FS	37.2	J	589			
1711173	OR-T1-C1-D	11/1/2017	OR-T1-C1-D-17_SED_03-05	FS	42.2	J	762			
1711173	OR-T1-C1-D	11/1/2017	OR-T1-C1-D-17_SED_05-07	FS	43.1	J	946			
1711173	OR-T1-C1-D	11/1/2017	OR-T1-C1-D-17_SED_07-10	FS	42.5	J	1,420			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_000-001CM	FS	44.7	J	363			

**TABLE 3
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_000-001CM_DUP	FD	43.4	J	367			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_001-002CM	FS	43.8	J	293			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_001-002CM_DUP	FD	46.1	J	283			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_002-003CM	FS	57.1	J	182			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_003-004CM	FS	61.6	J	99.8			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_003-004CM_DUP	FD	61.7	J	94.8			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_004-005CM	FS	68.7	J	52.8			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_004-005CM_DUP	FD	67.6	J	61.2			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_005-006CM	FS	75.1	J	26.3			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_005-006CM_DUP	FD	76	J	22.4			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_006-007CM	FS	80.7	J	5.03			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_006-007CM_DUP	FD	80.8	J	5.14			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_007-008CM	FS	80.7	J	4.64			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_007-008CM_DUP	FD	81.3	J	3.97	J		
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_008-009CM	FS	81.2	J	8.51			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_008-009CM_DUP	FD	81.5	J	8.33			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_009-010CM	FS	81.9	J	5.18			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_009-010CM_DUP	FD	82.2	J	6.45			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_010-011CM	FS	77.3	J	7.93			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_010-011CM_DUP	FD	77.7	J	7.38			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_011-012CM	FS	76.5	J	5.48			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_011-012CM_DUP	FD	77.1	J	5.14			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_012-013CM	FS	76	J	10.9			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_012-013CM_DUP	FD	75.8	J	9.79			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_013-014CM	FS	75.9	J	9.75			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_013-014CM_DUP	FD	76.7	J	8.33			

**TABLE 3
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method Parameter Unit Fraction		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_014-015CM	FS	79	J	8.14			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_014-015CM_DUP	FD	78.3	J	7.57			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_015-016CM	FS	79.9	J	8.73	J		
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_015-016CM_DUP	FD	79.3	J	7.58	J		
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_016-017CM	FS	76.3	J	12			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_016-017CM_DUP	FD	77.2	J	10.8			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_017-018CM	FS	78.5	J	6.89			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_017-018CM_DUP	FD	79	J	6.55			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_018-019CM	FS	80.4	J	7.7			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_018-019CM_DUP	FD	79.8	J	8.42			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_019-020CM	FS	79.9	J	6.4			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_019-020CM_DUP	FD	80.3	J	6.18			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_020-022CM	FS	79.4	J	5.38			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_020-022CM_DUP	FD	79.4	J	5.83			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_022-024CM	FS	80.1	J	7.76			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_022-024CM_DUP	FD	79.6	J	8.41			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_024-026CM	FS	81.9	J	8.5			
1711174	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_024-026CM_DUP	FD	81.6	J	9.38			
1711328	MM-T1-C1-B	11/1/2017	MM-T1-C1-B-17_SED_00-01	FS	41.1	J	759			
1711328	MM-T1-C1-B	11/1/2017	MM-T1-C1-B-17_SED_01-03	FS	34.2	J	827			
1711328	MM-T1-C1-B	11/1/2017	MM-T1-C1-B-17_SED_03-05	FS	37.7	J	706			
1711328	MM-T1-C1-B	11/1/2017	MM-T1-C1-B-17_SED_03-05-Dup	FD	36.3	J	772			
1711328	MM-T1-C1-B	11/1/2017	MM-T1-C1-B-17_SED_05-07	FS	37.5	J	748			
1711328	MM-T1-C1-B	11/1/2017	MM-T1-C1-B-17_SED_07-10	FS	44.9	J	491			
1712044	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_022-024CM	FS	43.4	J	860			
1712044	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_022-024CM_DUP	FD	43.3	J	854			

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
					Final	Final	Final	Final	Final	Final		
					Result	Qualifier	Result	Qualifier	Result	Qualifier		
1712045	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_045-050CM	FS	70.8	J	10.6					
1712045	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_045-050CM_DUP	FD	70.9	J	10.6					
1712045	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_055-060CM	FS	76.4	J	10.2					
1712045	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_055-060CM_DUP	FD	76.3	J	9.09					
1712047	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_050-055CM	FS	67.5	J	18.1					
L1732774	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_000-001CM	FS	49.7					6.255		
L1732774	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_001-002CM	FS	57.2					3.23		
L1732774	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_002-003CM	FS	52.6					3.855		
L1732774	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_003-004CM	FS	50					5.415		
L1732774	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_004-005CM	FS	43.9					5.785		
L1732774	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_005-006CM	FS	41.3					6.27		
L1732774	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_006-007CM	FS	42.8					6.58		
L1732774	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_007-008CM	FS	45.2					5.195		
L1732774	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_008-009CM	FS	49.3					5.59		
L1732774	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_009-010CM	FS	46.3					8.595		
L1732774	MM-T3-C2-C	9/12/2017	MM-T3-C2-C-17_SED_010-011CM	FS	49.2					5.74		
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_011-012CM	FS	41.9					7.155		
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_012-013CM	FS	41.5					6.475		
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_013-014CM	FS	52.1					5.225		
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_014-015CM	FS	59.8					2.275		
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_015-016CM	FS	52.2					3.815		
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_016-017CM	FS	38.2					7.655		
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_017-018CM	FS	49.1					2.185		
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_018-019CM	FS	80.4					1.127		
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_019-020CM	FS	82.1					0.2275		
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_020-022CM	FS	86.3					0.1245		

**TABLE 3
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_022-024CM	FS	82.4				0.1415	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_024-026CM	FS	80.7				0.124	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_026-028CM	FS	80.2				0.1565	J
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_028-030CM	FS	77.8				0.143	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_030-032CM	FS	79.3				0.1555	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_032-034CM	FS	82.3				0.1005	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_034-036CM	FS	81.6				0.104	J
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_036-038CM	FS	81.9				0.0825	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_038-040CM	FS	80.9				0.092	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_040-045CM	FS	82.3				0.087	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_045-050CM	FS	82.1				0.082	J
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_050-055CM	FS	82.9				0.1035	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_055-060CM	FS	81.7				0.1025	J
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_060-065CM	FS	82.2				0.074	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_065-070CM	FS	81.9				0.067	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_070-075CM	FS	82.1				0.0655	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_075-080CM	FS	81.2				0.1	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_080-085CM	FS	79.6				0.058	
L1732774	MM-T3-C2-C	9/13/2017	MM-T3-C2-C-17_SED_085-090CM	FS	81.8				0.094	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_000-001CM	FS	49.6				3.51	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_001-002CM	FS	50				3.345	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_002-003CM	FS	49.1				3.35	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_003-004CM	FS	47.5				3.06	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_004-005CM	FS	51.9				3.275	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_005-006CM	FS	52				2.965	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_006-007CM	FS	55				2.415	

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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_007-008CM	FS	56.9				2.56	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_008-009CM	FS	56.3				2.575	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_009-010CM	FS	61				2.515	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_010-011CM	FS	56.4				2.655	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_011-012CM	FS	59.4				2.12	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_012-013CM	FS	56.7				2.185	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_013-014CM	FS	59.8				2.295	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_014-015CM	FS	62.8				1.97	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_015-016CM	FS	61.8				1.51	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_016-017CM	FS	63.1				1.7	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_017-018CM	FS	60				1.725	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_018-019CM	FS	61				2.05	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_019-020CM	FS	60.4				2.305	J
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_020-022CM	FS	60.2				1.98	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_022-024CM	FS	59				1.75	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_024-026CM	FS	61				1.83	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_026-028CM	FS	58				1.89	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_028-030CM	FS	57.1				2.365	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_030-032CM	FS	53.5				2.35	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_032-034CM	FS	55.9				2.605	J
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_034-036CM	FS	55.8				2.045	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_036-038CM	FS	56.3				2.15	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_038-040CM	FS	57.4				1.71	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_040-045CM	FS	62				1.75	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_045-050CM	FS	73				1.74	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_050-055CM	FS	56.4				1.97	

TABLE 3
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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_055-060CM	FS	56.9				2.04	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_060-065CM	FS	56				2.335	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_065-070CM	FS	56.4				2.01	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_070-075CM	FS	54.8				1.885	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_075-080CM	FS	54.9				1.87	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_080-085CM	FS	58				1.875	
L1733612	OR-T1-C4-C	9/14/2017	OR-T1-C4-C-17_SED_085-090CM	FS	53				2.08	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_000-001CM	FS	33.3	J			5.895	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_001-002CM	FS	43.2				5.06	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_002-003CM	FS	44.2				5.18	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_003-004CM	FS	50				4.04	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_004-005CM	FS	56.5				3.905	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_005-006CM	FS	65.1				2.93	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_006-007CM	FS	67.9				2.23	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_007-008CM	FS	81				1.295	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_008-009CM	FS	77.8				1.365	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_009-010CM	FS	81.6				0.9485	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_010-011CM	FS	81.8				0.3455	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_011-012CM	FS	77.3				0.822	
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_012-013CM	FS	89.1				0.1825	J
L1733618	MM-T1-C3-B	9/13/2017	MM-T1-C3-B-17_SED_013-014CM	FS	89.1				0.1365	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_014-015CM	FS	93.1				0.1145	J
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_015-016CM	FS	88.9				0.0995	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_016-017CM	FS	85.7				0.1255	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_017-018CM	FS	89.8				0.1185	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_018-019CM	FS	90.7				0.129	

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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_019-020CM	FS	86				0.1565	J
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_020-022CM	FS	90.6				0.132	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_022-024CM	FS	89.1				0.164	J
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_024-026CM	FS	91.4				0.2115	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_026-028CM	FS	86.7				0.1285	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_028-030CM	FS	90				0.1015	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_030-032CM	FS	86.2				0.144	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_032-034CM	FS	83.3				0.1425	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_034-036CM	FS	88.2				0.1715	J
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_036-038CM	FS	85.2				0.1275	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_038-040CM	FS	86.5				0.119	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_040-045CM	FS	69.2				0.149	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_045-050CM	FS	81.8				0.171	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_050-055CM	FS	48.8				0.1925	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_055-060CM	FS	100				0.103	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_060-065CM	FS	82.4				0.1265	J
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_065-070CM	FS	83.6				0.1035	
L1733618	MM-T1-C3-B	9/14/2017	MM-T1-C3-B-17_SED_070-075CM	FS	85.7				0.152	J
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_000-001CM	FS	47.2				4.91	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_001-002CM	FS	48				4.065	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_002-003CM	FS	44.6				7.285	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_003-004CM	FS	45				6.005	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_004-005CM	FS	48.2				4.96	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_005-006CM	FS	50.5				3.985	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_006-007CM	FS	55.6				3.095	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_007-008CM	FS	55.8				2.455	J

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_008-009CM	FS	57.9				2.525	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_009-010CM	FS	59.7				2.79	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_010-011CM	FS	60.4				2.035	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_011-012CM	FS	62.5				2.32	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_012-013CM	FS	66.3				1.63	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_013-014CM	FS	67				1.84	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_014-015CM	FS	69.4				1.395	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_015-016CM	FS	72.7				1.155	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_016-017CM	FS	74.9				1.115	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_017-018CM	FS	75.2				1.15	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_018-019CM	FS	72.8				1.125	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_019-020CM	FS	73.3				1.0735	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_020-022CM	FS	80.3				0.603	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_022-024CM	FS	84.2				0.7385	J
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_024-026CM	FS	87				0.3405	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_026-028CM	FS	87.1				0.356	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_028-030CM	FS	87.2				0.3235	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_030-032CM	FS	87.1				0.282	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_032-034CM	FS	82.3				0.324	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_034-036CM	FS	79.5				0.7015	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_036-038CM	FS	81.6				0.719	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_038-040CM	FS	83				0.532	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_040-045CM	FS	83.1				0.411	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_045-050CM	FS	81.4				0.439	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_050-055CM	FS	83.7				0.379	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_055-060CM	FS	81.9				0.473	

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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_060-065CM	FS	78.6				0.426	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_065-070CM	FS	82.2				0.4575	J
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_070-075CM	FS	81				0.8045	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_075-080CM	FS	80				0.572	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_080-085CM	FS	81.7				0.3735	
L1733619	MM-T2-C4-B	9/15/2017	MM-T2-C4-B-17_SED_085-090CM	FS	78.6				0.638	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_000-001CM	FS	42.4				5.13	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_001-002CM	FS	37.1				7.82	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_002-003CM	FS	37.9				5.325	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_003-004CM	FS	47.2				3.855	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_004-005CM	FS	43.3				3.67	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_005-006CM	FS	51.6				3.04	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_006-007CM	FS	52.8				3.71	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_007-008CM	FS	50				2.67	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_008-009CM	FS	56.5				2.89	J
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_009-010CM	FS	52.6				2.8	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_010-011CM	FS	56.2				2.595	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_011-012CM	FS	59.1				2.645	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_012-013CM	FS	58.3				1.8	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_013-014CM	FS	56				6.045	J
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_014-015CM	FS	60.8				1.735	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_015-016CM	FS	61				1.515	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_016-017CM	FS	65.9				1.975	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_017-018CM	FS	62.9				1.735	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_018-019CM	FS	65.5				1.3	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_019-020CM	FS	68.5				1.135	

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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_020-022CM	FS	69				1.16	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_022-024CM	FS	67.7				1.17	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_024-026CM	FS	63.9				1.805	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_026-028CM	FS	64.4				1.61	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_028-030CM	FS	67				1.395	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_030-032CM	FS	62.9				1.56	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_032-034CM	FS	63.5				1.355	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_034-036CM	FS	64				1.46	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_036-038CM	FS	64.2				1.435	J
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_038-040CM	FS	77.1				1.47	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_040-045CM	FS	62.1				1.62	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_045-050CM	FS	63.4				1.655	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_050-055CM	FS	65.4				1.28	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_055-060CM	FS	67.8				1.265	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_060-065CM	FS	66.1				1.445	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_065-070CM	FS	67.6				1.555	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_070-075CM	FS	62.2				1.89	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_075-080CM	FS	68.8				2.275	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_080-085CM	FS	64.3				2.15	
L1733620	MM-T2-C5-A	9/15/2017	MM-T2-C5-A-17_SED_085-090CM	FS	62.1				2.04	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_000-001CM	FS	46.8	J			6.405	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_001-002CM	FS	42.9				4.735	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_002-003CM	FS	40				4.78	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_003-004CM	FS	39.2				5.915	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_004-005CM	FS	34.4				6.085	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_005-006CM	FS	34.2				5.79	

**TABLE 3
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_006-007CM	FS	38.9				5.875	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_007-008CM	FS	56.2				5.92	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_008-009CM	FS	34.2				6.385	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_009-010CM	FS	44				5.77	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_010-011CM	FS	42.6				4.78	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_011-012CM	FS	40.4				5.96	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_012-013CM	FS	39.5				5.84	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_013-014CM	FS	45.8				5.705	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_014-015CM	FS	47.2				4.735	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_015-016CM	FS	34.8				5.09	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_016-017CM	FS	38.1				5.145	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_017-018CM	FS	43.3				5.1	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_018-019CM	FS	37.9				4.26	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_019-020CM	FS	34.6				5.565	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_020-022CM	FS	39.5				4.86	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_022-024CM	FS	34.8				6	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_024-026CM	FS	43.8				4.205	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_026-028CM	FS	38.3				4.685	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_028-030CM	FS	47.9				3.965	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_030-032CM	FS	43.8				4.52	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_032-034CM	FS	37.9				5.585	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_034-036CM	FS	45.4				5.685	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_036-038CM	FS	38.6				5.42	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_038-040CM	FS	39.2				5.33	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_040-045CM	FS	43.8				5.355	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_045-050CM	FS	45.9				4.75	

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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_050-055CM	FS	56.9				4.155	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_055-060CM	FS	45.4				7.34	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_060-065CM	FS	46.3				6.695	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_065-070CM	FS	43.8				8.39	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_070-075CM	FS	56.2				4.39	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_075-080CM	FS	44.4				6.71	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_080-085CM	FS	50				4.265	
L1733621	MM-T2-C6-A	9/18/2017	MM-T2-C6-A-17_SED_085-090CM	FS	62.9				1.975	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_000-001CM	FS	30				6.38	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_001-002CM	FS	29.1				6.745	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_002-003CM	FS	31.8				7.925	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_003-004CM	FS	35.5				6.62	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_004-005CM	FS	32.4				6.825	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_005-006CM	FS	32				6.395	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_006-007CM	FS	39.5				6.455	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_007-008CM	FS	41.5				6.2	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_008-009CM	FS	34.4				6.61	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_009-010CM	FS	40.6				7.355	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_010-011CM	FS	33.9				7.46	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_011-012CM	FS	38				6.86	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_012-013CM	FS	33.3				7.75	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_013-014CM	FS	36.4				7.62	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_014-015CM	FS	38.2				7.185	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_015-016CM	FS	36.4				6.465	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_016-017CM	FS	36.4				6.32	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_017-018CM	FS	35.4				7.345	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_018-019CM	FS	38.2				7.36	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_019-020CM	FS	34.6				7.505	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_020-022CM	FS	39.6				7.045	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_022-024CM	FS	42				6.92	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_024-026CM	FS	39.4				6.915	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_026-028CM	FS	43.1				6.785	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_028-030CM	FS	44.8				7.42	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_030-032CM	FS	47.7				7.08	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_032-034CM	FS	46.8				6.455	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_034-036CM	FS	48.6				6.635	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_036-038CM	FS	55.9				3.075	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_038-040CM	FS	55.2				3.72	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_040-045CM	FS	60.8				2.915	J
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_045-050CM	FS	61.8				3.08	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_050-055CM	FS	58.7				2.84	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_055-060CM	FS	59.3				2.785	
L1736451	MM-T1-C2-B	10/3/2017	MM-T1-C2-B-17_SED_060-065CM	FS	61.4				2.835	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_000-001CM	FS	35	J			4.475	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_001-002CM	FS	39.2				4.925	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_002-003CM	FS	43.3				4.57	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_003-004CM	FS	40.3				4.925	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_004-005CM	FS	37.3				4.625	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_005-006CM	FS	40.4				4.86	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_006-007CM	FS	34.3				5.175	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_007-008CM	FS	37.1				5.33	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_008-009CM	FS	38.5				5.12	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_009-010CM	FS	29.4				4.82	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_010-011CM	FS	40.8				4.765	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_011-012CM	FS	46.2				5.185	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_012-013CM	FS	39.7				4.925	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_013-014CM	FS	41.5				4.875	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_014-015CM	FS	40				4.905	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_015-016CM	FS	40				5.235	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_016-017CM	FS	24.5				5.61	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_017-018CM	FS	26.8				5.595	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_018-019CM	FS	43.9				5.245	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_019-020CM	FS	12.6				6.305	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_020-022CM	FS	44.7				6.05	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_022-024CM	FS	42.9				5.03	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_024-026CM	FS	41				5.79	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_026-028CM	FS	40.7				5.51	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_028-030CM	FS	43.6				5.51	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_030-032CM	FS	40				5.885	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_032-034CM	FS	41.8				6.03	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_034-036CM	FS	40.6				5.275	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_036-038CM	FS	16.2				6.41	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_038-040CM	FS	40.5				6.25	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_040-045CM	FS	36.1				7.84	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_045-050CM	FS	34.9				8.1	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_050-055CM	FS	36.8				7.57	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_055-060CM	FS	37.5				5.885	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_060-065CM	FS	8.51				6.8	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_065-070CM	FS	40				8.485	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_070-075CM	FS	41.7				7.55	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_075-080CM	FS	39.4				5.745	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_080-085CM	FS	67.2				2.15	
L1736453	OR-T1-C2-B	9/28/2017	OR-T1-C2-B-17_SED_085-090CM	FS	63.9				2.215	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_000-001CM	FS	38.9				4.315	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_001-002CM	FS	41.7				4.975	J
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_002-003CM	FS	40				4.025	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_003-004CM	FS	2.12				7.6	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_004-005CM	FS	49.4				4.495	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_005-006CM	FS	39.4				3.77	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_006-007CM	FS	39.6				4.96	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_007-008CM	FS	39.7				5.48	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_008-009CM	FS	38.4				6.01	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_009-010CM	FS	37.4				4.75	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_010-011CM	FS	14.9				5.04	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_011-012CM	FS	49				4.34	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_012-013CM	FS	50				3.485	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_013-014CM	FS	46.2				3.44	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_014-015CM	FS	50				3.275	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_015-016CM	FS	49.1				5.015	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_016-017CM	FS	48				4.695	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_017-018CM	FS	44.4				4.355	J
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_018-019CM	FS	45.6				4.265	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_019-020CM	FS	43.2				5.77	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_020-022CM	FS	41.3				7.37	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_022-024CM	FS	45.2				4.98	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_024-026CM	FS	46.7				4.485	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_026-028CM	FS	24.8				5.965	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_028-030CM	FS	73.4				3.8	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_030-032CM	FS	46.4				5.965	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_032-034CM	FS	48.6				5.385	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_034-036CM	FS	47.6				6.525	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_036-038CM	FS	46.8				5.04	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_038-040CM	FS	40.9				5.295	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_040-045CM	FS	38.6				4.42	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_045-050CM	FS	51				3.17	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_050-055CM	FS	48				4.75	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_055-060CM	FS	40				4.355	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_060-065CM	FS	7.78				6.805	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_065-070CM	FS	30.8				5.645	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_070-075CM	FS	46.2				4.505	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_075-080CM	FS	48.1				8.29	J
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_080-085CM	FS	26.1				8.565	
L1736454	OR-T1-C5-A	9/29/2017	OR-T1-C5-A-17_SED_085-090CM	FS	41.5				5.42	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_000-001CM	FS	40.7	J			7.67	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_001-002CM	FS	36.5				6.885	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_002-003CM	FS	37.5				7.31	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_003-004CM	FS	35.9				6.68	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_004-005CM	FS	38.2				6.635	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_005-006CM	FS	31.7				6.385	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_006-007CM	FS	40.5				6.02	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_007-008CM	FS	42				5.875	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_008-009CM	FS	40.5				6.155	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_009-010CM	FS	43.4				6.125	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_010-011CM	FS	5.88				7.27	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_011-012CM	FS	44.4				6.69	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_012-013CM	FS	45.8				6.58	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_013-014CM	FS	42				8.12	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_014-015CM	FS	27.1				7.965	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_015-016CM	FS	19.2				8.515	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_016-017CM	FS	43.8				7.27	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_017-018CM	FS	42.1				8.32	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_018-019CM	FS	19				8.285	J
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_019-020CM	FS	40				7.475	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_020-022CM	FS	36.4				9.15	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_022-024CM	FS	36.4				7.61	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_024-026CM	FS	41.7				9.02	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_026-028CM	FS	43.3				7.12	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_028-030CM	FS	44.7				7.125	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_030-032CM	FS	46.9				5.64	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_032-034CM	FS	47.8				6.14	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_034-036CM	FS	19.4				5.22	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_036-038CM	FS	48				6.265	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_038-040CM	FS	52.5				5.075	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_040-045CM	FS	59.4				4.11	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_045-050CM	FS	68.8				2.23	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_050-055CM	FS	65.8				1.945	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total	Final	Final	Total	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_055-060CM	FS	71.9				2.07	
L1736455	OR-T2-C1-C	9/29/2017	OR-T2-C1-C-17_SED_060-065CM	FS	67.3				2.125	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_000-001CM	FS	18.6	J			6.39	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_001-002CM	FS	46.8				4.92	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_002-003CM	FS	43.8				5.495	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_003-004CM	FS	51.8				4.905	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_004-005CM	FS	46.4				4.695	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_005-006CM	FS	22.8				6.85	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_006-007CM	FS	42.6				6.235	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_007-008CM	FS	40.7				7.305	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_008-009CM	FS	15				7.035	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_009-010CM	FS	38.6				7.505	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_010-011CM	FS	43.9				6.05	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_011-012CM	FS	42.4				6.075	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_012-013CM	FS	41.1				6.85	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_013-014CM	FS	37.5				5.485	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_014-015CM	FS	45.6				4.895	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_015-016CM	FS	37.1				5.53	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_016-017CM	FS	43.4				5.91	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_017-018CM	FS	44.2				5.025	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_018-019CM	FS	40.4				6.185	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_019-020CM	FS	42.4				7.65	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_020-022CM	FS	40.6				8.185	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_022-024CM	FS	40.6				6.32	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_024-026CM	FS	41.5				9.58	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_026-028CM	FS	37.2				9.33	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_028-030CM	FS	37.8				9.34	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_030-032CM	FS	40.6				6.23	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_032-034CM	FS	41				6.175	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_034-036CM	FS	40				9.635	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_036-038CM	FS	36.8				9.11	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_038-040CM	FS	31.2				8.015	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_040-045CM	FS	42.9				6.735	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_045-050CM	FS	39.2				6.18	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_050-055CM	FS	23				10.37	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_055-060CM	FS	34.9				8.02	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_060-065CM	FS	11.6				10.85	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_065-070CM	FS	18.2				7.845	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_070-075CM	FS	57.4				16.75	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_075-080CM	FS	27.3				9.025	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_080-085CM	FS	8.2				7.605	
L1736456	OR-T2-C4-A	10/3/2017	OR-T2-C4-A-17_SED_085-090CM	FS	7.79				9.42	
L1736458	OR-T3-C3-B	9/29/2017	OR-T3-C3-B-17_SED_000-001CM	FS	21.8				14.35	
L1736458	OR-T3-C3-B	9/29/2017	OR-T3-C3-B-17_SED_001-002CM	FS	24.7				13.4	
L1736458	OR-T3-C3-B	9/29/2017	OR-T3-C3-B-17_SED_002-003CM	FS	18.8				16.15	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_003-004CM	FS	25				15.15	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_004-005CM	FS	26.2				22.35	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_005-006CM	FS	32				10.9	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_006-007CM	FS	29.5				16.45	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_007-008CM	FS	26.5				12.55	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_008-009CM	FS	25.4				12.6	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_009-010CM	FS	24.1				15.4	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_010-011CM	FS	25.4				22.25	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_011-012CM	FS	17.6				25.45	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_012-013CM	FS	19.2				21.55	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_013-014CM	FS	19.5				20.85	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_014-015CM	FS	18.2				27.15	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_015-016CM	FS	14.2				27.55	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_016-017CM	FS	16.4				27.1	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_017-018CM	FS	18.6				21.65	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_018-019CM	FS	16.4				23.15	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_019-020CM	FS	17				23.05	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_020-022CM	FS	22	J			14	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_022-024CM	FS	28.7				9.94	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_024-026CM	FS	24.6				16.25	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_026-028CM	FS	12.9				9.99	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_028-030CM	FS	31.6				10.45	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_030-032CM	FS	36.2				6.755	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_032-034CM	FS	36.7				6.985	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_034-036CM	FS	30.4				9.695	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_036-038CM	FS	26.1				10.9	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_038-040CM	FS	29.7				11.75	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_040-045CM	FS	32.9				9.765	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_045-050CM	FS	48				4.085	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_050-055CM	FS	15.2				6.26	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_055-060CM	FS	40				7.59	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_060-065CM	FS	20.1				5.395	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_065-070CM	FS	29.1				10.05	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_070-075CM	FS	27.3				11.7	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_075-080CM	FS	30.6				11.55	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_080-085CM	FS	29.3				9.11	
L1736458	OR-T3-C3-B	10/2/2017	OR-T3-C3-B-17_SED_085-090CM	FS	38.5				8.585	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_000-001CM	FS	42.9				6.75	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_001-002CM	FS	41.4				6.675	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_002-003CM	FS	42.7				6.945	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_003-004CM	FS	41.8				6.875	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_004-005CM	FS	46.8				7.155	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_005-006CM	FS	37.7				7.21	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_006-007CM	FS	36.7				7.35	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_007-008CM	FS	39.7				7.28	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_008-009CM	FS	41				6.72	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_009-010CM	FS	45.2				7.435	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_010-011CM	FS	42.6				6.54	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_011-012CM	FS	33.1				6.295	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_012-013CM	FS	42.6				6.56	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_013-014CM	FS	45.7				6.705	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_014-015CM	FS	44.3				6.765	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_015-016CM	FS	42				6.845	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_016-017CM	FS	41.7				7.01	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_017-018CM	FS	39.8				6.95	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_018-019CM	FS	41				7.085	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_019-020CM	FS	41.7				7.105	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_020-022CM	FS	41.8				6.64	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_022-024CM	FS	43.2				6.68	

**TABLE 3
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_024-026CM	FS	46.8				6.3	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_026-028CM	FS	47.3				6.395	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_028-030CM	FS	43.1				6.725	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_030-032CM	FS	42.5				6.9	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_032-034CM	FS	30.5				7.045	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_034-036CM	FS	38.1				6.47	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_036-038CM	FS	43.3				6.915	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_038-040CM	FS	27.1				7.86	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_040-045CM	FS	34.9				6.765	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_045-050CM	FS	44.2				6.195	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_050-055CM	FS	43.2				6.74	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_055-060CM	FS	45.7				7.215	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_060-065CM	FS	43.2				6.785	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_065-070CM	FS	30.9				6.425	
L1737040	MM-C1-C	10/6/2017	MM-C1-C-17_SED_070-075CM	FS	43.8				6.41	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_000-001CM	FS	34.2				5.985	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_001-002CM	FS	28.6				6.8	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_002-003CM	FS	26.8				6.38	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_003-004CM	FS	35.3				6.365	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_004-005CM	FS	36.6				5.945	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_005-006CM	FS	32.6				5.645	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_006-007CM	FS	34.4				6.29	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_007-008CM	FS	25.4				6.105	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_008-009CM	FS	33.3				6.55	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_009-010CM	FS	33.8				6.41	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_010-011CM	FS	34.8				6.41	

**TABLE 3
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_011-012CM	FS	19.2				6.21	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_012-013CM	FS	35.6				5.685	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_013-014CM	FS	38.1				5.33	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_014-015CM	FS	38.4				5.8	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_015-016CM	FS	35.5				6.115	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_016-017CM	FS	25.9				5.62	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_017-018CM	FS	37.8				6.435	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_018-019CM	FS	35.2				6.4	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_019-020CM	FS	40.8				6.395	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_020-022CM	FS	38.8				6.53	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_022-024CM	FS	40.2				6.47	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_024-026CM	FS	44.3				6.595	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_026-028CM	FS	44.3				6.28	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_028-030CM	FS	46.2				6.12	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_030-032CM	FS	43.2				4.985	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_032-034CM	FS	53.9				4.425	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_034-036CM	FS	51.7				5.05	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_036-038CM	FS	34				4.525	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_038-040CM	FS	45.6				6.69	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_040-045CM	FS	48.5				4.47	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_045-050CM	FS	57.4				3.225	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_050-055CM	FS	52.9				3.5	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_055-060CM	FS	56.4				3.495	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_060-065CM	FS	54				2.97	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_065-070CM	FS	51.6				3.595	
L1737041	MM-T1-C1-A	10/6/2017	MM-T1-C1-A-17_SED_070-075CM	FS	57.4				3.42	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_000-001CM	FS	40.8				7.32	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_001-002CM	FS	37.5				7.685	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_002-003CM	FS	36.7				7.965	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_003-004CM	FS	35.5				8.24	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_004-005CM	FS	34.1				8.265	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_005-006CM	FS	37.4				8.375	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_006-007CM	FS	39.7				7.43	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_007-008CM	FS	15.7				8.04	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_008-009CM	FS	40.5				7.445	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_009-010CM	FS	39.8				6.9	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_010-011CM	FS	38.8				7.6	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_011-012CM	FS	37				7.72	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_012-013CM	FS	37.2				7.97	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_013-014CM	FS	38.1				7.78	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_014-015CM	FS					8.195	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_015-016CM	FS	34.9				9.17	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_016-017CM	FS					7.905	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_017-018CM	FS	36.5				7.59	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_018-019CM	FS	33.8				8.07	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_019-020CM	FS	27.1				8.175	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_020-022CM	FS	35.8				7.4	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_022-024CM	FS	30.3				7.475	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_024-026CM	FS	30.5				8.04	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_026-028CM	FS	37.8				7.73	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_028-030CM	FS	40.2				8.69	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_030-032CM	FS	37				8.075	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_032-034CM	FS	37				8.09	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_034-036CM	FS	22.9				7.69	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_036-038CM	FS	39.8				8.02	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_038-040CM	FS	31.6				9.085	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_040-045CM	FS	38.7				8.185	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_045-050CM	FS	39.3				7.075	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_050-055CM	FS	41				7.055	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_055-060CM	FS	27.7				6.575	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_060-065CM	FS	45.3				6.465	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_065-070CM	FS	51.2				6.225	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_070-075CM	FS	47				5.09	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_075-080CM	FS	36.4				5.205	
L1737042	MM-T1-C4	10/6/2017	MM-T1-C4-17_SED_080-085CM	FS	53.7				4.51	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_000-001CM	FS	29.5				11.4	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_001-002CM	FS	13.3				13.75	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_002-003CM	FS	27.3				12.15	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_003-004CM	FS	26.4				14.65	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_004-005CM	FS					13.9	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_005-006CM	FS	30.9				13.8	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_006-007CM	FS	22				14.95	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_007-008CM	FS	8.82				13.1	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_008-009CM	FS					12	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_009-010CM	FS	34.2				12.2	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_010-011CM	FS	29.1				11.2	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_011-012CM	FS	17.1				12.15	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_012-013CM	FS	4.09				12.05	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_013-014CM	FS	28.8				12.75	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_014-015CM	FS	28.6				11.8	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_015-016CM	FS	29.4				11.85	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_016-017CM	FS	27.9				11.6	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_017-018CM	FS	28.9				12.25	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_018-019CM	FS	30.6				13.4	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_019-020CM	FS	11.5				13.05	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_020-022CM	FS	25				13.35	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_022-024CM	FS	31.6				11.4	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_024-026CM	FS	32.7				12.55	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_026-028CM	FS	30.5				11.85	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_028-030CM	FS	29.5				12.1	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_030-032CM	FS	22.9				12.05	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_032-034CM	FS	34				12.95	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_034-036CM	FS	13.9				12	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_036-038CM	FS	32				25.05	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_038-040CM	FS	38.6				5.705	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_040-045CM	FS	34				7.625	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_045-050CM	FS	36.1				6.4	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_050-055CM	FS	17.3				6.15	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_055-060CM	FS	42.6				6.995	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_060-065CM	FS	22.1				3.23	
L1737043	MM-T1-C5	10/9/2017	MM-T1-C5-A-17_SED_065-070CM	FS	40				5.355	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_000-001CM	FS	16.7				25.3	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_001-002CM	FS	13.3				23	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_002-003CM	FS	17.6				22.15	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_003-004CM	FS	13.6				20.4	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_004-005CM	FS	16.4				22	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_005-006CM	FS	17.1				21.8	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_006-007CM	FS	14.9				22.2	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_007-008CM	FS	15.7				27.55	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_008-009CM	FS	14.3				21	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_009-010CM	FS	14.3				13.35	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_010-011CM	FS	18.6				24.15	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_011-012CM	FS	19.2				23.35	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_012-013CM	FS	19.7				23.25	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_013-014CM	FS	16.3				28.6	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_014-015CM	FS	17.1				30.65	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_015-016CM	FS	6.45				28.55	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_016-017CM	FS	14.6				29.5	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_017-018CM	FS	15				28.7	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_018-019CM	FS					25.9	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_019-020CM	FS	17.2				25.85	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_020-022CM	FS	14				26.95	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_022-024CM	FS	16.9				23.05	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_024-026CM	FS	16.3				23.35	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_026-028CM	FS	20.5				16.1	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_028-030CM	FS	17.2				22.85	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_030-032CM	FS	16.9				19.6	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_032-034CM	FS	22.1				13.25	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_034-036CM	FS	18.7				17.9	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_036-038CM	FS	20.6				17	

**TABLE 3
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2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total	Final	Final	Total	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_038-040CM	FS	20.6				16.75	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_040-045CM	FS	25				12.6	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_045-050CM	FS	20				15.5	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_050-055CM	FS	20.7				14.95	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_055-060CM	FS	20.8				17.75	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_060-065CM	FS	24.2				14.9	
L1737044	MM-T1-C6	10/9/2017	MM-T1-C6-A-17_SED_065-070CM	FS	18.8				16.05	
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_000-001CM	FS	46.5	J			4.775	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_001-002CM	FS	52.4				3.8	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_002-003CM	FS	54.3				3.705	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_003-004CM	FS	53.7				2.92	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_004-005CM	FS	48.9				3.28	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_005-006CM	FS	53.5				3.045	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_006-007CM	FS	51.9				3.185	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_007-008CM	FS	50.7				3.48	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_008-009CM	FS	53				2.76	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_009-010CM	FS	48.8				3.08	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_010-011CM	FS	50.6				3.52	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_011-012CM	FS	45.4				3.39	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_012-013CM	FS	54.7				4.095	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_013-014CM	FS	49.3				4.84	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_014-015CM	FS	36.4				5.905	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_015-016CM	FS	40.8				4.41	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_016-017CM	FS	57				3.135	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_017-018CM	FS	48.4				3.27	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_018-019CM	FS	51				3.32	J

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_019-020CM	FS	56.4				3.18	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_020-022CM	FS	48.2				4.21	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_022-024CM	FS	87.8				2.025	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_024-026CM	FS	43.4				0.594	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_026-028CM	FS	81.7				0.409	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_028-030CM	FS	75.9				0.4735	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_030-032CM	FS	84.2				0.688	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_032-034CM	FS	53				1.365	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_034-036CM	FS	71.7				0.7425	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_036-038CM	FS	75.4				0.4015	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_038-040CM	FS	56.6				0.376	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_040-045CM	FS	76.6				0.3565	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_045-050CM	FS	85.8				0.362	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_050-055CM	FS	84.8				0.7885	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_055-060CM	FS	83.5				0.754	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_060-065CM	FS	72.9				0.7745	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_065-070CM	FS	86.8				0.3145	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_070-075CM	FS	88				0.1645	J
L1737045	MM-T3-C3-B2	10/4/2017	MM-T3-C3-B2-17_SED_075-080CM	FS	83.6				0.1025	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_000-001CM	FS	46.3				4.42	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_001-002CM	FS	43.3				4.705	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_002-003CM	FS	40.5				4.825	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_003-004CM	FS	42.6				5.38	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_004-005CM	FS	40.8				5.34	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_005-006CM	FS	41.2				5.37	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_006-007CM	FS	42				6.005	J

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_007-008CM	FS	34.2				5.615	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_008-009CM	FS	39.8				5.935	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_009-010CM	FS	39				5.74	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_010-011CM	FS	42.5				5.845	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_011-012CM	FS	30.2				5.085	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_012-013CM	FS	43				6.665	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_013-014CM	FS	45.4				5.735	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_014-015CM	FS	45.3				5.625	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_015-016CM	FS	41				6.3	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_016-017CM	FS	42.4				6.04	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_017-018CM	FS	44.6				6.245	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_018-019CM	FS	42.2				7.75	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_019-020CM	FS	32.9				8.015	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_020-022CM	FS	41.7				6.35	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_022-024CM	FS	38.3				5.845	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_024-026CM	FS	45.3				7.88	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_026-028CM	FS	24.1				6.89	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_028-030CM	FS	36.8				6.87	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_030-032CM	FS	40.2				6.595	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_032-034CM	FS	30.1				7.57	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_034-036CM	FS	29.7				7.515	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_036-038CM	FS	41.7				8.185	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_038-040CM	FS	34.6				8.24	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_040-045CM	FS	44.6				9.38	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_045-050CM	FS	32.3				8.785	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_050-055CM	FS	38.4				9.545	J

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_055-060CM	FS	49.5				5.86	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_060-065CM	FS	39.8				6.805	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_065-070CM	FS	45.2				7.585	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_070-075CM	FS	31.9				7.515	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_075-080CM	FS	38.1				6.695	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_080-085CM	FS	45.7				6.525	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_085-090CM	FS	47.9				5.62	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_090-095CM	FS	59.6				2.97	J
L1737046	OR-T1-C3-A	10/4/2017	OR-T1-C3-A-17_SED_095-101CM	FS	61.9				2.31	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_000-001CM	FS	12.3				24.7	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_001-002CM	FS	52.9				3.66	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_002-003CM	FS	38.5				7.07	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_003-004CM	FS	31.5				4.68	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_004-005CM	FS	34.3				3.2	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_005-006CM	FS	11.8				5.525	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_006-007CM	FS	66.7				3.895	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_007-008CM	FS	66.1				2.68	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_008-009CM	FS	40.3				3.34	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_009-010CM	FS	39.6				3.06	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_010-011CM	FS	56				3.305	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_011-012CM	FS	20.3				3.335	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_012-013CM	FS	42.4				3.295	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_013-014CM	FS	39.7				2.275	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_014-015CM	FS	63.5				2.16	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_015-016CM	FS	44.7				2.085	J
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_016-017CM	FS	50				2.025	J

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
					Final	Final	Final	Final	Final	Final		
					Result	Qualifier	Result	Qualifier	Result	Qualifier		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_017-018CM	FS	45				1.72	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_018-019CM	FS	19				1.73	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_019-020CM	FS	61.9				1.61	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_020-022CM	FS	52.1				1.845	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_022-024CM	FS	61.9				1.945	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_024-026CM	FS	43.3				1.915	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_026-028CM	FS	64.9				2.125	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_028-030CM	FS	65				1.92	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_030-032CM	FS	65.3				2.16	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_032-034CM	FS	50				1.875	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_034-036CM	FS	50				1.875	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_036-038CM	FS	67.9				1.645	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_038-040CM	FS	66.2				1.85	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_040-045CM	FS	67				1.74	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_045-050CM	FS	62.9				1.9	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_050-055CM	FS	70.3				1.97	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_055-060CM	FS	44.4				1.635	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_060-065CM	FS	59.3				2.285	J		
L1737047	OR-T2-C3-B	10/3/2017	OR-T2-C3-B-17_SED_065-070CM	FS	65.5				2.31	J		
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_000-001CM	FS	30	J			15.85	J		
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_001-002CM	FS	21.4				16.15	J		
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_002-003CM	FS					18.25	J		
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_003-004CM	FS	16.7				20	J		
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_004-005CM	FS	18.8				21.25	J		
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_005-006CM	FS					20.25	J		
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_006-007CM	FS					19.15	J		

**TABLE 3
DATA VALIDATION SUMMARY
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_007-008CM	FS					12.45	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_008-009CM	FS					10.8	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_010-011CM	FS	25.6				14.95	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_011-012CM	FS	19.6				19.65	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_012-013CM	FS	21.7				20.4	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_013-014CM	FS	19				18.75	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_014-015CM	FS	23.8				14.85	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_015-016CM	FS	25.4				12.75	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_016-017CM	FS	27.7				10.59	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_017-018CM	FS	26.4				11.3	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_018-019CM	FS	27.6				12.7	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_019-020CM	FS	26.7				12	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_020-022CM	FS	26				12.15	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_022-024CM	FS	27.3				11.1	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_024-026CM	FS	31.9				8.23	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_026-028CM	FS	33.3				7.77	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_028-030CM	FS	33.9				6.72	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_030-032CM	FS	36.2				6.655	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_032-034CM	FS	27.5				7.275	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_034-036CM	FS	34.6				7.195	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_036-038CM	FS	32.9				6.285	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_038-040CM	FS	39.2				5.965	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_040-045CM	FS	35.1				5.66	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_045-050CM	FS	34.5				5.88	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_050-055CM	FS	37.5				5.92	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_055-060CM	FS	27.4				12.2	J

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_060-065CM	FS	25.3				11.45	J
L1738093	MM-T3-C6	10/10/2017	MM-T3-C6-17_SED_065-070CM	FS	26.8				14.2	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_000-001CM	FS	35				8.14	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_001-002CM	FS	30.2				9.485	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_002-003CM	FS	32.9				9.675	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_003-004CM	FS	33.6				7.98	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_004-005CM	FS	34.9				8.35	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_005-006CM	FS	29.7				9.14	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_006-007CM	FS	30				11.75	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_007-008CM	FS	28.8				10.9	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_008-009CM	FS	32.8				9.675	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_009-010CM	FS	31.9				9.885	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_010-011CM	FS	34.1				10.02	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_011-012CM	FS	29.8				12.4	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_012-013CM	FS	28				12.15	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_013-014CM	FS	33.3				12	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_014-015CM	FS	17.6				10.35	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_015-016CM	FS	35.2				10.59	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_016-017CM	FS	37.1				11.05	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_017-018CM	FS	33.6				11.15	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_018-019CM	FS	35				11.4	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_019-020CM	FS	35.3				10.9	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_020-022CM	FS	33.8				12.65	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_022-024CM	FS	30.3				13.45	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_024-026CM	FS	33.5				14.8	J
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_026-028CM	FS	33.5				11.05	J

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN			
					Parameter	Unit	% Solids		Mercury		TOC	
							PERCENT	Total	NG/G	Total	PERCENT	Total
					Final	Final	Final	Final	Final	Final		
					Result	Qualifier	Result	Qualifier	Result	Qualifier		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_028-030CM	FS	36				10.55	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_030-032CM	FS	40.4				8.11	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_032-034CM	FS	39.8				9.02	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_034-036CM	FS	42.3				5.57	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_036-038CM	FS	42.5				7.06	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_038-040CM	FS	41.4				8.815	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_040-045CM	FS	32.8				11.85	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_045-050CM	FS	30.9				12.95	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_050-055CM	FS	34				12.1	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_055-060CM	FS	31				14.35	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_060-065CM	FS	26.3				18.85	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_065-070CM	FS	24.9				17.65	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_070-075CM	FS	20.8				21.3	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_075-080CM	FS	17.3				23.15	J		
L1738103	MM-T4-C1	10/10/2017	MM-T4-C1-17_SED_080-085CM	FS	19				21.6	J		
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_000-001CM	FS	27.5				16.25	J		
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_001-002CM	FS	25.8				15.15	J		
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_002-003CM	FS	23.4				17.6	J		
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_003-004CM	FS	21.2				18.65	J		
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_004-005CM	FS	23				15.6	J		
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_005-006CM	FS					17.75	J		
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_006-007CM	FS	21.4				16.6	J		
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_007-008CM	FS	23.9				15.85	J		
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_008-009CM	FS	33.7				10.6	J		
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_009-010CM	FS	20.2				10.215	J		
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_010-011CM	FS	25.9				13.9	J		

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method	% Solids		EPA 1631		LLOYD KAHN	
				Parameter	PERCENT		Mercury		TOC	
				Unit	Total		NG/G		PERCENT	
QC Code	Final	Final	Final	Final	Final	Final				
				Fraction	Result	Qualifier	Result	Qualifier	Result	Qualifier
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_011-012CM	FS					13.35	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_012-013CM	FS	26.9				13.05	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_013-014CM	FS	10.4				14.1	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_014-015CM	FS	25.9				13.9	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_015-016CM	FS	25.9				14.2	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_016-017CM	FS	25.8				13.2	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_017-018CM	FS	28.2				11.65	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_018-019CM	FS	30.2				9.975	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_019-020CM	FS	30.7				9.355	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_020-022CM	FS	37.3				7.635	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_022-024CM	FS	31.1				11.65	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_024-026CM	FS	36.5				8.725	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_026-028CM	FS	36.9				8.11	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_028-030CM	FS	37.9				7.14	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_030-032CM	FS	35.2				8.505	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_032-034CM	FS	34.7				8.415	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_034-036CM	FS	33.7				9.73	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_036-038CM	FS	33.3				10.7	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_038-040CM	FS	38.8				8.92	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_040-045CM	FS	41.1				7.44	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_045-050CM	FS	43.1				8.155	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_050-055CM	FS	47.4				5.32	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_055-060CM	FS	54				4.795	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_060-065CM	FS	35.7				4.96	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_065-070CM	FS	45.4				5.805	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_070-075CM	FS	63.9				2.33	J

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_075-080CM	FS	56.2				3.93	J
L1738104	MM-T4-C5	10/11/2017	MM-T4-C5-17_SED_080-085CM	FS	53.3				4.035	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_000-001CM	FS	38.5				7.36	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_001-002CM	FS	40.7				7.7	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_002-003CM	FS	39.3				7.505	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_003-004CM	FS	41.4				7.34	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_004-005CM	FS	41				7.405	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_005-006CM	FS	39.2				6.895	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_006-007CM	FS	41.9				6.295	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_007-008CM	FS	41.4				6.72	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_008-009CM	FS	38.9				6.745	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_009-010CM	FS	43.4				6.545	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_010-011CM	FS	43.8				6.6	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_011-012CM	FS	43.3				6.62	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_012-013CM	FS	44.6				6.82	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_013-014CM	FS	44				7.22	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_014-015CM	FS	40.3				7.99	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_015-016CM	FS	39.1				9.015	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_016-017CM	FS	30.6				8.99	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_017-018CM	FS	39.3				9.085	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_018-019CM	FS	27.2				9.59	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_019-020CM	FS	35.6				9.49	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_020-022CM	FS	43.1				9.09	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_022-024CM	FS	35.4				10.85	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_024-026CM	FS	39.2				10.4	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_026-028CM	FS	36.2				10.95	J

TABLE 3
DATA VALIDATION SUMMARY
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_028-030CM	FS	38.2				12.2	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_030-032CM	FS	37.4				12.45	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_032-034CM	FS	39				11.9	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_034-036CM	FS	36.7				11.3	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_036-038CM	FS	40				9.77	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_038-040CM	FS	40.9				7.815	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_040-045CM	FS	46.7				6.615	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_045-050CM	FS	48.5				6.1	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_050-055CM	FS	48.4				6.13	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_055-060CM	FS	51.6				6.225	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_060-065CM	FS	46.3				5.65	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_065-070CM	FS	50				5.075	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_070-075CM	FS	48.8				4.895	J
L1738105	MM-T4-C6	10/11/2017	MM-T4-C6-17_SED_075-080CM	FS	58.4				4.585	J
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_000-001CM	FS	27.9				12.85	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_001-002CM	FS	24.2				13.35	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_002-003CM	FS					14.15	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_003-004CM	FS					15.1	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_004-005CM	FS					14.75	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_005-006CM	FS	25.7				14	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_006-007CM	FS	23.7				12.95	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_007-008CM	FS	25				15.1	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_008-009CM	FS					14.95	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_009-010CM	FS	32				14.3	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_010-011CM	FS	28				13.9	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_011-012CM	FS	24.7				13.8	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_012-013CM	FS	22.6				17.65	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_013-014CM	FS	21				16.95	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_014-015CM	FS	20.5				19.4	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_015-016CM	FS	16.2				20.6	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_016-017CM	FS	18				22.05	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_017-018CM	FS	17				22.75	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_018-019CM	FS					21.6	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_020-022CM	FS	19.5				19.5	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_022-024CM	FS	7.8				16.5	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_024-026CM	FS	24.2				17.55	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_026-028CM	FS	21.8				13.55	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_028-030CM	FS	24.1				14.7	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_030-032CM	FS	27.6				13.9	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_032-034CM	FS	34.9				9.81	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_034-036CM	FS	31.2				11.7	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_036-038CM	FS	31.1				13.55	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_038-040CM	FS	29.5				13.3	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_040-045CM	FS	31.7				13.4	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_045-050CM	FS	35.1				6.835	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_050-055CM	FS	58.8				5.865	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_055-060CM	FS	29.3				10.4	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_060-065CM	FS	34.8				7.26	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_065-070CM	FS	34.6				9	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_070-075CM	FS	34				8.41	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_075-080CM	FS	32.3				9.73	
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_080-085CM	FS	28.9				9.19	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total	Final	Final	Total	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1738106	MM-T5-C1	10/13/2017	MM-T5-C1-17_SED_085-090CM	FS	37.9				6.43	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_000-001CM	FS					4.085	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_001-002CM	FS	40.2	J			5.27	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_002-003CM	FS	47.6				5.45	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_003-004CM	FS	47.1				5.15	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_004-005CM	FS	48.7				5.105	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_005-006CM	FS	48.8				5.26	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_006-007CM	FS	48.1				5.1	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_007-008CM	FS	51.2				4.915	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_008-009CM	FS	49				5.925	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_009-010CM	FS	46.8				4.97	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_010-011CM	FS	47				6.04	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_011-012CM	FS	45.2				7.28	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_012-013CM	FS	42.9				7.615	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_013-014CM	FS	38.6				8.455	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_014-015CM	FS	40.3				9.32	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_015-016CM	FS	37.5				5.565	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_016-017CM	FS	48.6				5.96	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_017-018CM	FS	50				4.46	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_018-019CM	FS	46.6				4.85	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_019-020CM	FS	53.1				5.27	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_020-022CM	FS	47.4				4.19	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_022-024CM	FS	52.9				4.03	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_024-026CM	FS	53.6				4.53	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_026-028CM	FS	52.2				4.805	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_028-030CM	FS	48.9				4.95	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total	Final	Final	Total	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_030-032CM	FS	48.4				5.125	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_032-034CM	FS	50				5.665	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_034-036CM	FS	50				4.705	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_036-038CM	FS	53				4.94	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_038-040CM	FS	26.6				4.405	J
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_040-045CM	FS	60.3				3.56	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_045-050CM	FS	52.8				3.655	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_050-055CM	FS	64.9				2.945	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_055-060CM	FS	74.3				2.33	
L1738128	MM-T5-C2	10/12/2017	MM-T5-C2-17_SED_060-065CM	FS	72.5				2.275	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_000-001CM	FS	45.7				5.895	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_001-002CM	FS	45.3				6.36	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_002-003CM	FS	45.3				5.545	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_003-004CM	FS	45.5				5.73	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_004-005CM	FS	43.9				6.37	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_005-006CM	FS	49.7				4.96	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_006-007CM	FS	47.7				5.67	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_007-008CM	FS	44.8				5.86	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_008-009CM	FS	45.4				5.82	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_009-010CM	FS	46.2				5.41	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_010-011CM	FS	47.8				4.735	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_011-012CM	FS	44.4				5.905	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_012-013CM	FS	41.1				7.08	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_013-014CM	FS	43.9				5.725	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_014-015CM	FS	44				6.245	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_015-016CM	FS	44.6				6.435	

TABLE 3
DATA VALIDATION SUMMARY
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_016-017CM	FS	46.7				5.285	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_017-018CM	FS	45.5				5.46	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_018-019CM	FS	45				6.21	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_019-020CM	FS	46.9				5.64	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_020-022CM	FS	47.2				5.605	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_022-024CM	FS	45.1				6.365	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_024-026CM	FS	44.1				6.475	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_026-028CM	FS	46				4.805	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_028-030CM	FS	44.4				6.505	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_030-032CM	FS	42.9				6.975	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_032-034CM	FS	44.6				7.485	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_034-036CM	FS	44				6.445	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_036-038CM	FS	44				7.32	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_038-040CM	FS	43.4				7.095	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_040-045CM	FS	42.9				8.09	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_045-050CM	FS	40.7				8.965	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_050-055CM	FS	45.7				5.68	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_055-060CM	FS	45.7				6.415	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_060-065CM	FS	47.6				6.57	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_065-070CM	FS	42.4				6.85	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_070-075CM	FS	33.5				8.92	
L1739120	MM-T3-C4-D	10/16/2017	MM-T3-C4-D-17_SED_075-080CM	FS	23.1				29.2	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_000-001CM	FS	19				25.85	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_001-002CM	FS	19.8				25.55	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_002-003CM	FS	18.3				27.25	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_003-004CM	FS					24.7	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_004-005CM	FS	20.8				23.4	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_005-006CM	FS					22.7	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_006-007CM	FS	19				26.3	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_008-009CM	FS					27	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_009-010CM	FS					26.65	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_010-011CM	FS	17.8				18.65	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_011-012CM	FS	23.1				18.95	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_012-013CM	FS	21.7				28.35	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_013-014CM	FS	23.2				20.2	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_014-015CM	FS	20.8				18.8	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_015-016CM	FS	20.7				19.7	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_016-017CM	FS	23.9				18.35	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_017-018CM	FS	27.1				16.7	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_018-019CM	FS	25				16.85	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_019-020CM	FS	28.1				17.7	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_020-022CM	FS	29.8				18.4	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_022-024CM	FS	29				17	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_024-026CM	FS	26.2				17.85	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_026-028CM	FS	23.5				23.45	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_028-030CM	FS	21.2				20.7	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_030-032CM	FS	22.6				20.55	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_032-034CM	FS	24.8				17.9	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_034-036CM	FS	24.6				18.25	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_036-038CM	FS	23.2				21.7	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_038-040CM	FS	24.4				19.25	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_040-045CM	FS	28.2				15.25	

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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_045-050CM	FS	26.7				12.65	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_050-055CM	FS	27.3				12.05	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_055-060CM	FS	31.1				10.95	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_060-065CM	FS	33.9				9.89	
L1739121	MM-T3-C7	10/16/2017	MM-T3-C7-17_SED_065-070CM	FS	35				9.205	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_000-001CM	FS	34				6.295	J
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_001-002CM	FS	38				5.87	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_002-003CM	FS	38.6				6.465	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_003-004CM	FS	43.4				6.91	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_004-005CM	FS	46				6.275	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_005-006CM	FS	47.4				7.57	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_006-007CM	FS	47.6				5.885	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_007-008CM	FS	47.9				5.27	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_008-009CM	FS	40.8				6.135	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_009-010CM	FS	39.1				6.845	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_010-011CM	FS	36.6				6.455	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_011-012CM	FS	39.1				6.63	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_012-013CM	FS	41.6				6.58	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_013-014CM	FS	36.9				6.44	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_014-015CM	FS	34.4				6.105	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_015-016CM	FS	39				5.375	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_016-017CM	FS	35.7				6.05	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_017-018CM	FS	43.4				4.96	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_018-019CM	FS	43.1				5.11	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_019-020CM	FS	52.1				3.12	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_020-022CM	FS	72.3				0.4335	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_022-024CM	FS	78.8				0.1755	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_024-026CM	FS	76.9				0.2005	J
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_026-028CM	FS	72.6				0.207	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_028-030CM	FS	74.8				0.204	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_030-032CM	FS	75.4				0.208	J
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_032-034CM	FS	76.3				0.1675	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_034-036CM	FS	76.7				0.1645	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_036-038CM	FS	78.2				0.1555	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_038-040CM	FS	78.4				0.1935	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_040-045CM	FS	76.4				0.1905	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_045-050CM	FS	72.3				0.186	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_050-055CM	FS	73.5				0.189	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_055-060CM	FS	75.9				0.1895	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_060-065CM	FS	75.9				0.188	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_065-070CM	FS	72				0.179	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_070-075CM	FS	75.7				0.175	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_075-080CM	FS	73.1				0.1895	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_080-085CM	FS	75.8				0.1505	
L1739122	MM-T4-C7	10/16/2017	MM-T4-C7-17_SED_085-090CM	FS	75.9				0.1395	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_000-001CM	FS	30.7				13.2	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_001-002CM	FS	30.9				13.4	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_002-003CM	FS					12.45	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_003-004CM	FS	33.3				11.7	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_004-005CM	FS					10.82	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_005-006CM	FS	27.6				13.85	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_006-007CM	FS	28.6				12.2	

**TABLE 3
DATA VALIDATION SUMMARY
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_007-008CM	FS	36.1				10.205	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_008-009CM	FS	33.8				9.84	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_009-010CM	FS	31.7				11.25	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_010-011CM	FS	31.3				12.35	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_011-012CM	FS	29.2				13	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_012-013CM	FS	32.2				12.55	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_013-014CM	FS	27.9				12	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_014-015CM	FS	29.9				12	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_015-016CM	FS	28.3				12.75	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_016-017CM	FS	27.4				13.25	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_017-018CM	FS	26				13.45	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_018-019CM	FS	26.7				13.05	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_019-020CM	FS	25.8				14.4	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_020-022CM	FS	27.9				12.45	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_022-024CM	FS	30.7				12.55	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_024-026CM	FS	27.9				11.85	
L1739123	MM-T5-C3	10/13/2017	MM-T5-C3-17_SED_026-028CM	FS	28.4				12.15	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_028-030CM	FS	26.4				11.9	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_030-032CM	FS	24.6				13.8	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_032-034CM	FS	25.8				12.5	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_034-036CM	FS	25.6				12.9	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_036-038CM	FS	28.1				12.15	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_038-040CM	FS	33				10.07	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_040-045CM	FS	33.7				10.55	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_045-050CM	FS	39.1				8.965	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_050-055CM	FS	45				7.5	

TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_055-060CM	FS	43.2				7.565	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_060-065CM	FS	48				5.29	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_065-070CM	FS	42				7.47	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_070-075CM	FS	42.9				6.47	
L1739123	MM-T5-C3	10/16/2017	MM-T5-C3-17_SED_075-080CM	FS	44.5				5.78	
L1739124	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_00-01	FS	52.9				4.025	
L1739124	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_01-03	FS	51.6				4.935	
L1739124	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_03-05	FS	49.3				3.99	
L1739124	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_05-07	FS	51.7				3.19	
L1739124	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_07-10	FS	55.9				3.44	
L1739124	VN-MU3-GC-1-G	10/16/2017	VN-MU3-GC-1-G-17_SED_10-15	FS	50.7				3.69	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_000-001CM	FS	41.2				5.565	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_001-002CM	FS	42.4				5.845	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_002-003CM	FS	38.1				5.125	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_003-004CM	FS	38.5				5.015	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_004-005CM	FS	39				5.13	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_005-006CM	FS	44.1				6.15	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_006-007CM	FS	41.2				6.225	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_007-008CM	FS	39.2				5.82	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_008-009CM	FS	40.2				5.94	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_009-010CM	FS	40.4				5.88	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_010-011CM	FS	41.9				5.925	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_011-012CM	FS	40.4				6.375	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_012-013CM	FS	42.7				6.095	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_013-014CM	FS	43.2				5.945	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_014-015CM	FS	42.3				5.56	

**TABLE 3
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SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_015-016CM	FS	49.6				5.18	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_016-017CM	FS	47.7				5.44	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_017-018CM	FS	47.4				5.13	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_018-019CM	FS	50.5				5.265	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_019-020CM	FS	48.8				5.025	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_020-022CM	FS	49.1				5.13	J
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_022-024CM	FS	52.1				4.565	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_024-026CM	FS	53.9				4.34	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_026-028CM	FS	51.6				4.955	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_028-030CM	FS	52.4				4.415	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_030-032CM	FS	53.6				4.48	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_032-034CM	FS	50				4.935	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_034-036CM	FS	55.2				4.175	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_036-038CM	FS	60.2				3.115	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_038-040CM	FS	62.6				2.72	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_040-045CM	FS	64.5				2.535	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_045-050CM	FS	66.7				2.26	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_050-055CM	FS	64.6				2.035	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_055-060CM	FS	65.4				2.255	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_060-065CM	FS	66.1				1.825	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_065-070CM	FS	64.6				2.3	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_070-075CM	FS	66.2				2.28	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_075-080CM	FS	67.4				2.435	
L1739127	OR-T3-C4-A	10/17/2017	OR-T3-C4-A-17_SED_080-085CM	FS	63.8				2.44	
L1739536	ES-01-F	10/20/2017	ES-01-F-17_SED_00-01	FS	32.4				4.56	
L1739536	ES-01-F	10/20/2017	ES-01-F-17_SED_01-03	FS	34.5				4.595	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1739536	ES-01-F	10/20/2017	ES-01-F-17_SED_03-05	FS	33.1				4.54	
L1739536	ES-01-F	10/20/2017	ES-01-F-17_SED_05-07	FS	30.4				4.515	
L1739537	ES-18-F	10/23/2017	ES-18-F-17_SED_00-01	FS	51.8				1.985	
L1739537	ES-18-F	10/23/2017	ES-18-F-17_SED_01-03	FS	53.3				2.545	
L1739537	ES-18-F	10/23/2017	ES-18-F-17_SED_03-05	FS	52.5				3.495	J
L1739537	ES-18-F	10/23/2017	ES-18-F-17_SED_05-07	FS	53.2				2.415	
L1739540	MM-T1-C2-D	10/20/2017	MM-T1-C2-D-17_SED_00-01	FS	24.4				6.975	
L1739540	MM-T1-C2-D	10/20/2017	MM-T1-C2-D-17_SED_01-03	FS	32.4				6.61	
L1739540	MM-T1-C2-D	10/20/2017	MM-T1-C2-D-17_SED_03-05	FS	32.3				6.835	
L1739540	MM-T1-C2-D	10/20/2017	MM-T1-C2-D-17_SED_05-07	FS	34.7				6.91	J
L1739540	MM-T1-C2-D	10/20/2017	MM-T1-C2-D-17_SED_07-10	FS	40.8				6.69	
L1739541	MM-T2-C8-B	10/24/2017	MM-T2-C8-B-17_SED_00-01	FS	22.1				17.95	
L1739541	MM-T2-C8-B	10/24/2017	MM-T2-C8-B-17_SED_01-03	FS	22				17.25	
L1739541	MM-T2-C8-B	10/24/2017	MM-T2-C8-B-17_SED_03-05	FS	25				13.4	
L1739541	MM-T2-C8-B	10/24/2017	MM-T2-C8-B-17_SED_05-07	FS	22.9				15.55	
L1739541	MM-T2-C8-B	10/24/2017	MM-T2-C8-B-17_SED_07-10	FS	21.5				15.25	
L1739542	MM-T3-C2-F	10/20/2017	MM-T3-C2-F-17_SED_00-01	FS	35.6				4.34	
L1739542	MM-T3-C2-F	10/20/2017	MM-T3-C2-F-17_SED_01-03	FS	35.9				8.05	
L1739542	MM-T3-C2-F	10/20/2017	MM-T3-C2-F-17_SED_03-05	FS	33.3				8.6	
L1739542	MM-T3-C2-F	10/20/2017	MM-T3-C2-F-17_SED_05-07	FS	29.8				9.345	
L1739572	MM-T3-C3-C	10/19/2017	MM-T3-C3-C-17_SED_00-01	FS	75				0.726	
L1739572	MM-T3-C3-C	10/19/2017	MM-T3-C3-C-17_SED_01-03	FS	52.2				2.27	
L1739572	MM-T3-C3-C	10/19/2017	MM-T3-C3-C-17_SED_03-05	FS	47.2				2.69	
L1739573	MM-T4-C2-F	10/24/2017	MM-T4-C2-F-17_SED_00-01	FS	37.5				4.46	
L1739573	MM-T4-C2-F	10/24/2017	MM-T4-C2-F-17_SED_01-03	FS	37.8				6.97	J
L1739573	MM-T4-C2-F	10/24/2017	MM-T4-C2-F-17_SED_03-05	FS	50.9				2.545	

TABLE 3
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1739573	MM-T4-C2-F	10/24/2017	MM-T4-C2-F-17_SED_05-07	FS	39.5				5.49	
L1739573	MM-T4-C2-F	10/24/2017	MM-T4-C2-F-17_SED_07-10	FS	30.6				6.765	
L1739577	OR-T1-C2-C	10/19/2017	OR-T1-C2-C-17_SED_00-01	FS	39				4.79	
L1739577	OR-T1-C2-C	10/19/2017	OR-T1-C2-C-17_SED_01-03	FS	42.8				5.01	
L1739577	OR-T1-C2-C	10/19/2017	OR-T1-C2-C-17_SED_03-05	FS	43.6				5.465	
L1739577	OR-T1-C2-C	10/19/2017	OR-T1-C2-C-17_SED_05-07	FS	45.6				5.28	
L1739577	OR-T1-C2-C	10/19/2017	OR-T1-C2-C-17_SED_07-10	FS	42.7				6.2	
L1739578	OR-T1-C3-C	10/19/2017	OR-T1-C3-C-17_SED_00-01	FS	44.7				5.135	
L1739578	OR-T1-C3-C	10/19/2017	OR-T1-C3-C-17_SED_01-03	FS	40				6.035	
L1739578	OR-T1-C3-C	10/19/2017	OR-T1-C3-C-17_SED_03-05	FS	42.7				5	
L1739578	OR-T1-C3-C	10/19/2017	OR-T1-C3-C-17_SED_05-07	FS	40.2				7.025	
L1739579	OR-T1-C5-C	10/23/2017	OR-T1-C5-C-17_SED_00-01	FS	22.7				7.875	
L1739579	OR-T1-C5-C	10/23/2017	OR-T1-C5-C-17_SED_01-03	FS	41.9				5.68	
L1739579	OR-T1-C5-C	10/23/2017	OR-T1-C5-C-17_SED_03-05	FS	45.8				5.52	
L1739579	OR-T1-C5-C	10/23/2017	OR-T1-C5-C-17_SED_05-07	FS	48.6				5.25	
L1739579	OR-T1-C5-C	10/23/2017	OR-T1-C5-C-17_SED_07-10	FS	48				5.02	
L1739580	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_00-01	FS	39.4				8.28	
L1739580	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_01-03	FS	37.7				7.51	
L1739580	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_03-05	FS	41.5				7.88	
L1739580	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_05-07	FS	39.7				9.12	
L1739580	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_07-10	FS	45.6				7.58	
L1739580	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_10-15	FS	57.6				3.55	
L1739580	OR-T2-C1-D	10/24/2017	OR-T2-C1-D-17_SED_15-20	FS	66.2				2.2	
L1739581	OR-T2-C2-E	10/20/2017	OR-T2-C2-E-17_SED_00-01	FS	31.5				7.38	
L1739581	OR-T2-C2-E	10/20/2017	OR-T2-C2-E-17_SED_01-03	FS	38				7.045	
L1739581	OR-T2-C2-E	10/20/2017	OR-T2-C2-E-17_SED_03-05	FS	38.6				7.035	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1739581	OR-T2-C2-E	10/20/2017	OR-T2-C2-E-17_SED_05-07	FS	41.2				6.385	
L1739581	OR-T2-C2-E	10/20/2017	OR-T2-C2-E-17_SED_07-10	FS	44.3				6.56	
L1739593	OR-T2-C3-C	10/20/2017	OR-T2-C3-C-17_SED_00-01	FS	29.7				9.065	
L1739593	OR-T2-C3-C	10/20/2017	OR-T2-C3-C-17_SED_01-03	FS	49				3.575	
L1739593	OR-T2-C3-C	10/20/2017	OR-T2-C3-C-17_SED_03-05	FS	49.6				4.28	
L1739593	OR-T2-C3-C	10/20/2017	OR-T2-C3-C-17_SED_05-07	FS	48.7				4.12	
L1739593	OR-T2-C3-C	10/20/2017	OR-T2-C3-C-17_SED_07-10	FS	45.7				4.5	
L1739594	OR-T2-C4-C	10/23/2017	OR-T2-C4-C-17_SED_00-01	FS	25.4				9.825	
L1739594	OR-T2-C4-C	10/23/2017	OR-T2-C4-C-17_SED_01-03	FS	39.9				6.02	
L1739594	OR-T2-C4-C	10/23/2017	OR-T2-C4-C-17_SED_03-05	FS	38.6				8.72	
L1739594	OR-T2-C4-C	10/23/2017	OR-T2-C4-C-17_SED_05-07	FS	41.2				6.17	
L1739594	OR-T2-C4-C	10/23/2017	OR-T2-C4-C-17_SED_07-10	FS	37.3				6.05	
L1739595	OR-T2-C5-E	10/24/2017	OR-T2-C5-E-17_SED_00-01	FS	39.5				6.29	
L1739595	OR-T2-C5-E	10/24/2017	OR-T2-C5-E-17_SED_01-03	FS	39.6				6.07	
L1739595	OR-T2-C5-E	10/24/2017	OR-T2-C5-E-17_SED_03-05	FS	41.1				6.19	
L1739595	OR-T2-C5-E	10/24/2017	OR-T2-C5-E-17_SED_05-07	FS	43.7				6.47	
L1739595	OR-T2-C5-E	10/24/2017	OR-T2-C5-E-17_SED_07-10	FS	42.4				5.91	
L1739596	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_00-01	FS	33.8				5.96	
L1739596	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_01-03	FS	37.9				6.75	
L1739596	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_03-05	FS	34.2				7.51	
L1739596	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_05-07	FS	35.3				8.015	
L1739596	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_07-10	FS	38.6				7.39	
L1739596	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_10-15	FS	28.4				10.05	
L1739596	OR-T3-C1-F	10/24/2017	OR-T3-C1-F-17_SED_15-20	FS	30.5				10.3	
L1739597	OR-T3-C2-F	10/23/2017	OR-T3-C2-F-17_SED_00-01	FS	29.1				6.115	
L1739597	OR-T3-C2-F	10/23/2017	OR-T3-C2-F-17_SED_01-03	FS	40.2				7.245	

**TABLE 3
DATA VALIDATION SUMMARY
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method	% Solids		EPA 1631		LLOYD KAHN		
					Parameter	PERCENT	Mercury	TOC				
					Unit	Total	Final	Final	Final	Final		
					Fraction		Result	Qualifier	Result	Qualifier	Result	Qualifier
L1739597	OR-T3-C2-F	10/23/2017	OR-T3-C2-F-17_SED_03-05	FS		39.8					7.36	
L1739597	OR-T3-C2-F	10/23/2017	OR-T3-C2-F-17_SED_05-07	FS		38.1					7.81	
L1739598	OR-T3-C4-F	10/23/2017	OR-T3-C4-F-17_SED_00-01	FS		32					5.705	
L1739598	OR-T3-C4-F	10/23/2017	OR-T3-C4-F-17_SED_01-03	FS		39.6					6.325	
L1739598	OR-T3-C4-F	10/23/2017	OR-T3-C4-F-17_SED_03-05	FS		45.4					5.425	
L1739598	OR-T3-C4-F	10/23/2017	OR-T3-C4-F-17_SED_05-07	FS		51.7					4.655	
L1739598	OR-T3-C4-F	10/23/2017	OR-T3-C4-F-17_SED_07-10	FS		50					4.56	
L1739599	OR-T3-C5-E	10/24/2017	OR-T3-C5-E-17_SED_00-01	FS		35.3					6.22	
L1739599	OR-T3-C5-E	10/24/2017	OR-T3-C5-E-17_SED_01-03	FS		41.1					6.095	
L1739599	OR-T3-C5-E	10/24/2017	OR-T3-C5-E-17_SED_03-05	FS		40.5					6.605	
L1739599	OR-T3-C5-E	10/24/2017	OR-T3-C5-E-17_SED_05-07	FS		36.9					6.695	
L1739599	OR-T3-C5-E	10/24/2017	OR-T3-C5-E-17_SED_07-10	FS		42.7					7.36	
L1739601	PBR-18-I	10/20/2017	PBR-18-I-17_SED_00-01	FS		27.6					6.675	
L1739601	PBR-18-I	10/20/2017	PBR-18-I-17_SED_01-03	FS		33.6					6.145	
L1739601	PBR-18-I	10/20/2017	PBR-18-I-17_SED_03-05	FS		38.7					6.535	
L1739601	PBR-18-I	10/20/2017	PBR-18-I-17_SED_05-07	FS		38.5					6.82	
L1739602	PBR-20-G	10/23/2017	PBR-20-G-17_SED_00-01	FS		45.4					2.735	
L1739602	PBR-20-G	10/23/2017	PBR-20-G-17_SED_01-03	FS		50					1.99	
L1739602	PBR-20-G	10/23/2017	PBR-20-G-17_SED_03-05	FS		48.1					2.71	
L1739653	UPB-MU11-GC-1-E	10/23/2017	UPB-MU11-GC-1-E-17_SED_00-01	FS		29.2					5.59	
L1739653	UPB-MU11-GC-1-E	10/23/2017	UPB-MU11-GC-1-E-17_SED_01-03	FS		34.4					4.83	
L1739653	UPB-MU11-GC-1-E	10/23/2017	UPB-MU11-GC-1-E-17_SED_03-05	FS		38.5					4.87	
L1739653	UPB-MU11-GC-1-E	10/23/2017	UPB-MU11-GC-1-E-17_SED_05-07	FS		37					5.06	
L1739653	UPB-MU11-GC-1-E	10/23/2017	UPB-MU11-GC-1-E-17_SED_07-10	FS		35.8					4.005	
L1739656	VE-MU4-GC-1-F	10/19/2017	VE-MU4-GC-1-F-17_SED_00-01	FS		40.7					4.925	
L1739656	VE-MU4-GC-1-F	10/19/2017	VE-MU4-GC-1-F-17_SED_01-03	FS		51.1					2.72	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1739656	VE-MU4-GC-1-F	10/19/2017	VE-MU4-GC-1-F-17_SED_03-05	FS	68.4				1.53	J
L1739691	MM-T3-C4-C	10/24/2017	MM-T3-C4-C-17_SED_00-01	FS	34.1				5.73	
L1739691	MM-T3-C4-C	10/24/2017	MM-T3-C4-C-17_SED_01-03	FS	40.4				6.285	
L1739691	MM-T3-C4-C	10/24/2017	MM-T3-C4-C-17_SED_03-05	FS	35.5				7.545	
L1739691	MM-T3-C4-C	10/24/2017	MM-T3-C4-C-17_SED_05-07	FS	41.6				5.95	
L1739691	MM-T3-C4-C	10/24/2017	MM-T3-C4-C-17_SED_07-10	FS	45.2				5.655	
L1740283	PBR-28	11/1/2017	PBR-28-17_SED_00-01	FS	35.8				5.185	
L1740283	PBR-28	11/1/2017	PBR-28-17_SED_01-03	FS	43.5				5.225	
L1740283	PBR-28	11/1/2017	PBR-28-17_SED_03-05	FS	42.6				5.7	
L1740283	PBR-28	11/1/2017	PBR-28-17_SED_05-07	FS	48.4				5.87	
L1740283	PBR-28	11/1/2017	PBR-28-17_SED_07-10	FS	57.1				3.79	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_000-001CM	FS	45.4				5.885	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_001-002CM	FS	46				5.365	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_002-003CM	FS	44				5.735	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_003-004CM	FS	44.6				5.915	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_004-005CM	FS	45.7				5.775	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_005-006CM	FS	46.4				5.44	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_006-007CM	FS	43.8				6.03	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_007-008CM	FS	49.1				5.97	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_008-009CM	FS	49.3				6.065	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_009-010CM	FS	46.5				6.755	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_010-011CM	FS	45.7				6.68	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_011-012CM	FS	39.9				8.295	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_012-013CM	FS	42.3				6.585	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_013-014CM	FS	40.9				6.95	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_014-015CM	FS	41.7				6.67	

**TABLE 3
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SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_015-016CM	FS	44				6.045	J
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_016-017CM	FS	41.4				7.2	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_017-018CM	FS	39.3				7.09	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_018-019CM	FS	36.5				9.27	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_019-020CM	FS	40.2				8.05	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_020-022CM	FS	36.4				8.345	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_022-024CM	FS	39.2				8.915	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_024-026CM	FS	38.5				8.48	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_026-028CM	FS	37.4				9.195	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_028-030CM	FS	38.1				11.6	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_030-032CM	FS	39.1				9.55	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_032-034CM	FS	36.7				9.305	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_034-036CM	FS	35.9				11.4	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_036-038CM	FS	33.3				12.4	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_038-040CM	FS	39.5				10.4	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_040-045CM	FS	37.6				10.85	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_045-050CM	FS	40.7				8.96	
L1740284	MM-T2-C7-A	11/1/2017	MM-T2-C7-A-17_SED_050-055CM	FS	41.7				8.73	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_000-001CM	FS	46.8				4.97	J
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_001-002CM	FS	48.1				4.78	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_002-003CM	FS	51.6				4.675	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_003-004CM	FS	61.2				2.28	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_004-005CM	FS	68.4				1.395	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_005-006CM	FS	75.2				0.41	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_006-007CM	FS	80.6				0.112	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_007-008CM	FS	81.1				0.073	J

**TABLE 3
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PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
				Fraction	PERCENT		NG/G		PERCENT	
					Total	Final	Final	Total	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_008-009CM	FS	81.4				0.05	U
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_009-010CM	FS	81.8				0.05	U
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_010-011CM	FS	78.1				0.086	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_011-012CM	FS	76.7				0.0985	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_012-013CM	FS	76.5				0.1	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_013-014CM	FS	76.4				0.114	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_014-015CM	FS	79.6				0.0955	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_015-016CM	FS	80.1				0.124	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_016-017CM	FS	78.5				0.146	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_017-018CM	FS	79.7				0.102	J
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_018-019CM	FS	81.2				0.1	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_019-020CM	FS	81.7				0.0935	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_020-022CM	FS	78.5				0.1165	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_022-024CM	FS	79.7				0.113	
L1740285	MM-T3-C1	10/31/2017	MM-T3-C1-17_SED_024-026CM	FS	81				0.1835	
L1740287	OR-T1-C1-D	11/1/2017	OR-T1-C1-D-17_SED_00-01	FS	24.1				5.475	
L1740287	OR-T1-C1-D	11/1/2017	OR-T1-C1-D-17_SED_01-03	FS	37.1				5.535	
L1740287	OR-T1-C1-D	11/1/2017	OR-T1-C1-D-17_SED_03-05	FS	41.9				6.48	
L1740287	OR-T1-C1-D	11/1/2017	OR-T1-C1-D-17_SED_05-07	FS	42.8				5.89	
L1740287	OR-T1-C1-D	11/1/2017	OR-T1-C1-D-17_SED_07-10	FS	42.4				6.785	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_000-001CM	FS	44.2				5.58	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_001-002CM	FS	45.7				5.16	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_002-003CM	FS	49				4.71	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_003-004CM	FS	48.5				5.88	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_004-005CM	FS	47.9				6.24	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_005-006CM	FS	41.1				7.605	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	QC Code	Analysis Method		EPA 1631		LLOYD KAHN	
					Parameter	Unit	% Solids		Mercury	
					PERCENT		NG/G		PERCENT	
					Total		Total		Total	
					Final	Final	Final	Final	Final	Final
					Result	Qualifier	Result	Qualifier	Result	Qualifier
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_006-007CM	FS	42.4				8.535	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_007-008CM	FS	38.2				8.47	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_008-009CM	FS	37.5				9.35	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_009-010CM	FS	34				10.95	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_010-011CM	FS	35.8				10.85	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_011-012CM	FS	35.7				10.9	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_012-013CM	FS	33.6				10.95	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_013-014CM	FS	33.8				10.65	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_014-015CM	FS	37.9				10.05	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_015-016CM	FS	37.5				10.2	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_016-017CM	FS	39.3				10.65	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_017-018CM	FS	39.1				10.25	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_018-019CM	FS	36.5				10.9	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_019-020CM	FS	38.1				9.965	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_020-022CM	FS	41.7				9.46	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_022-024CM	FS	68.7				8.56	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_024-026CM	FS	41.8				8.8	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_026-028CM	FS	40.7				8.74	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_028-030CM	FS	41				8.33	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_030-032CM	FS	40.3				8.56	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_032-034CM	FS	42.9				8.245	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_034-036CM	FS	40.7				8.43	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_036-038CM	FS	42.5				8.355	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_038-040CM	FS	43.2				8.135	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_040-045CM	FS	42				8.165	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_045-050CM	FS	42.4				7.335	

**TABLE 3
DATA VALIDATION SUMMARY
2017 GEOCHRONOLOGY INTERVAL SEDIMENT CORES
PENOBSCOT RIVER ESTUARY PHASE III - ENGINEERING EVALUATION**

SDG	Location ID	Sample Date	Sample ID	Analysis Method Parameter Unit Fraction QC Code	% Solids PERCENT Total		EPA 1631 Mercury NG/G Total		LLOYD KAHN TOC PERCENT Total	
					Final Result	Final Qualifier	Final Result	Final Qualifier	Final Result	Final Qualifier
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_050-055CM	FS	46.5				6.885	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_055-060CM	FS	46.6				6.92	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_060-065CM	FS	47.2				6.585	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_065-070CM	FS	27.9				5.64	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_070-075CM	FS	51.8				5.13	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_075-080CM	FS	53.2				4.82	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_080-085CM	FS	53.4				4.91	
L1740289	OR-T3-C1-B	10/31/2017	OR-T3-C1-B-17_SED_085-090CM	FS	53.5				4.105	
L1741133	MM-T1-C1-B	11/1/2017	MM-T1-C1-B-17_SED_00-01	FS	26.7				7.105	
L1741133	MM-T1-C1-B	11/1/2017	MM-T1-C1-B-17_SED_01-03	FS	33.6				7.01	
L1741133	MM-T1-C1-B	11/1/2017	MM-T1-C1-B-17_SED_03-05	FS	32.9				7.815	
L1741133	MM-T1-C1-B	11/1/2017	MM-T1-C1-B-17_SED_05-07	FS	36.6				7.845	J
L1741133	MM-T1-C1-B	11/1/2017	MM-T1-C1-B-17_SED_07-10	FS	42.6				6.01	

Units:

NG/G = Nanogram per gram

Qualifiers:

J = Value is estimated

U = The target compound was not detected above the method detection limit

Notes:

FD = Field Duplicate

FS = Field Sample

SDG = Sample Delivery Group

TOC = Total Organic Carbon

APPENDIX C

SUPPLEMENTAL SPATIAL ANALYSIS OF SEDIMENTARY MERCURY (HG) DISTRIBUTION IN THE LOWER PENOBSCOT RIVER BASIN, ME – INFORMING SYSTEM-WIDE REMEDIAL DESIGN AND IMPLEMENTATION

**SUPPLEMENTAL SPATIAL ANALYSIS OF SEDIMENTARY MERCURY (Hg)
DISTRIBUTION IN THE LOWER PENOBSCOT RIVER BASIN, ME – INFORMING
SYSTEM-WIDE REMEDIAL DESIGN AND IMPLEMENTATION**

A revision submitted to Amec Foster Wheeler, Portland, Maine

September 2018

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1. SUMMARY

The assembled data set includes physical, geochemical and radiochemical data derived from the analytical characterization of sediment cores collected from 66 coring stations sampled during the field season of 2017 (32 cores were characterized for geochronology, and 34 were characterized for Hg only). These stations were located throughout the lower Penobscot River basin, and sampled environments included the Penobscot River (PBR), Mendall Marsh (MM), the Orland River (OR) and the Penobscot estuary (ES). The focus here was on sedimentary total mercury (Hg) in the Penobscot River system, which is the location of the HoltraChem chlor-alkali production facility, a primary point source of Hg pollution in the lower Penobscot River basin, which was in operation from 1967 to 2000. The specific locations of these stations were chosen based on three primary objectives included in the relevant Amec Foster Wheeler work order, which included:

Objective A: Some core locations were selected considering data gathered by the Penobscot River Mercury Study (PRMS) - Phase II, and the desire to collect an adequate depth of relatively undisturbed sediment sufficient to represent a relevant historical timeframe (50 to 100 years).

Objective B: Sampling in the PRMS - Phase II was focused on identifying stations where 'high fidelity cores' - defined as cores from locations where continuous and relatively undisturbed sedimentation was likely - could be collected. While this approach was appropriate for identifying locations in which a continuous geochronological record could be obtained, it provided limited data on sediment mixing and mercury (Hg) depositional patterns in more perturbed areas of the study system. The sampling conducted here was therefore also focused on broadening our understanding of depositional patterns and sediment stability throughout the study system.

Objective C: Relatedly, within Mendall Marsh, the PRMS - Phase II coring program generally targeted the edge of the marsh platform, rather than its interior, or associated intertidal and subtidal areas of the marsh. The PRMS - Phase II approach maximized the likelihood of recovering high-fidelity cores, but did not allow for assessment of sediment and Hg transport across the marsh platform. Data on sediment and Hg accumulation patterns across the marsh platform would improve understanding of the dynamics of Hg transport and deposition within the marsh, as well as the associated potential recovery rates for Mendall Marsh, overall.

To address the above work order objectives, a total of 21 cores were collected based on results provided by the PRMS - Phase II research, and a total of 45 cores (11 geochronology cores, and 34 Hg only cores) were collected in support of objectives B and C above. The data set generated was examined, processed, and organized into the following research objectives:

- (1) Quantify sedimentary inventories of total Hg in cores sampled in 2017 and compare them to values determined in replicate cores from 2009.
- (2) Quantify sediment accumulation rates in cores sampled in 2017 and compare them to values determined in replicate cores from 2009.
- (3) Quantify contemporary sedimentary fluxes of total Hg to sediments in cores sampled in 2017 and compare them to values determined in replicate cores from 2009.
- (4) Where possible, calculate apparent Hg recovery half times in cores sampled in 2017 and compare them to values determined in replicate cores from 2009.

(5) Examine, as possible, all of these variables across core transects sampled in 2017 in Mendall Marsh and the Orland River.

Sedimentary inventories of total Hg in cores collected in 2017 ranged from 4 to 1,282 mg m⁻². Differences throughout the system in terms of mean Hg inventories were apparent, and included in order of magnitudes, the Orland River (n = 16, 348 ± 210 mg m⁻²), the Penobscot River (n = 12, 346 ± 382 mg m⁻²), Mendall Marsh (n = 32, 187 ± 183 mg m⁻²), and the Penobscot estuary (n = 4, 126 ± 47 mg m⁻²) (uncertainties reported at 1σ). The large uncertainties associated with these values are not surprising, and are likely a function of both natural variability in these environments, and the specific rationale used to identify core sample locations. Comparing replicate core (2009 vs. 2017) data shows that re-sampled environments have not changed appreciably in terms of total Hg inventories during this eight year interval. Most of the variability in evidence between sample periods was found in cores from the Penobscot River. It is most likely that these differences in total Hg inventories in Penobscot River cores from 2009 and 2017 are not a reflection of net reductions in the amounts of total Hg held in these sediments over this period, but instead reflect variability in sedimentary records over small spatial scales in this dynamic river setting.

Unsurprisingly, given the range of physical and hydrological settings represented by these stations, a wide range in sediment accumulation rates was observed (0.11 to 1.35 cm y⁻¹). When comparing ¹³⁷Cs-based sediment accumulation rates available for the 13 stations sampled in both 2009 and 2017, it is clear that rates decreased at 10 of these stations (77%), and increased at three of them (23%). Given the data available, it is not possible to determine whether these differences represent actual changes in the rates of sediment delivery to these locations over this period, or simply reflect natural heterogeneities over small spatial scales.

It was possible to compare contemporary total Hg fluxes at a total of 14 stations, sampled in both 2009 and 2017. These data show that at eight stations (57%), total Hg fluxes decreased, at two stations (14%), total Hg fluxes increased, and at four stations (29%), total Hg fluxes remained unchanged. There is no evident relationship between these two total Hg flux data sets, which is likely a function of two factors, (1) natural heterogeneity between sample sites selected to repeat previous sampling, and (2) actual changes from 2009 to 2017 in sediment accumulation rates, and/or changes in total Hg concentrations on sediments deposited at these sites since 2009. As mentioned above, ¹³⁷Cs-based sediment accumulation rates decreased at 10 of 13 stations compared (77%), and increased at three of them (23%). Similarly, mean, near surface (0-3 cm) total Hg concentrations decreased at 10 of these same stations (77%), and increased at three of them (23%). It is clear from these data that reductions observed in contemporary total Hg fluxes to sediments at replicate stations is being driven, in part, by reductions in both sediment accumulation rates and the concentrations of total Hg on sediments delivered to these environments over the last eight years.

Apparent total Hg recovery half times and those calculated assuming (Hg_(∞)) of 400 ng g⁻¹ for replicate cores in 2009 and 2017 show that natural recovery is slowing in the Penobscot River system. For apparent total Hg recovery half times, nine of 11 stations (82%) compared show increasing values, and for apparent total Hg half times calculated assuming (Hg_(∞)) of 400 ng g⁻¹, eight of 10 stations (80%) compared show increasing values. Given that no large-scale active remediation has yet been conducted in the Penobscot River system, these results are not surprising. Considerable evidence was provided in the PRMS - Phase II study showing that sediment with elevated (i.e., above 400 ng g⁻¹) concentrations of total Hg were continuing to be mobilized and

transported throughout the system, either as part of a mobile pool, or as a function of sediment erosion, resuspension and transport. Slowing of natural recovery can also be seen in plots of total Hg concentrations with depth in sediment cores collected in 2017 from throughout the system. Continued inputs of above-background concentrations of total Hg produce shallow slopes of Hg concentration with depth (or time) as one approaches the sediment surface (or time 0), resulting in increasing apparent total Hg recovery half times. This scenario will not change except by either reductions in average total Hg concentrations on sediments being deposited throughout system, or by the passage of time (10's to 100's of years).

Eight core transects were established in 2017 (three in the Orland River, and five in Mendall Marsh), comprised mostly of Hg only cores (although all transects except for numbers one and five in Mendall Marsh included at least one geochronology station). All transects were oriented and sampled along lines normal to the Orland River, and marsh river (or major marsh distributary). Each group of transects were considered here as a collective (i.e., all transect data for the Orland River and Mendall Marsh). These transects were sampled to determine the presence of spatial relationships between core locations and the primary local water, sediment and total Hg sources. Lateral distance to the closest primary channel was compared to other variables, including total Hg inventories, mean surface (0-3 cm) total Hg concentrations, contemporary total Hg fluxes, and apparent total Hg recovery half times assuming $Hg_{(\infty)} = 400 \text{ ng g}^{-1}$. Given that all cores collected along transects in the Orland River were located either in open water, or on intertidal mudflats adjacent to the channel, it was not surprising to find no significant spatial relationships between lateral distances from the river channel and any of the variables considered. In this environment, there are no topographic or other physical barriers between these intertidal mudflats and the river proper. Core locations along these transects are regularly or permanently inundated by daily tidal fluctuations. This absence of lateral differentiation did allow for the direct comparison of longitudinal effects, in this case as a function of transect distance from the mouth of the Orland River. It was clear, and unsurprising, that the primary source of sediment (and total Hg) to the lower Orland River is not the Orland River watershed, but the Penobscot River. This was reflected by the clear increases in mean sediment accumulation rates, total Hg inventories, and total Hg fluxes with proximity to the mouth of the Orland River. Mean surface (0-3 cm) total Hg concentrations showed the opposite relationship, with total mean Hg surface concentrations progressively increasing with distance away from the Orland River mouth. This is likely a function of sediment transport dynamics here, where finer grained (and relatively enriched in Hg) sediments are transported a greater distance up the lower Orland River before being deposited. In Mendall Marsh, transect core locations beyond the marsh river or distributary channels are partially buffered from these water bodies by the marsh platform margins, which are typically elevated well above base flow and characterized by natural levees constructed over time by periodic inundation of the marsh. Clear relationships along Mendall Marsh core transects were evident between lateral distance from a primary channel and all of the variable considered. These data show that as lateral distance between the marsh core locations and the closest river or distributary channels decreases, total Hg inventories, mean surface concentrations, and contemporary fluxes all increase, as do the apparent total Hg recovery half times. These results are not surprising, and suggest that any remedial strategies under consideration for Mendall Marsh can utilize these proximity to source (waterways) relationships to identify areas of the marsh that do and do not require active remedial approaches, based on identified thresholds.

2. INTRODUCTION

The Penobscot River is ~425 km in length (including the West and South branches), drains a basin of approximately 22,300 km², and is the second largest river system in New England (after the Connecticut River). The Penobscot estuary extends from approximately the city of Bangor, Maine (ME), south to the city of Searsport, ME, where it meets Penobscot Bay. With a surface area of ~90 km², the Penobscot estuary is the largest in Maine, and part of one of the largest embayments on the U.S. east coast. An appreciable tidal range characterizes the estuary, with tidal influence extending 35 km up river to the city of Bangor.

Large-scale lumbering began on the Penobscot River in the 1770's, with saw mills constructed along the river and its tributaries, which contributed sawdust, edgings and bark to the waterways, a process which continued through the end of the 1950's (Cutting 1959). The presence of large quantities of sawdust has been documented at the bottom of portions of the lower Penobscot River and estuary (e.g., Haefner 1967; Shorey 1973), a condition that was also observed during field work carried out in 2009 and 2017 (associated with this project). The rise of pulp and paper mills in the lower basin began in 1889 (Goode 1934), and as this industry grew, it resulted in the discharge of large quantities of organic matter and industrial solids to the river and its tributaries. These discharges drove rapid depletion of dissolved oxygen in receiving waters. By 1960, numerous pulp and paper mills, leather plants and textile plants were located in the lower basin. In 1972, the University of Maine conducted the Penobscot River Study, which concluded that the river was periodically overloaded by oxygen-demanding wastes, and as a result was unable to support most fish species, or to be used as a municipal water supply (Penobscot River Study Team 1972). The Clean Water Act of 1972 resulted in the beginning of some pollution reduction and mitigation in the Penobscot River and estuary. Monitored pollutant loads to the river decreased by 85% and all of Maine's Department of Environmental Protection (DEP) sampling sites improved in terms of water quality and the health of macroinvertebrate communities (Davies 1999).

As with research conducted in 2009 as part of the Penobscot River Mercury Study (PRMS - Phase II), the focus of this study is total mercury (Hg), particularly that associated with sediments in discrete portions of the lower Penobscot River, Mendall Marsh, the Orland River and the Penobscot estuary. A primary, known point source of Hg pollution within the lower basin is the HoltraChem chlor-alkali production facility, which was in operation from 1967 to 2000. Total Hg concentrations measured in sediment collected from the Penobscot River upstream of the limit of tidal influence are of the order of 100 ng g⁻¹ dry weight, which is comparable to those of other New England rivers (Morgan 1998; Kamman et al. 2005). In the Penobscot estuary, total Hg concentrations in surficial, bottom sediments have been reported to range between 125 and 2,750 ng g⁻¹ (Merritt and Amirbahman 2007). The highest total Hg concentration reported in the literature is 230,000 ng g⁻¹, which corresponds to sediment collected within the HotraChem discharge zone (Morgan 1998). This Hg pollution has resulted in the widespread distribution of elevated concentrations of total Hg in sediments throughout the lower Penobscot River and estuary. In some parts of the system, the physical and geochemical setting has been conducive to the production and sustenance of highly elevated methyl Hg concentrations, with consequent and demonstrable impacts on ecosystem health (e.g., Williams and Cseh 2007; Sullivan and Kopec 2018).

The objectives of the research presented here include (Amec Foster Wheeler work order objectives are described in the Summary):

- (1) Quantify inventories of total Hg in cores sampled in 2017 and compare them to values determined in replicate cores from 2009.
- (2) Quantify sediment accumulation rates in cores sampled in 2017 and compare them to values determined in replicate cores from 2009.
- (3) Quantify contemporary fluxes of total Hg to sediments in cores sampled in 2017 and compare them to values determined in replicate cores from 2009.
- (4) Where possible, calculate apparent total Hg recovery half times in cores sampled in 2017 and compare them to values determined in replicate cores from 2009.
- (5) Examine, as possible, all variables listed above across core transects sampled in 2017 in both Mendall Marsh and the Orland River. Given that most of these cores were characterized for Hg only (not also for radionuclides), not all of the variables listed above will be possible to compare.

3. MATERIALS AND METHODS

3.1 Field and Initial Processing

During the field season of 2017, a total of 66 sediment coring stations were established and sampled throughout the lower Penobscot River, Mendall Marsh, the lower Orland River, and the Penobscot estuary. Of these, cores from 32 stations were characterized for geochronology, and cores from 34 stations were characterized for Hg only. The field campaign was organized and led by personnel from Amec Foster Wheeler. At each geochronology station, sediment cores were collected in triplicate (96 cores total) utilizing various techniques (see Amec Foster Wheeler Report, Section 2). These 66 stations were distributed from just north of Bangor, ME, south through the lower Penobscot River, and through the Penobscot estuary to include Ft. Point Cove (Figs. 1-9). The locations of these stations were chosen based in part on data gathered by the PRMS - Phase II, and to address other elements of the relevant Amec Foster Wheeler work order (see Summary).

Geochronology cores were returned to the Sedimentary and Environmental Radiochemistry Research Laboratory (SER₂L) at the University of Kentucky's (UK) Department of Earth and Environmental Sciences, or to Amec Foster Wheeler facilities for initial processing. All three sediment cores from each station were split longitudinally and inspected, described and photographed. One core was then selected from each station, with the objective being to select that core which appeared least disturbed based on observation of the sedimentary section. The other two cores from that station were then placed in storage. The core sectioning protocol was identical to that completed for the 2009 core data set (PRMS - Phase II), and produced with minimal exceptions a total of 40 sediment samples per core (1-20 cm sectioned at 1 cm, 20-40 cm sectioned at 2 cm, and 40-90 cm sectioned at 5 cm).

The quantity of sediment samples (~1,280 for geochronology cores; ~1,360 for Hg only cores, ~2,640 total), number of analyses required, and short project period (~four months), necessitated the division of labor between multiple cooperating laboratories:

- **University of Kentucky (UK):**

- Responsible for core processing and supply of samples to other laboratories (for approximately half of all cores from geochronology stations).

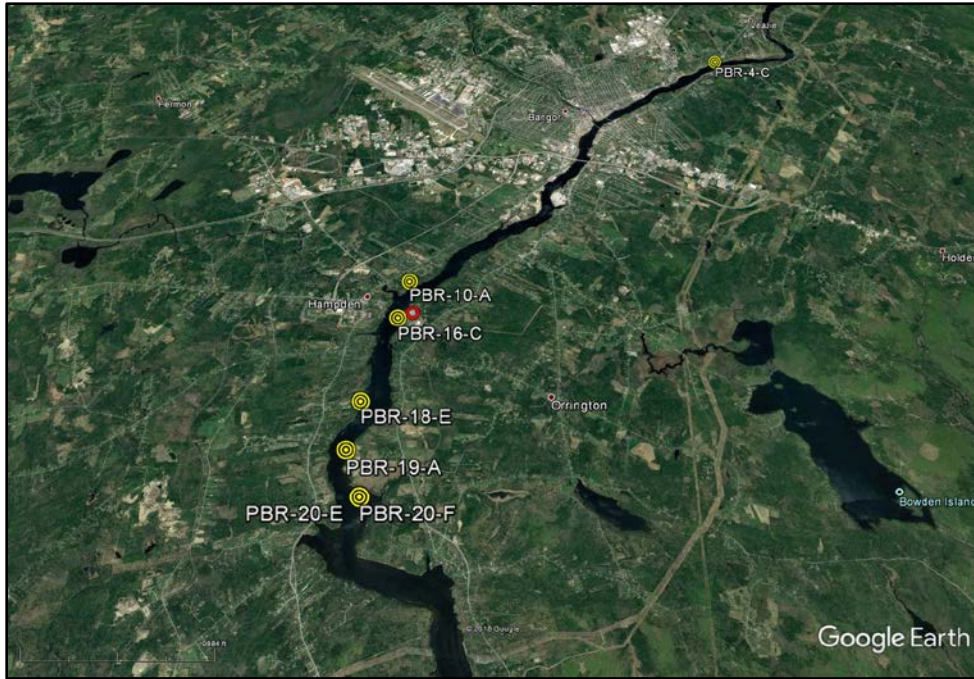


Figure 1: Sediment coring stations (2017). Yellow symbols = replicate geochronology cores (sampled in 2009, 2017), and red circle = location of the HoltraChem facility. Image from Google Earth (2018).

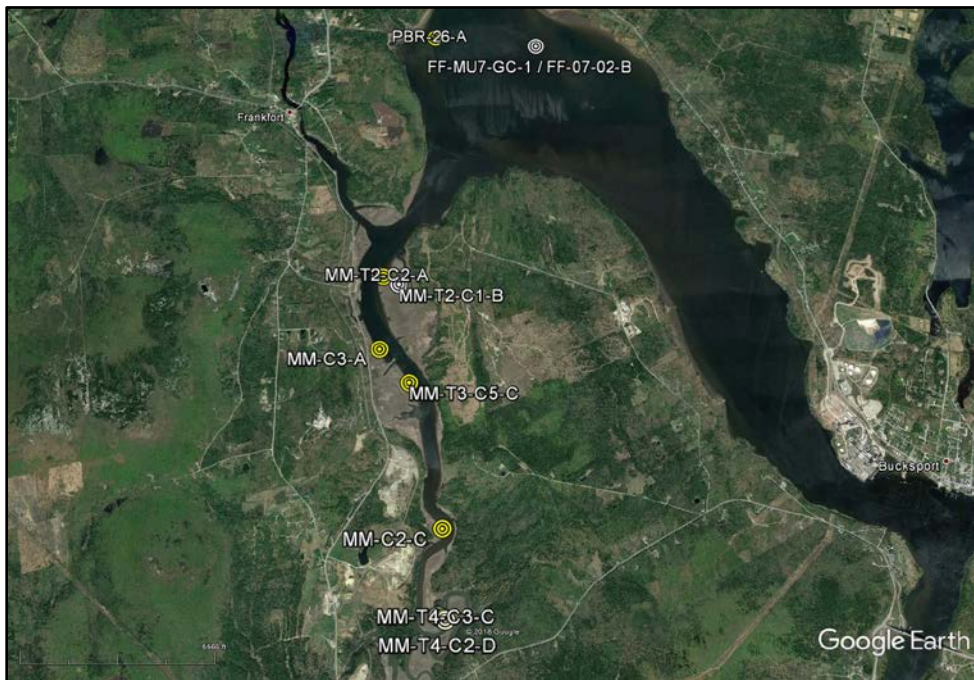


Figure 2: Sediment coring stations (2017). Yellow symbols = replicate geochronology cores (sampled in 2009, 2017), and white symbols = non-replicate geochronology cores. Image from Google Earth (2018).

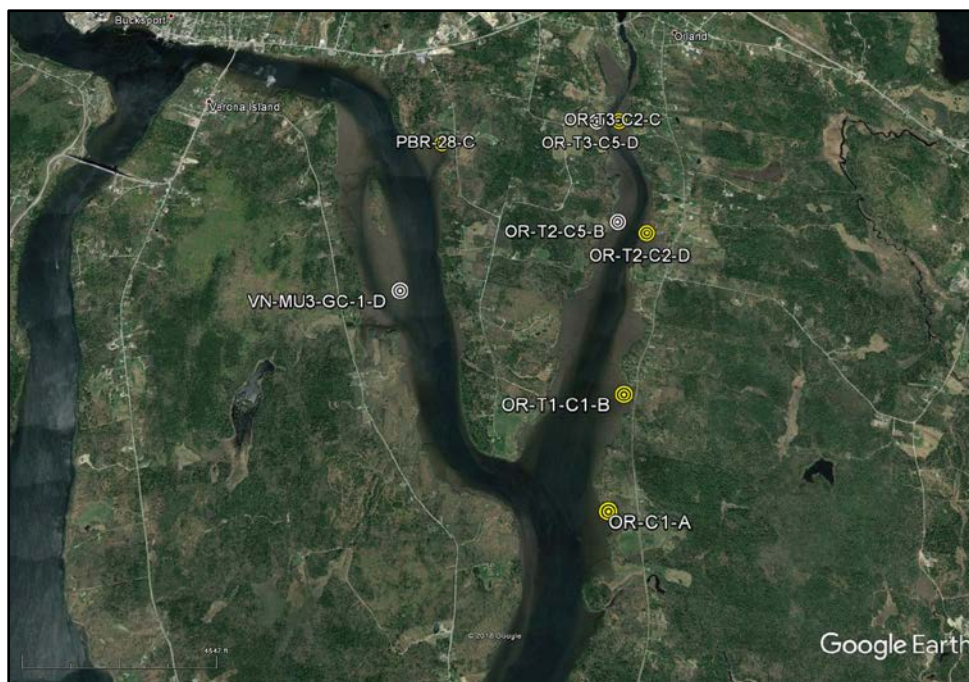


Figure 3: Sediment coring stations (2017). Yellow symbols = replicate geochronology cores (sampled in 2009, 2017), and white symbols = non-replicate geochronology cores. Image from Google Earth (2018).



Figure 4: Sediment coring stations (2017). Yellow symbols = replicate geochronology cores (sampled in 2009, 2017), and white symbols = non-replicate geochronology cores. Image from Google Earth (2018).



Figure 5: Sediment coring stations (2017), highlighting core transects from northern Mendall Marsh. Yellow symbols = replicate geochronology cores (sampled in 2009, 2017), white symbols = non-replicate geochronology cores, and red symbols = Hg only cores. Image from Google Earth (2018).

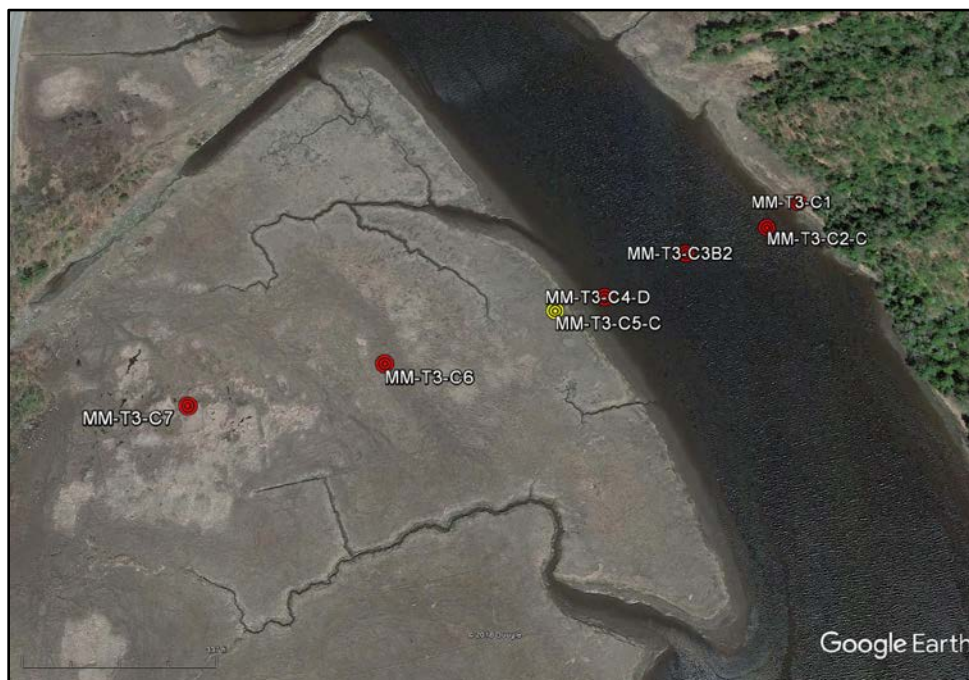


Figure 6: Sediment coring stations (2017), highlighting core transects from central Mendall Marsh. Yellow symbols = replicate geochronology cores (sampled in 2009, 2017), and red symbols = Hg only cores. Image from Google Earth (2018).



Figure 7: Sediment coring stations (2017), highlighting core transects from southern Mendall Marsh. Yellow symbols = replicate geochronology cores (sampled in 2009, 2017), white symbols = geochronology cores, and red symbols = Hg only cores. Image from Google Earth (2018).

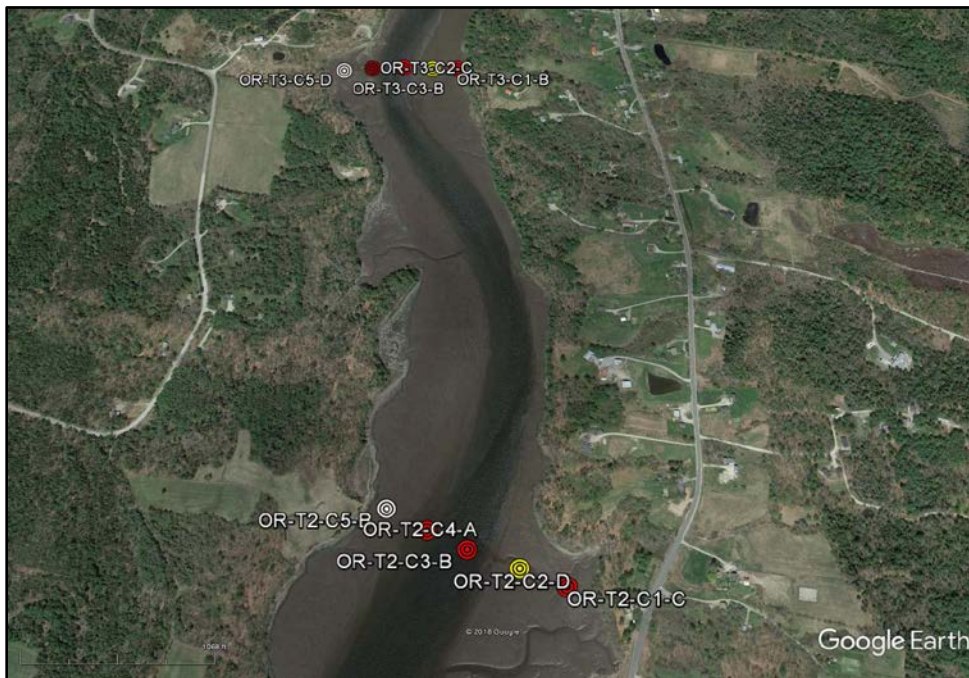


Figure 8: Sediment coring stations (2017), highlighting core transects from the northern and central Orland River. Yellow symbols = replicate geochronology cores (sampled in 2009, 2017), white symbols = geochronology cores, and red symbols = Hg only cores. Image from Google Earth (2018).



Figure 9: Sediment coring stations (2017), highlighting core transect from the southern Orland River. Yellow symbols = replicate geochronology cores (sampled in 2009, 2017), and red symbols = Hg only cores. Image from Google Earth (2018).

- Responsible for all sediment grain size analyses.
- Responsible for the determination of sedimentary particulate organic carbon (POC) in approximately half of all cores from geochronology stations.
- Responsible for radionuclide characterization by gamma and alpha spectrometry in approximately one third of all cores from geochronology stations.

• **Texas A&M University at Galveston (TAMUG):**

- Responsible for the determination of sedimentary POC in approximately half of all cores from geochronology stations.
- Responsible for radionuclide characterization by gamma and alpha spectrometry in approximately one third of all cores from geochronology stations.

• **Flett Research Ltd. (FLETT):**

- Responsible for the determination of all total Hg concentrations from geochronology stations.
- Responsible for radionuclide characterization by gamma and alpha spectrometry in approximately one third of all cores from geochronology stations.

• **Other Contract Laboratories:**

- Amec Foster Wheeler cooperated with other contract laboratories as needed for various analyses to meet the project timeline, as described elsewhere (see Amec Foster Wheeler Report, Section 2).

3.2 Physical and Chemical Variables

Sediments from each core interval were weighed, dried, and re-weighed to determine a range of physical variables, including dry bulk density (B_d), fraction of water (f_w), sediment grain density (ρ_s), sediment porosity (ϕ), and sediment mass depths and cumulative mass depths. The calculations for

each of these variables are described in Appendix 1, and their values are reported elsewhere (see Amec Foster Wheeler Report, Appendix B). Sediment textures were determined in geochronology cores only by quantifying the mineral grain size distribution and sand : silt : clay fractions as defined by the Wentworth Scale (Wentworth 1922). Texture samples were dried at ~100 °C for 24 h, gently disaggregated, wet-sieved through 2 and 0.5 mm sieves and treated with dilute H₂O₂ to destroy organic binding agents. Samples were analyzed using a Malvern Mastersizer, a laser-optical characterization instrument capable of resolving particles over a size range of 0.02 to 2000 μm.

Sedimentary particulate organic carbon (POC) was determined by UK and TAMUG via elemental analysis according to methods given in Santschi et al. (2001). Concentrations of total Hg were determined by FLETT using a DMA-80 analyzer (Milestone) according to EPA Method 7473 (<http://www.flett-research.ca/Webdoc2.htm>).

3.3 Radiochemistry

These methods pertain to analyses carried out at UK, radiochemical methods employed by partner laboratories involved in the project are given elsewhere (see Amec Foster Wheeler Report, Section 2 and Appendix B). High-resolution gamma spectrometry was employed to resolve ¹³⁷Cs ($t_{1/2} = 30$ y, $E_{\gamma} = 661$ keV) using Canberra HP-Ge well detectors and multi-channel analyzer, model DSA-1000. Samples were contained in plastic test tubes (inner diameter 1.3 cm, height 9.4 cm), and a standard (NIST, SRM #4357) was prepared and run on each detector in geometries identical to those for sediment samples to determine representative efficiencies. Efficiency errors based on standards were less than $\pm 5\%$, and samples were counted to reach a goal standard deviation of $< 20\%$ (all samples were stopped at 24 hours in consideration of the total number of samples to be counted over the project period). Alpha spectrometry was employed to resolve ²¹⁰Pb ($t_{1/2} = 22.3$ y) via ²¹⁰Po using a Canberra integrated alpha spectrometer, model 7200. Lead-210 samples were spiked with a certified ²⁰⁹Po tracer (Isotope Products Laboratory, #6209-100N) and completely digested (HF, HCl, HNO₃) over heat. Ascorbic acid was then added to bind free Fe (III), and a silver disk was added to the solution over heat to provide a substrate for the spontaneous deposition of polonium isotopes (Santschi et al. 1999; Yeager et al. 2004, 2007, 2012). Unsupported, or “excess” ²¹⁰Pb (²¹⁰Pb_{xs}) was determined by $^{210}\text{Pb}_{\text{xs}} = \text{Total } ^{210}\text{Pb} - ^{226}\text{Ra-supported } ^{210}\text{Pb}$, where the supported ²¹⁰Pb fraction was estimated as the mean total ²¹⁰Pb at the bottom of each sediment core profile.

3.4 Sediment Accumulation Modeling

Sediment accumulation rates have been determined in a range of terrestrial and aquatic settings using the bomb-fallout radionuclide ¹³⁷Cs (e.g., DeLaune et al. 1978; Edgington et al. 1991; Fuller et al. 1999; Yeager et al. 2006), and are determined here by:

$$S = (D_{\text{pk}}/t) \quad (1)$$

where: S = sediment accumulation rate (cm y⁻¹), D_{pk} = depth at which the maximum ¹³⁷Cs activity concentration occurs (1963), or alternatively the first time that ¹³⁷Cs can be determined (1952), and t = time. This model assumes (1) limited vertical mobility of ¹³⁷Cs in sediments; (2) that vertical mixing of sediments is negligible; and (3) that sedimentation is constant over the interval from surface to peak depth of ¹³⁷Cs (or its first appearance) (Huntley et al. 1995; Winkels et al. 1998; Valero-Garces et al. 1999).

As with ¹³⁷Cs, ²¹⁰Pb has been widely employed to determine sediment geochronology and rates of sediment accumulation in many terrestrial and aquatic settings (e.g., Carpenter et al. 1985; Schuler

et al. 1991; Santschi et al. 1999; Yeager et al. 2004). Because there are significant differences in the sampled environments, particularly in terms of the frequency and/or duration of inundation, more than one modeling approach using ^{210}Pb is appropriate. For parts of the system where inundation is periodic, and controlled principally by the tidal cycle and to a lesser extent by river stage (Penobscot River, Mendall Marsh, Orland River), sediment accumulation rates were determined using the constant rate of supply (CRS) model (Appleby and Oldfield 1978, 1992; Appleby 2008). This model is appropriate for settings such as these, where ^{210}Pb fallout may be constant (assumed), but sediment accumulation is not. The $^{210}\text{Pb}_{\text{xs}}$ distribution as a function of mass depth is:

$$^{210}\text{Pb}_{\text{xs}} = F_{210}e^{-\lambda t}/S_a \quad (2)$$

where: F_{210} = flux of ^{210}Pb , λ = ^{210}Pb decay constant (0.031 y^{-1}), t = time, and S_a = sediment mass accumulation rate (MAR) ($\text{g cm}^{-2} \text{ y}^{-1}$). The sediment MAR as a function of mass depth is:

$$S_a = \Delta m/\Delta t \quad (3)$$

where: m = mass depth (g cm^{-2}). For those parts of the system where inundation is constant (lower estuary, main river channels) the constant flux-constant sedimentation (CF-CS) model (Robbins 1978) was utilized, which calculates sediment accumulation rates assuming steady state conditions and a relatively constant porosity by:

$$[^{210}\text{Pb}_{\text{xs}}(z)] = [^{210}\text{Pb}_{\text{xs}}(0)]\exp(-\alpha z) \quad (4a)$$

$$\alpha = (\lambda/S) \quad (4b)$$

where: $[^{210}\text{Pb}_{\text{xs}}(z)]$ and $[^{210}\text{Pb}_{\text{xs}}(0)]$ represent $^{210}\text{Pb}_{\text{xs}}$ concentrations at depth z and at the sediment interface, respectively.

Because the year (1967) when the HoltraChem facility became operational, and also released the largest quantities of total Hg into the Penobscot River is known, total Hg can also be utilized as an additional chronological marker. This approach has been shown to be reasonable based on the strong correlations between sediment accumulation rates determined by radionuclides (^{137}Cs , ^{210}Pb , $^{239,240}\text{Pu}$) and total Hg, as shown in the PRMS - Phase II study, and Yeager et al. (2018b). As such, sediment accumulation rates have also been determined via equation (1), using total Hg and $t = (2017-1967) = 50 \text{ y}$. Assumptions associated with this approach are the same as those described previously using ^{137}Cs .

4. RESULTS AND DISCUSSION

Tabular data, including all variables for all cores (geochronology and Hg only) are provided elsewhere (see Amec Foster Wheeler Report, Section 4).

4.1 Objective 1: Sedimentary Inventories of Total Hg

Sedimentary inventories of total Hg (ng cm^{-2}) were calculated to 90 cm, or the end of each core (EOC) using:

$$I_{\text{Hg}} = \Sigma[\text{sediment interval (cm)} \times (1 - \varphi \times \rho_s) \times [\text{Hg}] (\text{ng g}^{-1})] \quad (5)$$

where: φ = porosity (%), and ρ_s = sediment grain density (g cm^{-3}). Differences throughout the study system in terms of mean total Hg inventories are apparent, and include in order of magnitudes the Orland River ($n = 16, 348 \pm 210 \text{ mg m}^{-2}$), the Penobscot River ($n = 12, 346 \pm 382 \text{ mg m}^{-2}$), Mendall

Marsh ($n = 32, 187 \pm 183 \text{ mg m}^{-2}$), and the Penobscot estuary ($n = 4, 126 \pm 47 \text{ mg m}^{-2}$) (uncertainties reported at 1σ). The large uncertainties associated with these mean total Hg inventory values were not surprising, and are likely a function of both natural variability in these environments and the specific rationale used to identify core sample locations. Sedimentary inventories of total Hg in cores collected in 2017 ranged from 4 to $1,282 \text{ mg m}^{-2}$ (Fig. 10). Comparing replicate core (2009 vs. 2017) locations only (Fig. 11) shows that re-sampled environments have not changed appreciably in terms of total Hg inventories during this eight year period. As can be seen in Figure 12, most variability between sample periods is found in cores from the Penobscot River. It is most likely that these differences in total Hg inventories in Penobscot River cores from 2009 and 2017 do not reflect net reductions in the amounts of total Hg held in these sediments over this period, but instead reflect the variability in sedimentary records over small spatial scales in this dynamic river setting.

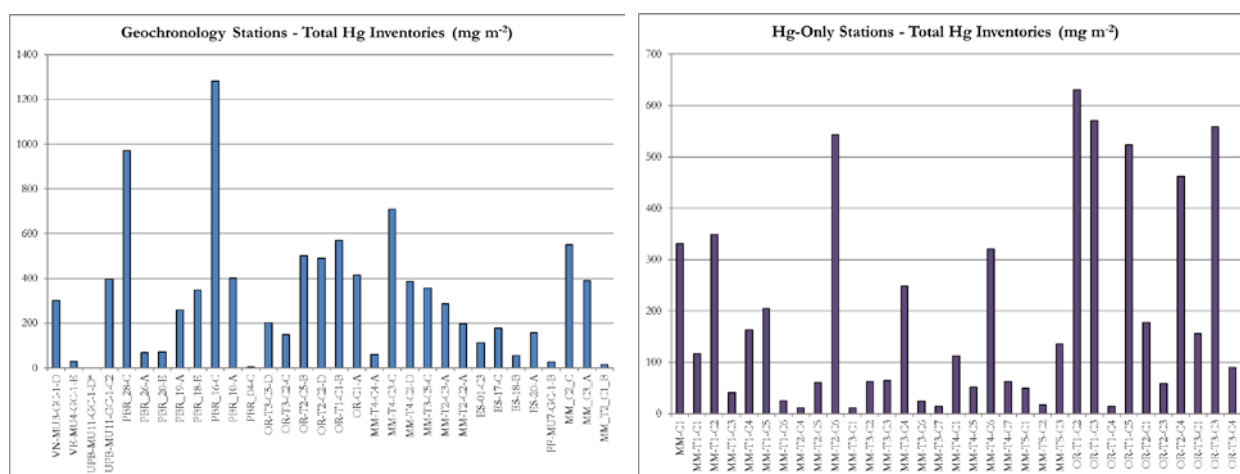


Figure 10: Total Hg inventories in 2017 geochronology (left) and Hg only (right) cores. All values calculated to 90 cm or end of core (EOC) (see Table 3).

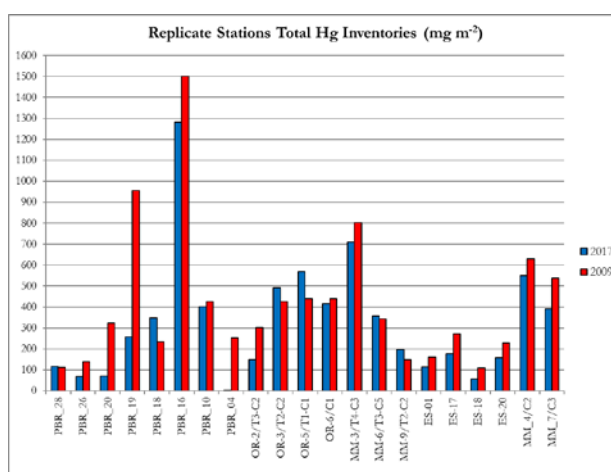


Figure 11: Comparison of total Hg inventories in 2009 and 2017 replicate cores. For cores from different years of unequal total length, total Hg inventories were calculated to the shortest depth resolved between the two cores to produce data from each core representing equal depths in section.

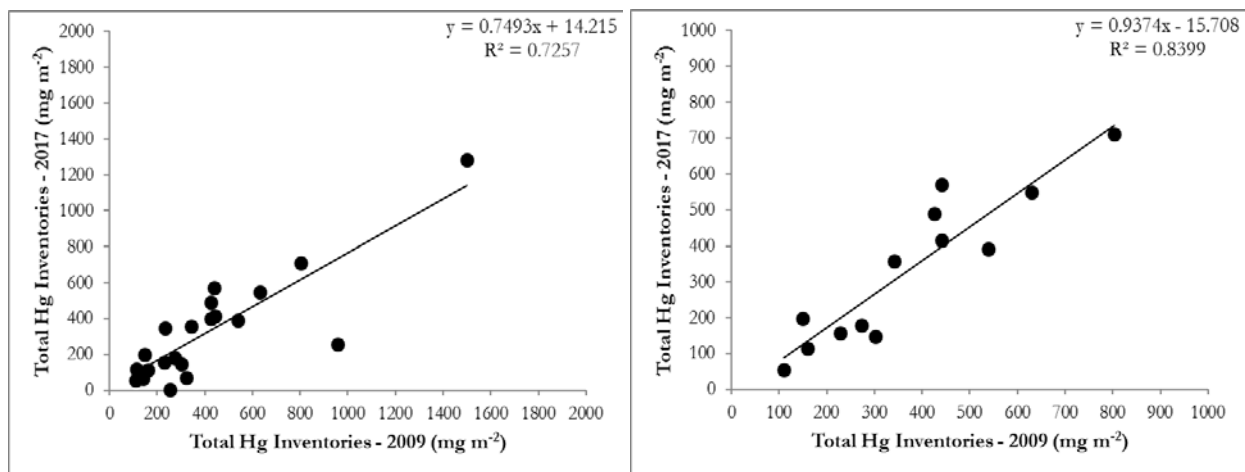


Figure 12: Comparison of total Hg inventories in 2009 and 2017 for all replicate cores (left), and for all replicate cores except those from the Penobscot River (right). For cores from different years of unequal total length, total Hg inventories were calculated to the shortest depth resolved between the two cores to produce data from each core representing equal depths in section.

4.2 Objective 2: Sediment Accumulation Rates

Determination of sediment accumulation rates must consider the effects of vertical mixing. Mixing can distort, broaden and/or displace the peaks of chronological markers, including the radionuclides and total Hg considered here (e.g., Santschi et al. 1999, 2001, 2017). Such effects can be estimated from peak broadening or profile irregularities of chronological markers, the nature of sediment porosity profiles, and variability of mineral grain size distribution profiles. As was the case in cores collected in 2009 (e.g., Santschi et al. 2017; Yeager et al. 2018b), data from cores collected in 2017 reflect some degree of near-surface mixing system-wide, as would be expected, however significant and extensive mixing was generally limited to sub-sets of sediment cores collected either from stations in the Penobscot River, or from river channel environments sampled in Mendall Marsh and the Orland River. In well-mixed sediments, porosity profiles often exhibit a gradient or are erratic with considerable variability in evidence over depth, whereas in relatively un-mixed cores, porosity profiles tend to be more uniform over depth (e.g., Mulsow et al. 1998; Meysman et al. 2007; Fig. 13). In terms of grain size distribution profiles, in well-mixed sediments, grain size is often erratic with variability in evidence over depth, whereas in relatively un-mixed sediments, grain size tends to be more uniform over depth (e.g., Flemming 2007; Woszczyk et al. 2014; Fig. 14).

To determine each core's suitability for modeling sediment accumulation rates, each was examined (where possible) in terms of physical variables (porosity, grain size), radionuclides (^{137}Cs , ^{210}Pb) and total Hg. A summary of these determinations, along with estimated mixing depths (where possible - geochronology cores only) are listed in Table 1, along with other relevant core station information. Overall, agreement between the various radionuclides (^{137}Cs , ^{210}Pb) and total Hg profiles in terms of derived sediment accumulation rates was not as strong as for the 2009 data set (Fig. 15), this is particularly true when comparing rates derived using $^{210}\text{Pb}_{\text{xs}}$ and ^{137}Cs (Fig. 16b), and total Hg (Fig. 16c). However, excellent agreement was observed between rates determined by ^{137}Cs and total Hg (Fig. 16a), similar to the 2009 data set, where sediment accumulation rates determined

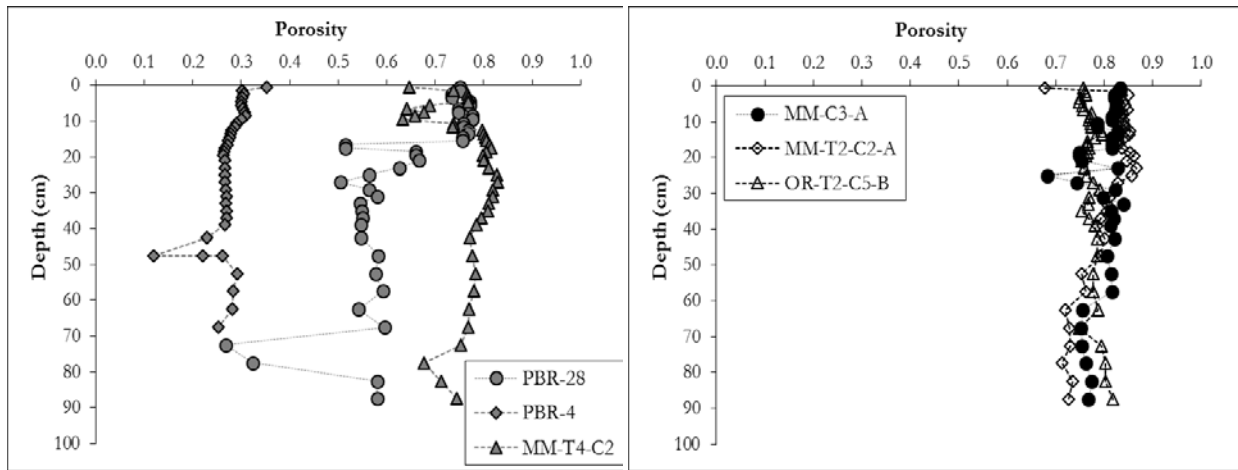


Figure 13: Comparison of example sediment porosity profiles for cores characterized as extensively mixed (left) vs. those cores characterized as not extensively mixed (right).

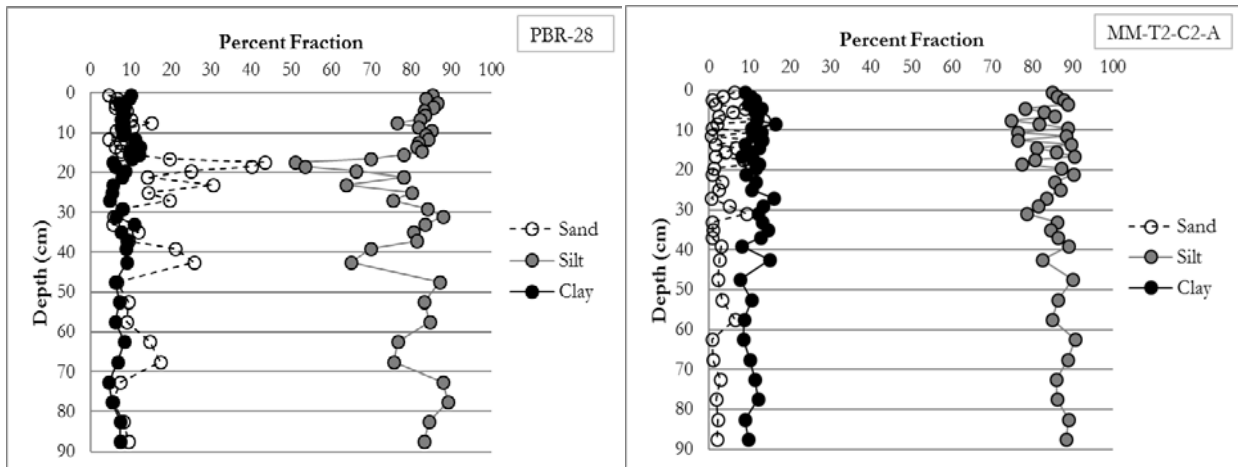


Figure 14: Comparison of example sediment grain size distributions (sand : silt : clay) for a core characterized as extensively mixed (left) vs. a core characterized as not extensively mixed (right).

by these two tracers were in the strongest agreement of those compared. Given the strong relationship between sediment accumulation rates derived using ^{137}Cs and total Hg, total Hg is utilized here as a reliable tracer (as with 2009 data set, Yeager et al. 2018b), allowing sediment accumulation rates to also be derived from a sub-set of the Hg only sediment cores (with identifiable subsurface peaks in total Hg concentration) (Fig. 17). Unsurprisingly, given the range of physical and hydrological settings represented by these stations, a wide range in sediment accumulation rates was observed (0.11 to 1.35 cm y^{-1}) (based on ^{137}Cs for geochronology cores, and total Hg for Hg-only cores) (Table 2). When comparing ^{137}Cs -based sediment accumulation rates available for the 13 stations sampled in both 2009 and 2017 (Fig. 18), it is clear that sediment accumulation rates decreased at 10 of these stations (77%), and increased at three of them (23%). Given the data available, it is not possible to determine whether these differences represent actual changes in the rates of sediment delivery to these stations over this eight year period, or simply reflect natural heterogeneities over small spatial scales.

Table 1: Summary data for all sediment cores, including type of analyses performed, inundation settings, data suitability for modeling, total lengths analyzed, and estimated mixed depths.

Station	Core type	Permanently inundated (PI) or not (NPI)	Suitable for modeling	Total core length (cm)	Estimated mixed depth (cm)
VN-MU3-GC-1-D	Geochronology	NPI	Yes	90	~25
VE-MU4-GC-1-E	Geochronology	NPI	No	65	~65
UPB-MU11-GC-1-D	Geochronology	PI	Yes	70	~20
UPB-MU11-GC-1-C2	Geochronology	PI	No	90	~35
FF-MU7-GC-1-B	Geochronology	PI	No	90	~90
PBR-28-C	Geochronology	NPI	No	90	~45
PBR-26-A	Geochronology	NPI	No	90	~40
PBR-20-E	Geochronology	NPI	No	50	~50
PBR-19-A	Geochronology	NPI	Yes	60	~15
PBR-18-E	Geochronology	NPI	Yes	60	~20
PBR-16-C	Geochronology	NPI	Yes	55	~5
PBR-10-A	Geochronology	NPI	Yes	55	~20
PBR-04-C	Geochronology	NPI	No	70	~70
OR-T3-C5-D	Geochronology	NPI	Yes	75	~15
OR-T3-C2-C	Geochronology	NPI	No	90	~90
OR-T2-C5-B	Geochronology	NPI	Yes	90	~25
OR-T2-C2-D	Geochronology	NPI	Yes	90	~25
OR-T1-C1-B	Geochronology	NPI	Yes	90	~15
OR-C1-A	Geochronology	NPI	Yes	80	~20
MM-T4-C4-A	Geochronology	NPI	Yes	90	~2
MM-T4-C3-C	Geochronology	NPI	No	90	~90
MM-T4-C2-D	Geochronology	NPI	No	90	~90
MM-T3-C5-C	Geochronology	NPI	Yes	90	~15
MM-T2-C3-A	Geochronology	NPI	Yes	90	~10
MM-T2-C2-A	Geochronology	NPI	Yes	90	~10
MM-C2-C	Geochronology	NPI	Yes	90	~10
MM-C3-A	Geochronology	NPI	Yes	90	~2
MM-T2-C1-B	Geochronology	NPI	No	85	~35
ES-01-C3	Geochronology	PI	Yes	90	~2
ES-17-C	Geochronology	PI	Yes	90	~10
ES-18-B	Geochronology	PI	No	75	--
ES-20-A	Geochronology	PI	Yes	90	~5
MM-C1-C	Hg only	NPI	No	75	--
MM-T1-C1	Hg only	NPI	No	75	--
MM-T1-C2	Hg only	NPI	No	75	--
MM-T1-C3	Hg only	PI	No	75	--
MM-T1-C4	Hg only	NPI	Yes	85	--
MM-T1-C5	Hg only	NPI	Yes	85	--
MM-T1-C6	Hg only	NPI	Yes	85	--
MM-T2-C4	Hg only	PI	No	90	--
MM-T2-C5	Hg only	PI	No	90	--
MM-T2-C6	Hg only	PI	Yes	90	--

Table 1: Continued.

Station	Core type	Permanently inundated (PI) or not (NPI)	Suitable for modeling	Total length (cm)
MM-T2-C7	Hg only	NPI	Yes	90
MM-T3-C1	Hg only	NPI	No	26
MM-T3-C2	Hg only	PI	No	90
MM-T3-C3	Hg only	PI	Yes	80
MM-T3-C4	Hg only	NPI	No	80
MM-T3-C6	Hg only	NPI	Yes	70
MM-T3-C7	Hg only	NPI	Yes	70
MM-T4-C1	Hg only	NPI	Yes	85
MM-T4-C5	Hg only	NPI	Yes	85
MM-T4-C6	Hg only	NPI	Yes	80
MM-T4-C7	Hg only	NPI	No	90
MM-T5-C1	Hg only	NPI	Yes	90
MM-T5-C2	Hg only	NPI	No	65
MM-T5-C3	Hg only	NPI	Yes	80
OR-T1-C2	Hg only	NPI	Yes	90
OR-T1-C3	Hg only	NPI	Yes	90
OR-T1-C4	Hg only	PI	No	90
OR-T1-C5	Hg only	NPI	Yes	90
OR-T2-C1	Hg only	NPI	Yes	65
OR-T2-C3	Hg only	PI	No	70
OR-T2-C4	Hg only	NPI	Yes	90
OR-T3-C1	Hg only	NPI	Yes	90
OR-T3-C3	Hg only	NPI	No	90
OR-T3-C4	Hg only	NPI	Yes	85

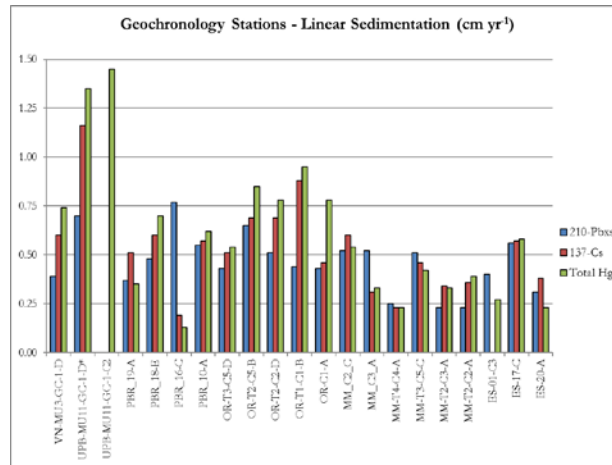


Figure 15: Linear sediment accumulation rates determined for all geochronology stations via ^{137}Cs , $^{210}\text{Pb}_{\text{ss}}$, and total Hg.

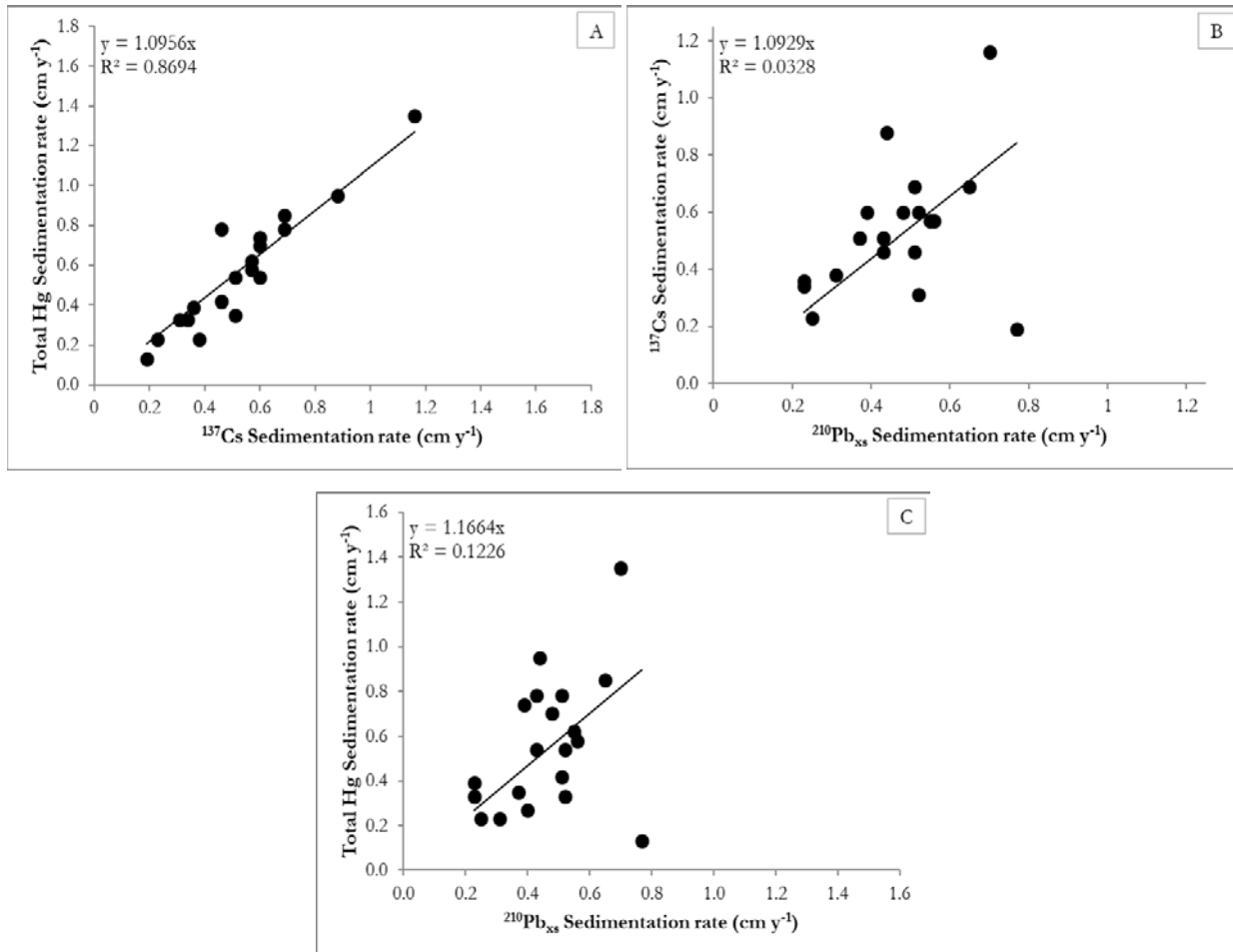


Figure 16: Comparisons of sediment accumulation rates derived by ^{137}Cs and total Hg (A); by $^{210}\text{Pb}_{\text{xs}}$ and ^{137}Cs (B); and by $^{210}\text{Pb}_{\text{xs}}$ and total Hg (C).

4.3 Objective 3: Contemporary Total Hg Fluxes

Estimates of contemporary total Hg fluxes ($\text{ng cm}^{-2} \text{y}^{-1}$) to sediments are presented using the mean concentrations of total Hg (ng g^{-1}) in the upper 3 cm of sediment cores multiplied by mass accumulation rates (MAR) ($\text{g cm}^{-2} \text{y}^{-1}$) determined either by ^{137}Cs (geochronology cores) or total Hg (Hg only cores). The mean total Hg concentration over the 0-3 cm interval was utilized here as that corresponds to the average active mixed depth as resolved by the PRMS study (e.g., PRMS, 2013; Yeager et al., 2018b). Figure 19 shows contemporary total Hg fluxes to sediments in geochronology and Hg only cores. A total of 14 stations, sampled in both 2009 and 2017, are available to compare total Hg fluxes (Fig. 20). These data show that at eight stations (57%), fluxes decreased, at two stations (14%), fluxes increased, and at four stations (29%), fluxes remained unchanged. A strong relationship between these two data sets is not present (Fig. 20), which is likely a function of two factors, (1) natural heterogeneity between sample sites selected to repeat previous sampling, and (2) actual changes from 2009 to 2017 in sediment accumulation rates (see sec. 4.2), and/or changes in total Hg concentrations on sediments deposited at these sites since 2009. A quantitative assessment of natural heterogeneity between sites sampled eight years apart is not possible with the data

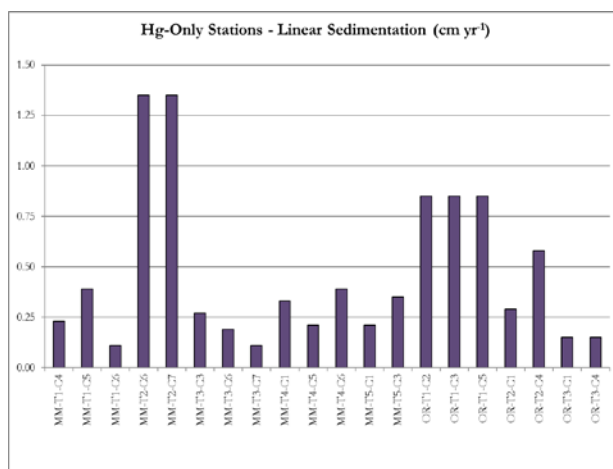


Figure 17: Linear sediment accumulation rates determined for Hg only stations via total Hg.

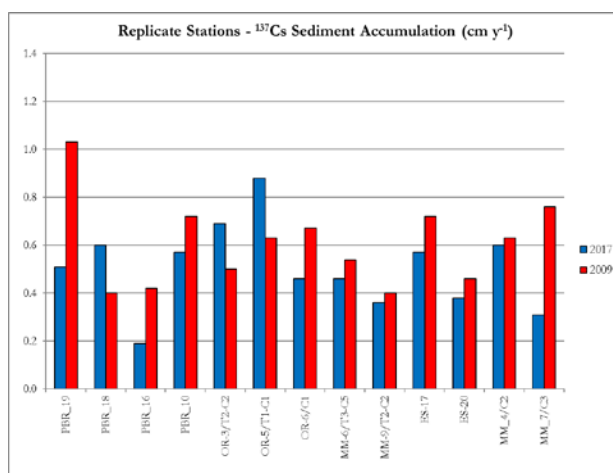


Figure 18: ¹³⁷Cs-based sediment accumulation rates at replicate stations (2009, 2017).

assembled here. However, an examination of 13 of these stations where both ¹³⁷Cs-based sediment accumulation rates and mean, near surface total Hg concentration data (0-3 cm) are available is possible, and provides some insights. As previously mentioned, ¹³⁷Cs-based sediment accumulation rates for these 13 stations (Fig. 18) show that sediment accumulation rates decreased at 10 of these stations (77%), and increased at three of them (23%). Figure 21 shows mean, near surface total Hg concentration data for these 13 stations, and it is clear that Hg concentrations decreased at 10 of these stations (77%), and increased at three of them (23%) (Note: while proportions and directions of change for both variables compared are the same, the specific stations where these changes were observed are not). It is clear from the data that reductions observed in contemporary total Hg fluxes to bottom sediments at replicate stations is being driven, in part, by both reductions in sediment accumulation rates, and reductions in the concentrations of total Hg on sediments delivered to these environments over the last eight years.

Table 2: Summary of sediment accumulation rates for each station as determined by $^{210}\text{Pb}_{\text{xs}}$, ^{137}Cs and total Hg (mixed stations are not included, see Table 1), and contemporary total Hg fluxes.

Station	Core type	$^{210}\text{Pb}_{\text{xs}}$ accumulation rates ($\text{cm y}^{-1}; g$ $\text{cm}^{-2} \text{y}^{-1}$)	^{137}Cs accumulation rate ($\text{cm y}^{-1}; g$ $\text{cm}^{-2} \text{y}^{-1}$)	Total Hg accumulation rate ($\text{cm y}^{-1}; g$ $\text{cm}^{-2} \text{y}^{-1}$)	Total Hg fluxes (ng $\text{cm}^{-2} \text{y}^{-1}$)
VN-MU3-GC-1-D	Geochronology	0.39; 0.29	0.60; 0.43	0.74; 0.53	270.04
UPB-MU11-GC-1-D	Geochronology	0.70; 1.82	1.16; 2.92	1.35; 3.40	1,968.08
UPB-MU11-GC-1-C2	Geochronology	NA	NA	1.45; 2.66	NA
PBR-19-A	Geochronology	0.37; 0.20	0.51; 0.22	0.35; 0.14	258.28
PBR-18-E	Geochronology	0.48; 0.20	0.60; 0.24	0.70; 0.28	204.24
PBR-16-C	Geochronology	0.77; 0.56	0.19; 0.16	0.13; 0.13	165.28
PBR-10-A	Geochronology	0.55; 0.33	0.57; 0.34	0.62; 0.36	290.36
OR-T3-C5-D	Geochronology	0.43; 0.26	0.51; 0.27	0.54; 0.29	182.25
OR-T2-C5-B	Geochronology	0.65; 0.33	0.69; 0.37	0.85; 0.47	263.07
OR-T2-C2-D	Geochronology	0.51; 0.30	0.69; 0.38	0.78; 0.43	394.06
OR-T1-C1-B	Geochronology	0.44; 0.32	0.88; 0.45	0.95; 0.49	368.55
OR-C1-A	Geochronology	0.43; 0.49	0.46; 0.32	0.78; 0.50	256.96
MM-T4-C4-A	Geochronology	0.25; 0.12	0.23; 0.07	0.23; 0.07	21.77
MM-T3-C5-C	Geochronology	0.51; 0.23	0.46; 0.22	0.42; 0.20	144.10
MM-T2-C3-A	Geochronology	0.23; 0.17	0.34; 0.24	0.33; 0.24	181.44
MM-T2-C2-A	Geochronology	0.23; 0.11	0.36; 0.14	0.39; 0.15	81.20
MM-C2-C	Geochronology	0.52; 0.25	0.60; 0.30	0.54; 0.28	176.40
MM-C3-A	Geochronology	0.52; 0.25	0.31; 0.12	0.33; 0.13	19.32
ES-01-C3	Geochronology	0.40; 0.53	NA	0.27; 0.12	NA
ES-17-C	Geochronology	0.56; 0.28	0.57; 0.25	0.58; 0.25	138.75
ES-20-A	Geochronology	0.31; 0.14	0.38; 0.26	0.23; 0.17	159.64
MM-T1-C4	Hg only	NA	NA	0.23; 0.11	105.49
MM-T1-C5	Hg only	NA	NA	0.39; 0.13	60.58
MM-T1-C6	Hg only	NA	NA	0.11; 0.01	14.19
MM-T2-C6	Hg only	NA	NA	1.35; 1.71	1,251.72
MM-T2-C7	Hg only	NA	NA	1.35; 3.31	115.85
MM-T3-C3	Hg only	NA	NA	0.27; 0.16	32.80
MM-T3-C6	Hg only	NA	NA	0.19; 0.05	10.70
MM-T3-C7	Hg only	NA	NA	0.11; 0.02	3.24
MM-T4-C1	Hg only	NA	NA	0.33; 0.14	75.88
MM-T4-C5	Hg only	NA	NA	0.21; 0.07	22.26
MM-T4-C6	Hg only	NA	NA	0.39; 0.18	140.76
MM-T5-C1	Hg only	NA	NA	0.21; 0.04	23.60
MM-T5-C3	Hg only	NA	NA	0.35; 0.10	59.70
OR-T1-C2	Hg only	NA	NA	0.85; 0.66	466.62
OR-T1-C3	Hg only	NA	NA	0.85; 0.48	332.16
OR-T1-C5	Hg only	NA	NA	0.85; 0.51	371.79
OR-T2-C1	Hg only	NA	NA	0.29; 0.15	121.35
OR-T2-C4	Hg only	NA	NA	0.58; 0.31	247.69
OR-T3-C1	Hg only	NA	NA	0.15; 0.08	49.60
OR-T3-C4	Hg only	NA	NA	0.15; 0.09	64.26

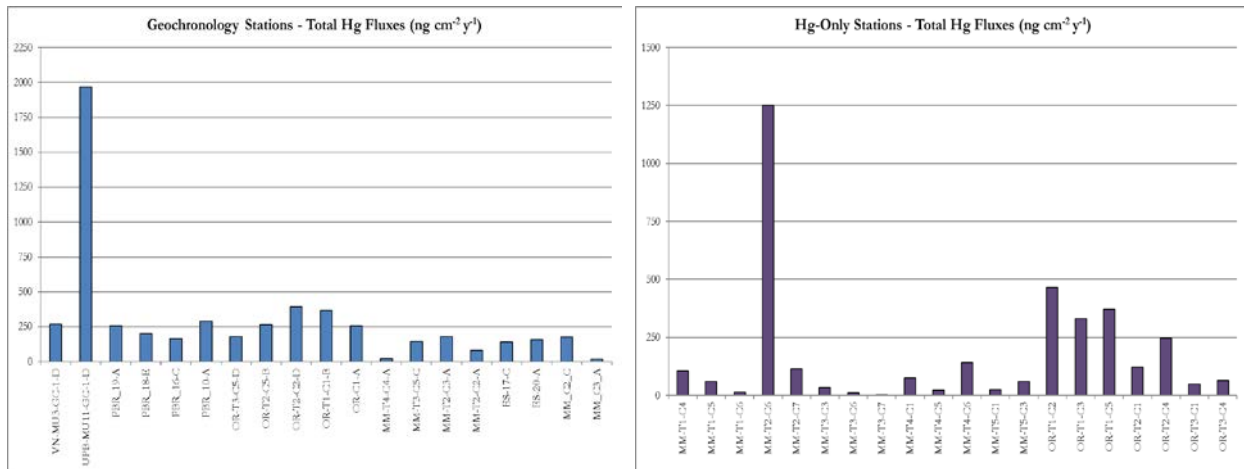


Figure 19: Contemporary fluxes of total Hg to surface sediments at geochronology (left) and Hg only (right) stations.

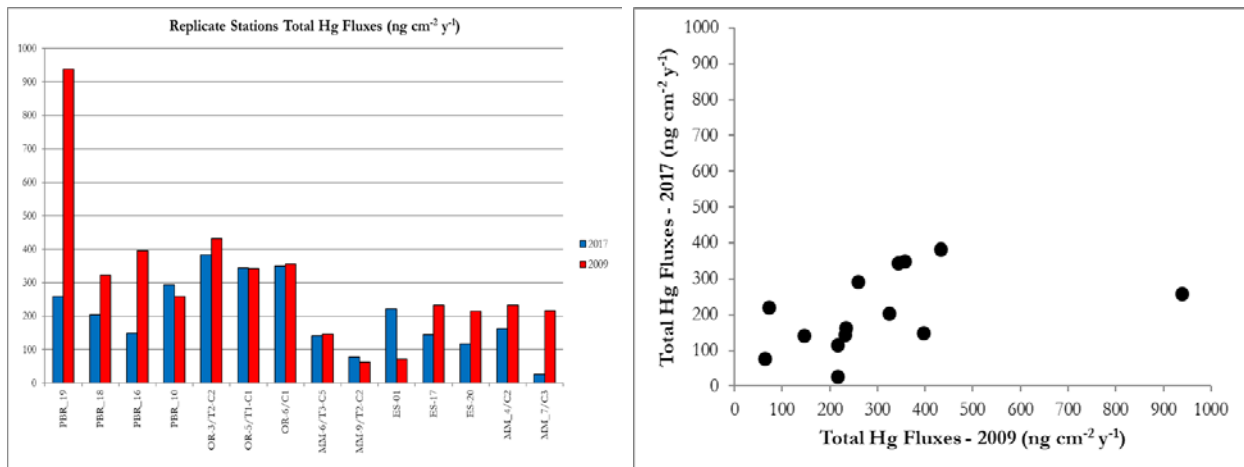


Figure 20: Contemporary fluxes of total Hg to surface sediments at replicate stations (2009, 2017) (left) and comparison (right).

4.4 Objective 4: Apparent Hg Recovery Half Times

The goal here was to calculate apparent total Hg recovery half times for all cores collected in 2017 where possible, and to compare these values with those calculated as part of the 2009 core data set at stations where replicate cores were available. This necessitates that the half times are calculated in exactly the same manner as was done previously by Dr. Peter Santschi for the 2009 core data set (Santschi et al. 2017). For the 2009 core data set, the approach was to use the last 21 years of total Hg profiles in those sediment cores. This was accomplished by using the calculated sediment accumulation rate (cm y^{-1}) based on ^{137}Cs to calculate each core's chronology, which for each core revealed the time of deposition of Hg.

As was the case in the 2009 core data set, the 2017 core data set shows that total Hg in most cores shows a sharp peak over about the lower half of the profile, and a much slower change in total Hg concentrations over the upper profiles. The time period since the primary Hg release was 42

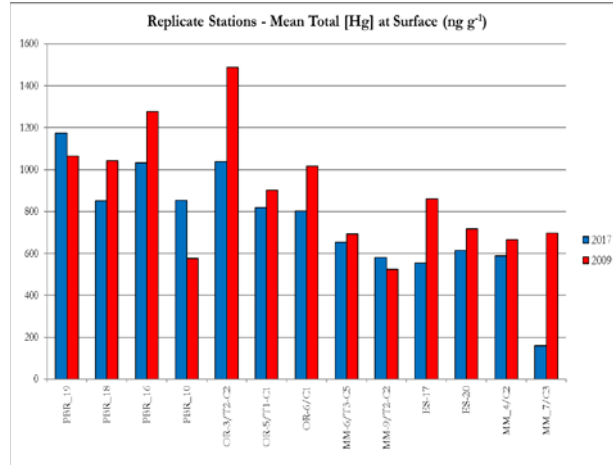


Figure 21: Mean, near surface (0-3 cm) total Hg concentrations at replicate stations (2009, 2017).

years (2009-1967) when considering the 2009 data set, and 50 years when considering the 2017 data set. When modeling the 2009 data set, Dr. Santschi focused on the recent 21 years (1988-2009) of record, which showed relatively slow recovery half times, deduced from relatively modest total Hg concentration changes during that period. For the 2017 data set, the last 21 years (1996-2017) of input history was the focus to determine apparent total Hg recovery half times, so that comparisons between the two data sets would consider equal amounts of time. Apparent recovery half times can be calculated in several ways, including analyses of total Hg peak spreading, a vertical mixed layer approach, or a recovery index ($Hg_{(t)}/Hg_{(max)}$ ratio) approach (Table 3). However, all these approaches suffer from assumptions of steady state, vertical transport only (i.e., no horizontal inputs), and constancy of recovery rates. As was the case with the 2009 data set, for the 2017 data set apparent recovery half times ($t_{1/2} = \ln 2/\alpha$) were calculated from an exponential fit (eq. 6) to total Hg concentration profiles over the past 21 years.

$$Hg_{(t)} = Hg_{(t=21)} * \exp(-\alpha*t) \quad (6)$$

Also consistent with treatment of the 2009 data set, for the 2017 data set apparent recovery half times were also calculated from an exponential fit to the total Hg concentration profiles over the past 21 years, assuming a non-zero asymptotic level ($Hg_{(\infty)}$).

$$Hg_{(t)} = Hg_{(t=21)} * \exp(-\alpha*t) + Hg_{(\infty)} \quad (7)$$

Like with the 2009 data set, for the 2017 data set an asymptotic level ($Hg_{(\infty)}$) of 400 ng g⁻¹ total Hg was utilized (Table 3). Example plots are shown in Figure 22.

Total Hg apparent recovery half times (Fig. 23) and those calculated assuming ($Hg_{(\infty)}$) of 400 ng g⁻¹ total Hg (Fig. 24) for replicate cores in 2009 and 2017 show that natural recovery is slowing in the Penobscot River system. For apparent total Hg recovery half times, nine of 11 stations (82%) compared show increasing values, and for apparent total Hg half times calculated assuming ($Hg_{(\infty)}$) of 400 ng g⁻¹ total Hg, eight of 10 stations (80%) compared show increasing values. Given that there has been no large scale active remediation yet conducted in this system, these results are not surprising. Considerable evidence was provided as part of the PRMS - Phase II study showing that

Table 3: Summary of apparent recovery half times ($T_{1/2} = \ln 2/\alpha$), calculated from exponential fits to total Hg concentration profiles ($Hg(t)$) over the past 21 years ($Hg_{(t=21)}$), as $Hg_{(t)} = Hg_{(t=21)} * \exp(-\alpha*t) + Hg(\infty)$, with $Hg(\infty)$ = asymptotic level of 400 ng g⁻¹ ($T_{1/2}^*$); i = increasing total Hg concentrations to the surface, nc = no change in total Hg concentrations; na = sediment accumulation rate data not available; additional parameters include surface ($Hg_{(0)}$) and maximum total Hg concentrations ($Hg_{(max)}$), apparent sediment accumulation rates calculated from the depth of $Hg_{(max)}$ and ¹³⁷Cs, and total Hg inventories. Where available, replicate stations from 2009 (Santschi et al. 2017) are included immediately following the relevant 2017 stations.

Station	Core type	Year sampled	$T_{1/2}$ (years)	$T_{1/2}^*$ (years)	$Hg_{(0)}$ (ng g ⁻¹)	$Hg_{(max)}$ (ng g ⁻¹)	$Hg_{(0)}/Hg_{(max)}$	$Hg_{(max)}$ Sed. rate (cm y ⁻¹)	Hg Inventory (ng cm ²)	¹³⁷ Cs Sed. rate (cm y ⁻¹)
VN-MU3-GC-1-D	Geochronology	2017	77	770	711	1,510	0.47	0.74	30,174	0.60
VE-MU4-GC-1-E	Geochronology	2017	nc	nc	953	953	1.00	--	2,911	--
UPB-MU11-GC-1-D	Geochronology	2017	50	25	668	3,190	0.21	1.35	--	1.16
UPB-MU11-GC-1-C2	Geochronology	2017	na	na	680	1,950	0.35	1.45	39,666	--
PBR-28-C	Geochronology	2017	na	na	713	891	0.80	--	11,752	--
PBR-26-A	Geochronology	2017	na	na	681	734	0.93	--	6,925	--
PBR-20-E	Geochronology	2017	na	na	1,070	1,290	0.83	--	7,066	--
PBR-19-A	Geochronology	2017	27	19	1,164	2,682	0.43	0.35	25,866	0.51
PBR-19-A	Geochronology	2009	12	8	643	6,440	0.10	1.25	95,720	1.03
PBR-18-E	Geochronology	2017	173	173	854	2,880	0.30	0.70	34,748	0.60
PBR-18-B	Geochronology	2009	23	15	969	2,320	0.42	0.44	24,507	0.40
PBR-16-C	Geochronology	2017	5	4	1,070	100,200	0.01	0.13	128,205	0.19
PBR-16-A	Geochronology	2009	16	na	1,001	73,300	0.01	0.42	150,451	0.72
PBR-10-A	Geochronology	2017	46	21	983	3,270	0.30	0.62	40,078	0.57
PBR-10-A	Geochronology	2009	13	7	507	3,870	0.13	0.83	43,719	0.85
PBR-04-C	Geochronology	2017	nc	nc	2	4	0.50	--	368	--
OR-T3-C5-D	Geochronology	2017	46	21	669	1,450	0.46	0.54	20,304	0.51
OR-T3-C2-C	Geochronology	2017	na	na	1,480	1,900	0.78	--	14,795	--
OR-T2-C5-B	Geochronology	2017	46	23	715	5,260	0.14	0.85	50,161	0.69
OR-T2-C2-D	Geochronology	2017	77	46	924	3,410	0.27	0.78	49,081	0.69
OR-03-A	Geochronology	2009	125	90	1,300	3,080	0.42	0.69	42,534	0.50
OR-T1-C1-B	Geochronology	2017	58	29	951	4,300	0.22	0.95	57,029	0.88
OR-05-C	Geochronology	2009	35	21	754	4,650	0.16	0.74	44,048	0.63
OR-C1-A	Geochronology	2017	nc	nc	863	2,950	0.29	0.78	41,507	0.46

*Surface Hg concentrations < 400 ng g⁻¹.

Table 3: Continued.

Station	Core type	Year sampled	T _{1/2} (years)	T _{1/2} * (years)	Hg ₍₀₎ (ng g ⁻¹)	Hg _(max) (ng g ⁻¹)	Hg _{(0)/} Hg _(max)	Hg _(max) Sed. rate (cm y ⁻¹)	Hg Inventory (ng cm ⁻²)	¹³⁷ Cs Sed. rate (cm y ⁻¹)
OR-06-B	Geochronology	2009	48	30	947	4,510	0.21	0.74	44,713	0.67
MM-T4-C4-A*	Geochronology	2017	19	--	278	2,330	0.12	0.23	5,993	0.23
MM-T4-C3-C	Geochronology	2017	na	na	674	1,750	0.39	--	71,086	--
MM-T4-C2-D*	Geochronology	2017	na	na	317	1,210	0.26	--	38,642	--
MM-T3-C5-C	Geochronology	2017	43	19	602	5,000	0.12	0.42	35,752	0.46
MM-06-A	Geochronology	2009	22	11	678	3,270	0.21	0.50	34,219	0.54
MM-T2-C3-A	Geochronology	2017	17	10	705	5,490	0.13	0.33	28,593	0.34
MM-T2-C2-A	Geochronology	2017	43	17	570	5,490	0.10	0.39	19,735	0.36
MM-09-B	Geochronology	2009	11	11	471	4,420	0.11	0.42	14,850	0.40
ES-01-C3	Geochronology	2017	na	na	707	1,230	0.57	0.27	11,421	--
ES-17-C	Geochronology	2017	39	15	583	1,200	0.49	0.58	17,855	0.57
ES-17-C	Geochronology	2009	123	--	873	2,710	0.32	0.79	27,304	0.16
ES-18-B	Geochronology	2017	i	i	706	706	1.00	--	5,501	--
ES-18-B	Geochronology	2009	i	--	872	1,200	0.73	0.08	11,416	0.27
ES-20-A	Geochronology	2017	173	63	586	1,620	0.36	0.23	15,764	0.38
ES-20-C	Geochronology	2009	100	48	725	2,060	0.35	0.46	22,902	0.34
FF-MU7-GC-1-B*	Geochronology	2017	i	i	349	349	1.00	--	2,575	--
MM-C2-C	Geochronology	2017	24	11	584	4,310	0.14	0.54	54,965	0.60
MM-04-C	Geochronology	2009	23	20	646	5,140	0.13	0.55	62,996	0.63
MM-C3-A	Geochronology	2017	231	87	665	5,570	0.12	0.33	39,105	0.31
MM-07-A	Geochronology	2009	15	12	626	6,310	0.10	0.69	53,799	0.76
MM-T2-C1-B*	Geochronology	2017	na	na	173	1,050	0.16	--	1,533	--
MM-C1	Hg only	2017	i	i	804	982	0.82	--	33,166	--
MM-T1-C1	Hg only	2017	na	na	608	936	0.65	--	11,661	--
MM-T1-C2	Hg only	2017	na	na	779	1,040	0.75	--	34,857	--
MM-T1-C3	Hg only	2017	i	i	565	565	1.00	--	4,080	--
MM-T1-C4	Hg only	2017	nc	nc	882	1,930	0.46	0.23	16,264	--
MM-T1-C5	Hg only	2017	20	6	494	4,430	0.11	0.39	20,571	--
MM-T1-C6*	Hg only	2017	i	i	136	464	0.29	0.11	2,558	--

*Surface Hg concentrations < 400 ng g⁻¹.

Table 3: Continued.

Station	Core type	Year sampled	T _{1/2} (years)	T _{1/2} * (years)	Hg ₍₀₎ (ng g ⁻¹)	Hg _(max) (ng g ⁻¹)	Hg _{(0)/} Hg _(max)	Hg _(max) Sed. rate (cm y ⁻¹)	Hg Inventory (ng cm ⁻²)	¹³⁷ Cs Sed. rate (cm y ⁻¹)
MM-T2-C4*	Hg only	2017	i	i	116	116	1.00	--	1,110	--
MM-T2-C5	Hg only	2017	i	i	544	544	1.00	--	6,076	--
MM-T2-C6	Hg only	2017	i	i	960	3,280	0.29	1.35	54,318	--
MM-T2-C7*	Hg only	2017	6	na	33	3,280	0.01	1.35	--	--
MM-T3-C1*	Hg only	2017	i	i	363	363	1.00	--	1,111	--
MM-T3-C2	Hg only	2017	na	na	604	720	0.84	--	6,288	--
MM-T3-C3*	Hg only	2017	173	na	225	615	0.37	0.27	6,412	--
MM-T3-C4	Hg only	2017	na	na	729	1,080	0.68	--	24,897	--
MM-T3-C6*	Hg only	2017	na	na	232	915	0.25	0.19	2,428	--
MM-T3-C7*	Hg only	2017	na	na	184	529	0.35	0.11	1,428	--
MM-T4-C1	Hg only	2017	58	17	482	2,620	0.18	0.33	11,296	--
MM-T4-C5*	Hg only	2017	na	na	282	2,050	0.14	0.21	5,148	--
MM-T4-C6	Hg only	2017	46	25	690	2,960	0.23	0.39	32,057	--
MM-T4-C7	Hg only	2017	i	i	681	844	0.81	--	6,275	--
MM-T5-C1	Hg only	2017	347	26	502	1,610	0.31	0.21	5,010	--
MM-T5-C2*	Hg only	2017	i	i	293	293	1.00	--	1,724	--
MM-T5-C3	Hg only	2017	39	17	669	3,770	0.18	0.35	13,547	--
OR-T1-C2	Hg only	2017	58	29	637	3,530	0.18	0.85	63,071	--
OR-T1-C3	Hg only	2017	43	23	647	3,510	0.18	0.85	57,076	--
OR-T1-C4*	Hg only	2017	i	i	86	86	1.00	--	1,438	--
OR-T1-C5	Hg only	2017	116	58	638	2,250	0.28	0.85	52,349	--
OR-T2-C1	Hg only	2017	139	69	721	2,310	0.31	0.29	17,734	--
OR-T2-C3	Hg only	2017	i	i	1,820	1,820	1.00	--	5,898	--
OR-T2-C4	Hg only	2017	24	14	771	3,680	0.21	0.58	46,241	--
OR-T3-C1	Hg only	2017	116	43	621	1,220	0.51	0.15	15,582	--
OR-T3-C3	Hg only	2017	na	na	1,110	2,330	0.48	--	55,909	--
OR-T3-C4	Hg only	2017	i	i	740	937	0.79	0.15	8,972	--

*Surface Hg concentrations < 400 ng g⁻¹.

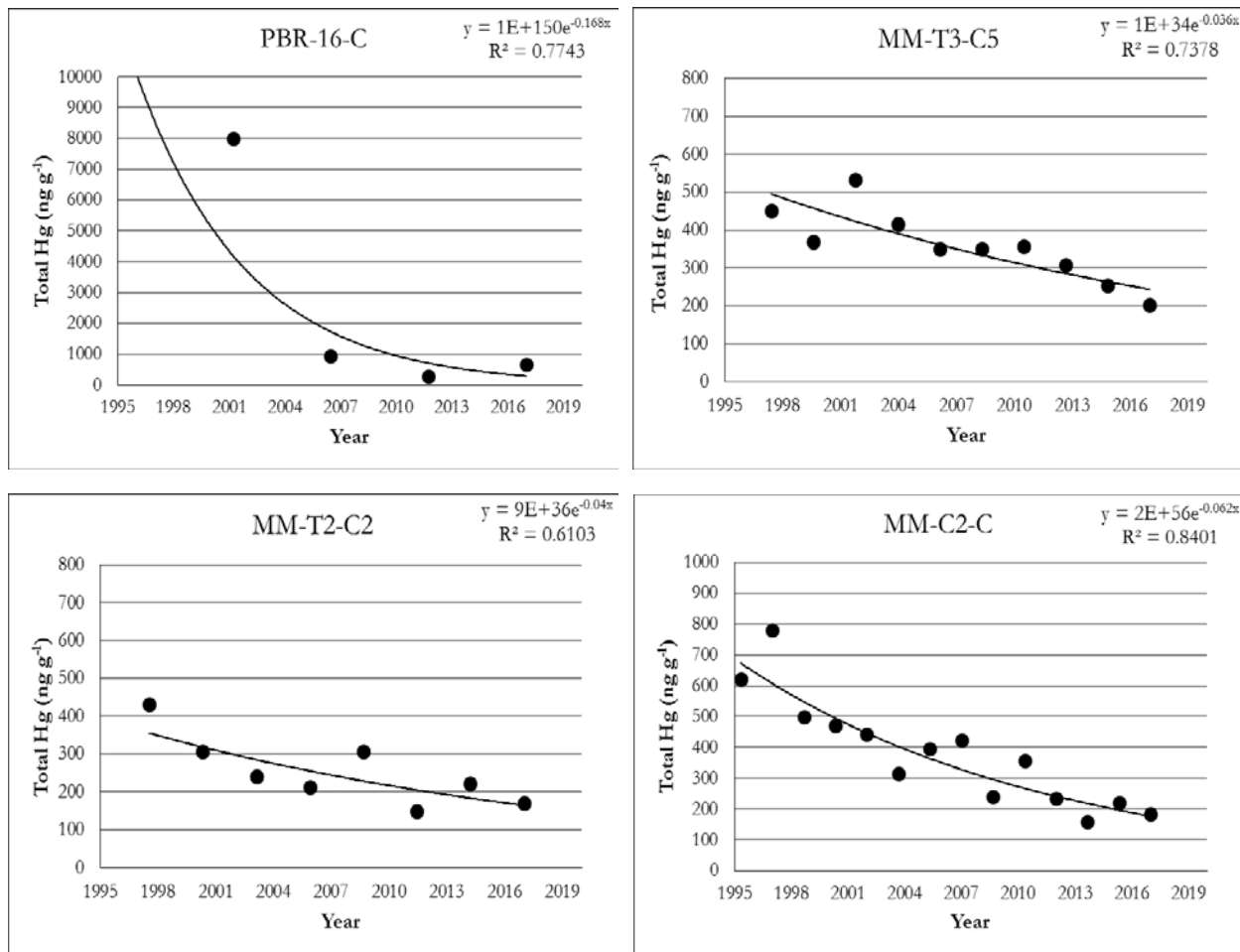


Figure 22: Example model plots from 2017 core stations for apparent total Hg recovery half times ($t_{1/2}$) assuming $Hg_{(\infty)} = 400 \text{ ng g}^{-1}$.

sediment with elevated (i.e., above 400 ng g^{-1}) concentrations of total Hg were continuing to be mobilized and transported throughout the study system, either as part of the mobile pool (Geyer and Ralston 2017), or as a function of sediment erosion, resuspension, and transport. The slowing of apparent recovery can also be seen in plots of total Hg concentrations with depth in sediment cores collected in 2017 from throughout the system (Fig. 25). The continued inputs of above background concentrations of total Hg produce shallow slopes of total Hg concentrations with depth (or time) as one approaches the sediment surface (or time 0), resulting in increasing apparent total Hg recovery half times. This scenario will not change except by either the reduction in average total Hg concentrations on sediments being deposited throughout the system, or by the passage of large amounts of time (10's to 100's of years).

4.5 Objective 5: Sediment Core Transects

A series of eight sediment core transects were established in 2017, comprised mostly of Hg only cores. All of these transects included at least one geochronology station, with the exception of transects one and five in Mendall Marsh. Three of these transects were established in the Orland

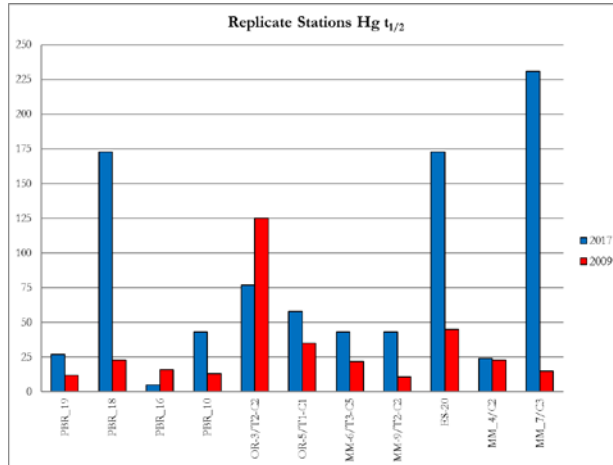


Figure 23: Total Hg apparent recovery half times ($t_{1/2}$) compared at replicate stations sampled in 2009 and 2017.

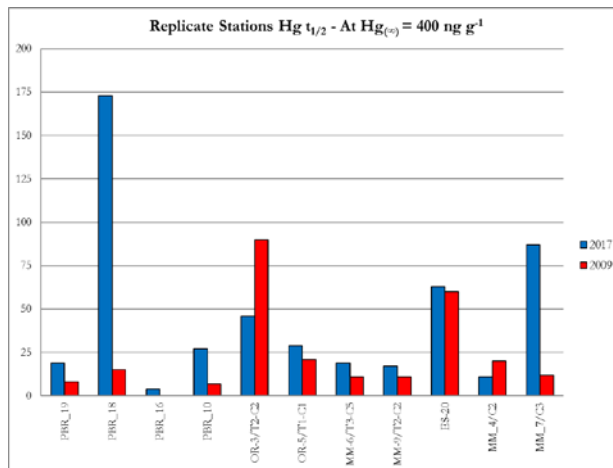


Figure 24: Total Hg apparent recovery half times ($t_{1/2}$) assuming $Hg_{(\infty)} = 400 \text{ ng g}^{-1}$ compared at replicate stations sampled in 2009 and 2017.

River (Figs. 8-9), and five in Mendall Marsh (Figs. 5-7). In every case, the transects were sampled along lines normal to the Orland River, the marsh river, and in the case of Mendall Marsh transect number five, normal to a major marsh distributary. Given the relatively small number of cores comprising each transect, and the limited amount of data available for each (primarily Hg only data), an examination of each individual transect is not useful. Instead, each group of transects were considered as a collective (i.e., all transect data for the Orland River and Mendall Marsh). The primary goal of these transects were to determine the presence of spatial relationships between core locations and the primary water and sediment (and Hg) sources. Sediment cores along transects that were located either in open water, or $< 10 \text{ m}$ from the closest channel, were not considered, since these locations would be expected to be regularly mixed by hydrologic processes. Lateral distance (m) to the closest primary channel for the remaining cores was compared to other variables,

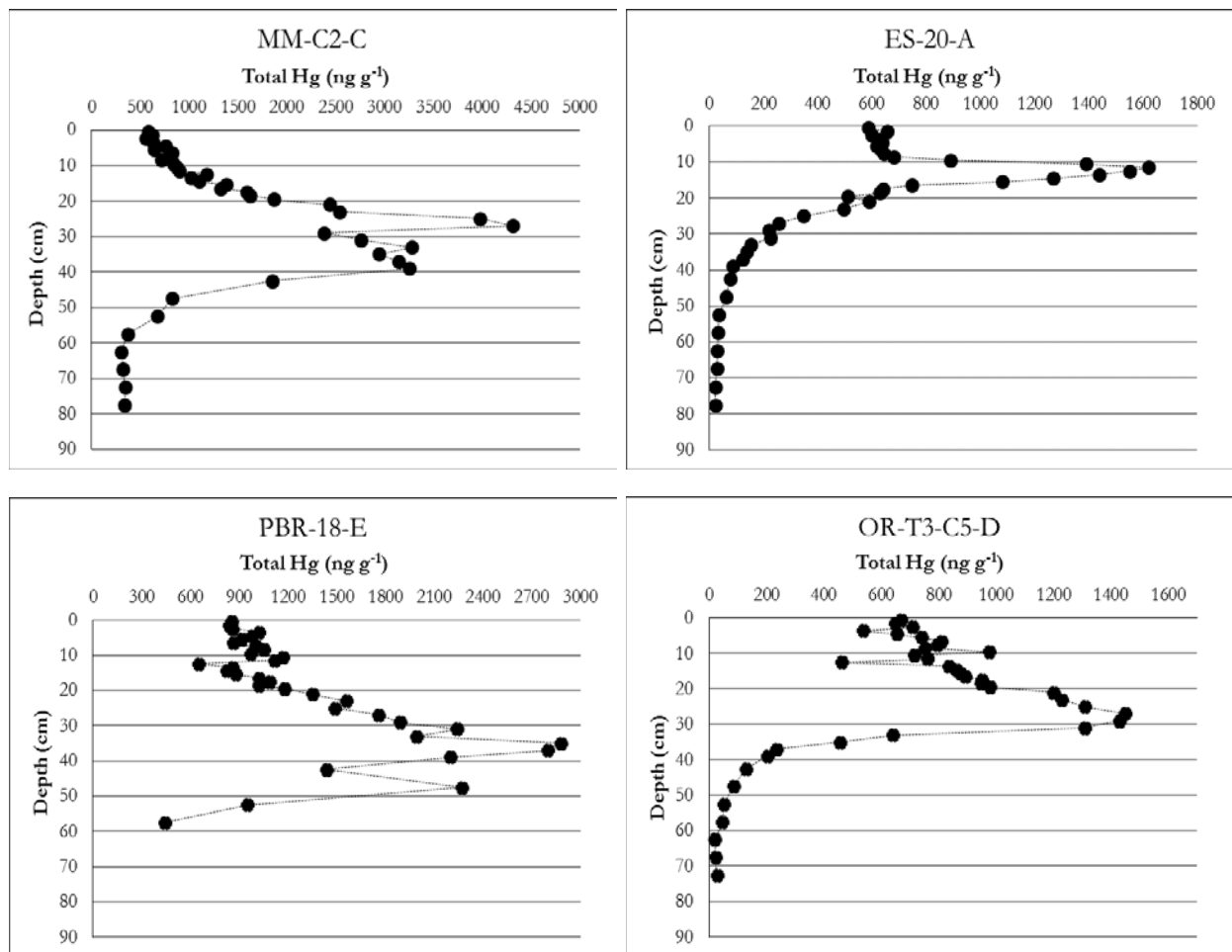


Figure 25: Example plots of total Hg concentrations with depth from throughout the study system.

including total Hg inventories, mean near surface (0-3 cm) total Hg concentrations, contemporary total Hg fluxes, and apparent total Hg recovery half times assuming $Hg_{(\infty)} = 400 \text{ ng g}^{-1}$.

Given that all cores collected along transects located in the Orland River were located either in open water (within the river channel itself), or on intertidal mudflats immediately adjacent to the river channel, it was not surprising to find no significant spatial relationships between core distance (lateral) from the Orland River channel and any of the variables considered (Figs. 26-27). In this environment, there are no topographic (i.e., elevation), or other physical barriers between these intertidal mudflats and the river proper. Cores along these transects are either permanently inundated (those located in the river channel), or regularly inundated by daily tidal fluctuations. This absence of lateral differentiation does allow for the direct comparison of longitudinal effects, in this case as a function of transect distance from the mouth of the Orland River, where it has confluence with the Penobscot River. Figure 28 shows mean values, for each of the three Orland River transects, of total Hg-based sediment accumulation rates, total Hg inventories, mean total Hg near surface (0-3 cm) concentrations, and total Hg fluxes, as a function of distance from the Orland River mouth. It is clear, and unsurprising, that the primary source of sediment (and Hg) to the lower

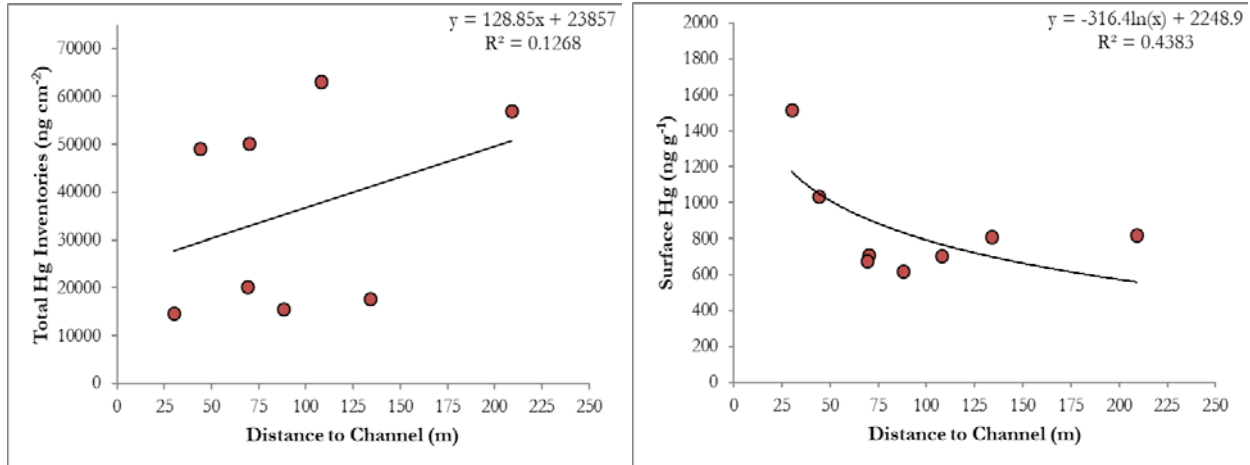


Figure 26: All Orland River transects compiled data, comparing total Hg inventories (left) and mean near surface total Hg concentrations (right) to lateral distance from Orland River channel margins.

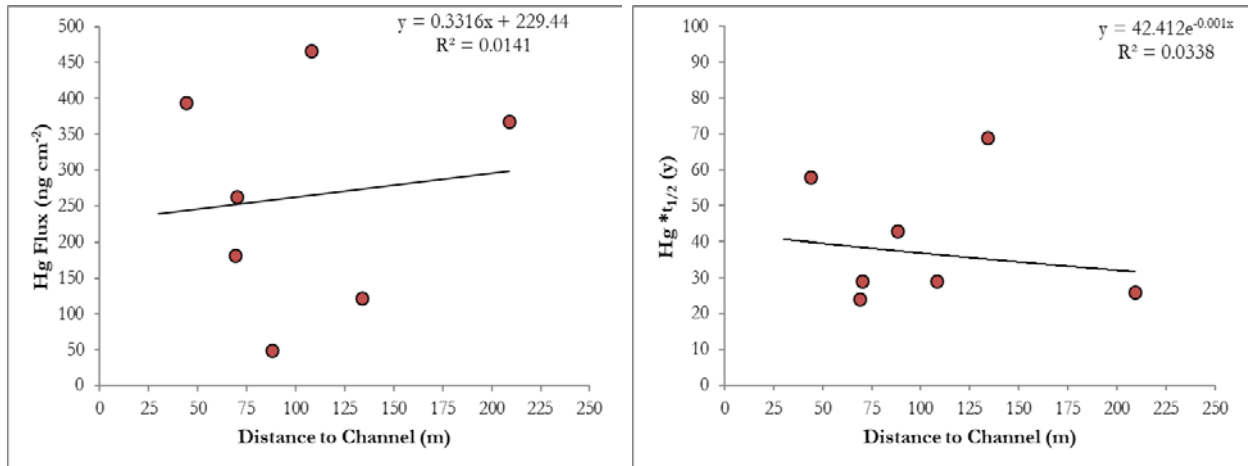


Figure 27: All Orland River transects compiled data, comparing total Hg fluxes (left) and apparent total Hg recovery half times ($t_{1/2}$) assuming $Hg_{(\infty)} = 400 \text{ ng g}^{-1}$ (right) to lateral distance from Orland River channel margins.

Orland River is not the Orland River watershed, but the Penobscot River. This is reflected by the clear increases in mean sediment accumulation rates, total Hg inventories, and total Hg fluxes with proximity to the mouth of the Orland River. It is interesting to note that mean near surface (0-3 cm) total Hg concentrations show the opposite relationship, with the total mean Hg near surface concentrations progressively increasing with distance away from the Orland River mouth. This is likely a function of sediment transport dynamics here, where finer grained sediments (and therefore relatively enriched in Hg; e.g., Barghigiani et al. 1996; Boszke et al. 2004; Liu et al. 2017) are transported a greater distance up the lower Orland River before being deposited.

The setting in Mendall Marsh differs considerably. Here, transect cores located beyond the marsh river or distributary channels are partially buffered from these water bodies by the margins of

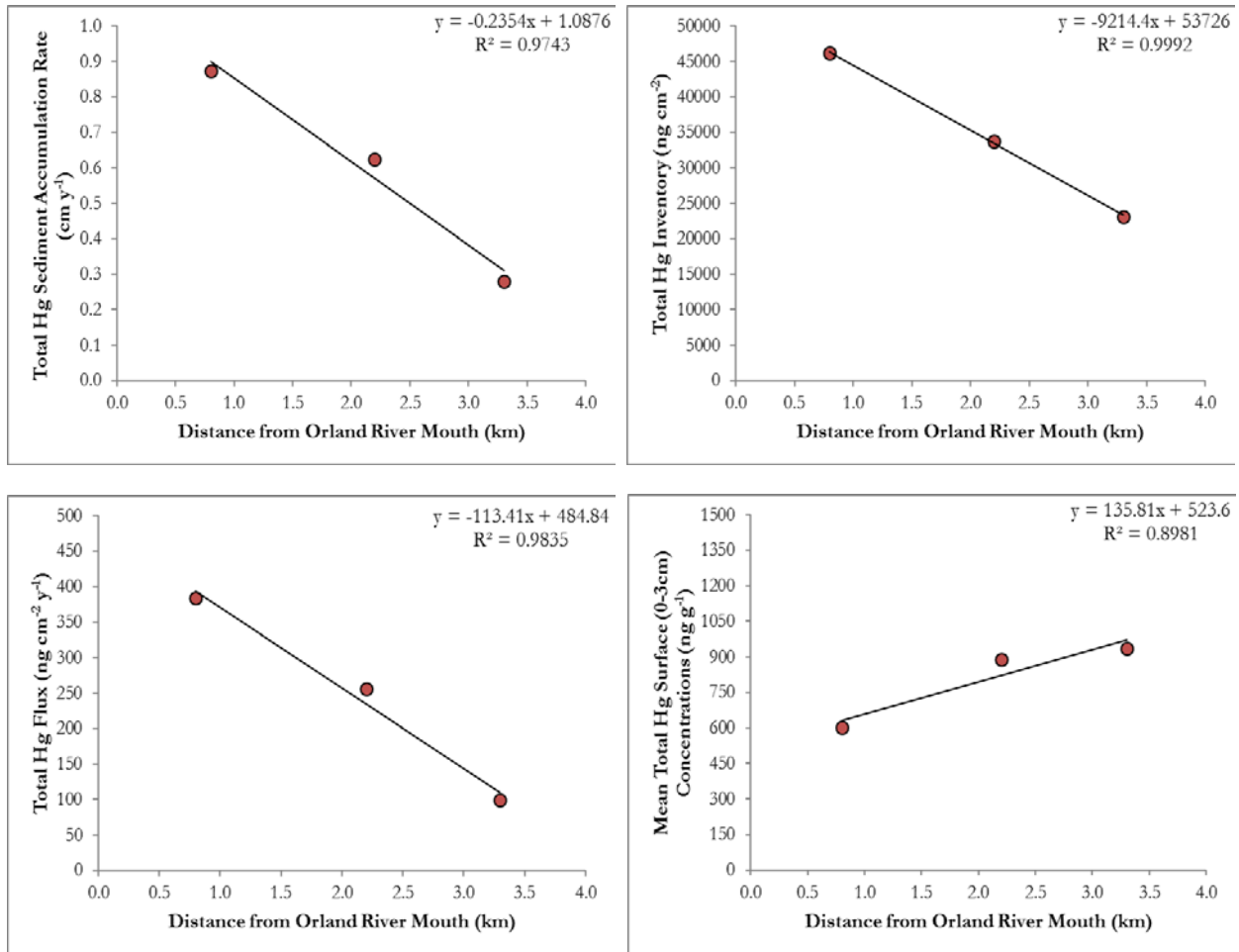


Figure 28: All Orland River transects compiled data, comparing total Hg inventories (left) and mean surface Hg concentrations (right) to distance from major river or distributary channel margins.

the marsh platform, which is typically elevated well above base flow elevations, and characterized by natural levees constructed over time by periodic inundation of the marsh during large magnitude hydrologic events (floods, spring tides, etc.) (e.g., Temmerman et al. 2004; Filgueira-Rivera et al. 2007). As such, marsh platforms tend to be relatively stable depocenters, where the distance on the marsh platform from major rivers and distributaries is an important control on sediment, nutrient and contaminant supplies (e.g., Villar et al. 1996; Callaway et al. 1998; Palinkas and Engelhardt 2016). As can be seen in Figures 29 and 30, clear relationships along Mendall Marsh core transects are evident between distance from a primary channel and all of the variable considered. All data relationships are best described by natural log functions, and all show that as the distance between the marsh locations and the closest, primary river or distributary channels decreases, total Hg inventories, near surface concentrations, and fluxes increase, as do the apparent recovery half times of Hg in these sediments. These results are not surprising, and suggest that remedial strategies under consideration for Mendall Marsh can utilize these proximity to source (waterways) data relationships to identify areas of the marsh that do and do not require active remedial approaches, based on identified thresholds.

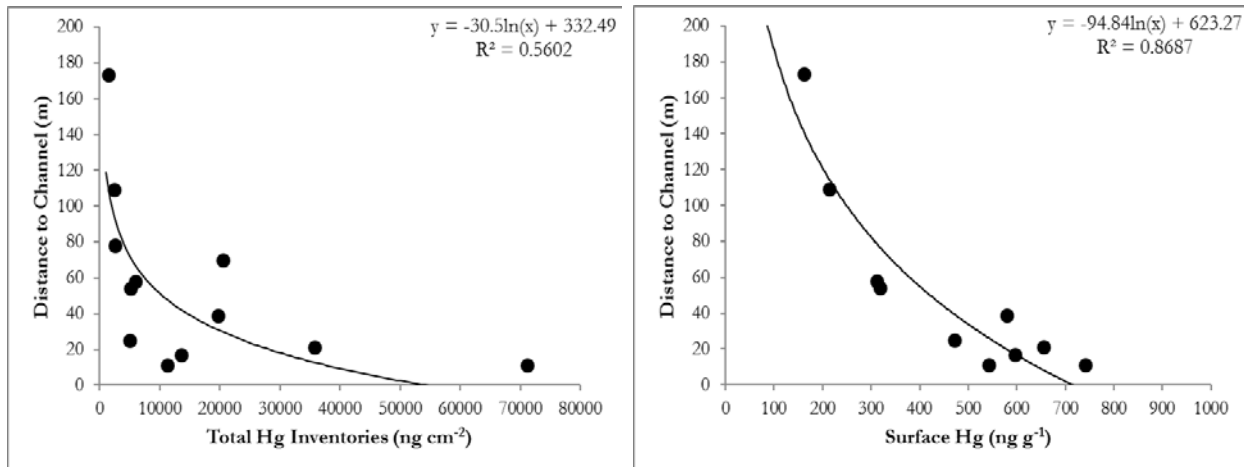


Figure 29: All Mendall Marsh transects compiled data, comparing total Hg inventories (left) and mean near surface total Hg concentrations (right) to lateral distance from major river or distributary channel margins.

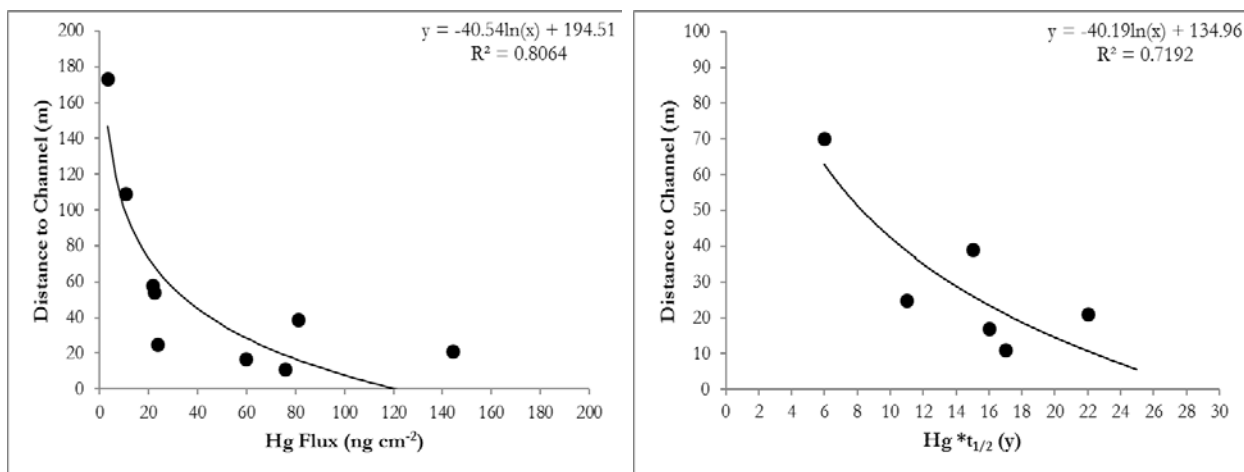


Figure 30: All Mendall Marsh transects compiled data, comparing total Hg fluxes (left) and apparent total Hg recovery half times ($t_{1/2}$) assuming $Hg_{(\infty)} = 400 \text{ ng g}^{-1}$ (right) to lateral distance from major river or distributary channel margins.

5. CONCLUSIONS

1. Sedimentary inventories of total Hg in cores collected in 2017 ranged from 4 to 1,282 mg m^{-2} . Differences throughout the system in terms of mean Hg inventories were apparent, and included in order of magnitudes, the Orland River ($n = 16, 348 \pm 210 \text{ mg m}^{-2}$), the Penobscot River ($n = 12, 346 \pm 382 \text{ mg m}^{-2}$), Mendall Marsh ($n = 32, 187 \pm 183 \text{ mg m}^{-2}$), and the Penobscot estuary ($n = 4, 126 \pm 47 \text{ mg m}^{-2}$) (uncertainties reported at 1σ). The large uncertainties associated with these values are not surprising, and are likely a function of both natural variability in these environments, and the specific rationale used to identify core sample locations. Comparing replicate core (2009 vs. 2017) locations only shows that re-sampled environments have not changed appreciably in terms of total

Hg sedimentary inventories during this eight year interval. Most of the variability in evidence between sample periods are found in cores from the Penobscot River. It is most likely that these differences in total Hg inventories in Penobscot River cores from 2009 and 2017 do not reflect net reductions in the amounts of total Hg held in these sediments over this period, but instead reflect variability in sedimentary records over small spatial scales in this dynamic river setting.

2. Unsurprisingly, given the range of physical and hydrological settings represented by these stations, a wide range in sediment accumulation rates was observed (0.11 to 1.35 cm y⁻¹) (based on ¹³⁷Cs for geochronology cores, and total Hg for Hg only cores). When comparing ¹³⁷Cs-based sediment accumulation rates available for the 13 stations sampled in both 2009 and 2017, it is clear that sediment accumulation rates decreased at 10 of these stations (77%), and increased at three of them (23%). Given the data available, it is not possible to determine whether these differences represent actual changes in the rates of sediment delivery to these locations over this eight year period, or simply reflect natural heterogeneities over small spatial scales.

3. It was possible to compare contemporary total Hg fluxes at a total of 14 stations, sampled in both 2009 and 2017. These data show that at eight stations (57%) fluxes decreased, at two stations (14%) fluxes increased, and at four stations (29%) fluxes remained unchanged. There is no evident relationship between these two total Hg flux data sets, which is likely a function of two factors, (1) natural heterogeneity between sample sites selected to repeat previous sampling, and (2) actual changes from 2009 to 2017 in sediment accumulation rates, and/or changes in total Hg concentrations on sediments deposited at these sites since 2009. As mentioned above, ¹³⁷Cs-based sediment accumulation rates decreased at 10 of 13 stations compared (77%), and increased at three of them (23%). Similarly, mean, near surface total Hg concentrations decreased at 10 of these same stations (77%), and increased at three of them (23%). It is clear from these data that reductions observed in contemporary total Hg fluxes to sediments at replicate stations is being driven, in part, by both reductions in sediment accumulation rates, and reductions in the concentrations of total Hg on sediments delivered to these environments over the last eight years.

4. Total Hg apparent recovery half times and those calculated assuming ($Hg_{(\infty)}$) of 400 ng g⁻¹ for replicate cores in 2009 and 2017 clearly show that natural recovery is slowing in the Penobscot River system. For apparent total Hg recovery half times, nine of 11 stations (82%) compared show increasing values, and for apparent total Hg half times calculated assuming ($Hg_{(\infty)}$) of 400 ng g⁻¹, eight of 10 stations (80%) compared show increasing values. Given that there has been no large scale active remediation yet conducted in this system, these results are not surprising. Considerable evidence was provided as part of the PRMS - Phase II study showing that sediment with elevated (i.e., above 400 ng g⁻¹) concentrations of total Hg were continuing to be mobilized and transported throughout the study system, either as part of a mobile pool, or as a function of sediment erosion, resuspension, and transport. The slowing of apparent recovery can also be seen in plots of total Hg concentrations with depth in sediment cores collected in 2017 from throughout the system. Continued inputs of above background concentrations of total Hg produce shallowing slopes of total Hg concentration with depth (or time) as one approaches the sediment surface (or time 0), resulting in increasing apparent total Hg recovery half times. This scenario will not change except by either the reduction in average total Hg concentrations on sediments being deposited throughout system, or by the passage of large amounts of time (10's to 100's of years).

5. Eight core transects were established in 2017 (three in the Orland River, and five in Mendall Marsh), comprised mostly of Hg only cores (although all transects except for numbers one and five in Mendall Marsh included at least one geochronology station). All transects were oriented and sampled along lines normal to the Orland River, and marsh river (or major marsh distributary). Each group of transects were considered as a collective (i.e., all transect data for the Orland River and Mendall Marsh). These transects were sampled to determine the presence of spatial relationships between core locations and the primary local water, sediment and total Hg sources. Lateral distance to the closest primary channel was compared to other variables, including total Hg inventories, mean near surface (0-3 cm) total Hg concentrations, contemporary total Hg fluxes, and apparent total Hg recovery half times assuming $Hg_{(\infty)} = 400 \text{ ng g}^{-1}$. Given that all cores collected along transects in the Orland River were located either in open water, or on intertidal mudflats adjacent to the channel, it was not surprising to find no significant spatial relationships between lateral distances from the river channel and any of the variables considered. In this environment, there are no topographic, or other physical barriers between these intertidal mudflats and the river proper. Core locations along these transects are either permanently inundated, or regularly inundated by daily tidal fluctuations. This absence of lateral differentiation did allow for the direct comparison of longitudinal effects, in this case as a function of transect distance from the mouth of the Orland River, where it has confluence with the Penobscot River. It was clear, and unsurprising, that the primary source of sediment (and total Hg) to the lower Orland River is not the Orland River watershed, but the Penobscot River. This was reflected by the clear increases in mean sediment accumulation rates, total Hg inventories, and total Hg fluxes with proximity to the mouth of the Orland River. Mean near surface (0-3 cm) total Hg concentrations showed the opposite relationship, with mean total Hg near surface concentrations progressively increasing with distance away from the Orland River mouth. This is likely a function of sediment transport dynamics here, where finer grained (and relatively enriched in Hg) sediments are transported a greater distance up the lower Orland River before being deposited. In Mendall Marsh, transect core locations beyond the marsh river or distributary channels are partially buffered from these water bodies by the marsh platform margins, which are typically elevated well above base flow and characterized by natural levees constructed over time by periodic inundation of the marsh. Clear relationships along Mendall Marsh core transects were evident between lateral distance from a primary channel and all of the variable considered. These data show that as lateral distance between the marsh core locations and the closest river or distributary channels decreases, total Hg inventories, mean near surface concentrations, and contemporary fluxes all increase, as do the apparent total Hg recovery half times. These results are not surprising, and suggest that any remedial strategies under consideration for Mendall Marsh can utilize these proximity to source (waterways) data relationships to identify areas of the marsh that do and do not require active remedial approaches, based on identified thresholds.

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APPENDIX 1

Physical Variables Reported (in report, appendices or supporting spreadsheets):

- (1) Sediment dry bulk density (B_d) – g cm^{-3} : Determined using a slight modification of the core method (Dane et al., 2002), by $B_d = \text{mass of dry solids (g)}/\text{total volume (cm}^3)$
- (2) Sediment fraction of water (f_w): Determined by $f_w = [(\text{sediment wet mass (g)} - \text{sediment dry mass (g)})/\text{sediment wet mass (g)}]$
- (3) Sediment fraction of organic matter (f_{om}) - %: Determined by $f_{om} = [2 \times \% \text{ POC}]$
- (4) Sediment grain density (ρ_s) – g cm^{-3} : An initial value of 2.50 g cm^{-3} is assumed, reflecting a mix of dominantly silicate minerals, and is modified where possible by considering the fraction of sedimentary organic matter (when available) by: $\rho_s = [((1.70 \text{ g cm}^{-3} \times f_{om}) + (2.50 \times (100 - f_{om}))/100]$
- (5) Sediment porosity (φ) - %: Determined by also considering the fraction of sedimentary organic matter (when available) by: $\varphi = [(f_w/(f_w + (1 - f_w)/\rho_s)]$
- (6) Sediment mass depth – g cm^{-2} : Determined by $[(1 - \varphi) \times \rho_s \times \text{interval thickness (cm)}]$
- (7) Sediment cumulative mass depth – g cm^{-2} : Determined as the sum of mass depths over depth
- (8) Fractions of sand, silt and clay – %: Size classes of mineral sediment corresponding to the Wentworth scale, sand ($2 \text{ mm} - 62.5 \mu\text{m}$), silt ($62.5 \mu\text{m} - 4 \mu\text{m}$) and clay ($< 4 \mu\text{m}$) (Wentworth, 1922)
- (9) Sedimentary inventories of total Hg (ng cm^{-2}) were calculated to 90 cm, or the end of each core (EOC) using: $I_{\text{Hg}} = \Sigma[\text{sediment interval (cm)} \times (1 - \varphi \times \rho_s) \times [\text{Hg}] (\text{ng g}^{-1})]$

9/11/18

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Re: Responses to project report by Dr. Peter H. Santschi

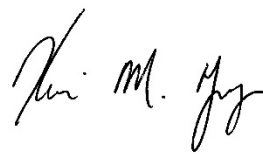
Dear Nelson,

I have completed a careful review of all of the questions and points of constructive criticism raised by Dr. Peter Santschi in his review of my report, and provide here a response to each in turn. To respond adequately to many of the points raised, it was necessary to revise my original report, a copy of the revised report is also provided.

Generally, I found the points of constructive criticism provided to be very helpful and in addressing them believe that the report has been improved.

Please contact me if you require any additional information. Thank you for your time and consideration.

Sincerely,

A handwritten signature in black ink that reads "Kevin M. Yeager". The signature is written in a cursive style with a large initial 'K' and 'Y'.

Dr. Kevin M. Yeager

General Remarks:

1. Physical mixing of near-surface sediments was deemed a topic of investigation in the summary report, but not much is said about it. How was near surface physical mixing evaluated?

Response: Near surface sediment mixing was estimated by examining a combination of data, including POC concentration profiles, total Hg concentration profiles, grain size profiles, and radionuclide activity concentration profiles (fallout isotopes – only available in some cores). This is described throughout the Yeager report, and is in direct response to Wood Group work order objective B.

Table 1. ‘Mixed depths’. It is not clear what is meant by that. It is very improbable that sediments can be vertically mixed down to 50 cm or so, as there is not enough physical mixing energy available in the environment, and bioturbation is restricted to very shallow depths, as detailed for the 2009 papers by Santschi et al. (2017) and Yeager et al. (2018a,b). The conclusions from the 2009 sampling expedition were that vertical mixing was restricted to the upper 1-3 cm. Thus, it might be better to label this as “homogeneous deposition” in the ‘Alternatives Evaluation Report’.

Response: Not revised. The conclusions of the 2009 expedition, resulting reports and publications are not in conflict with the results presented here. In 2017 (just as in 2009) there were some core locations that exhibited extensively mixed core sections, reflecting long-term mixing events at those locations. Having core sections where mixing extends over tens of centimeters below the surface are unlikely to be produced by bioturbation over short time scales, as Dr. Santschi points out. However, pervasive physical and biological sediment mixing over extended periods of time (decades or longer) at a given location can produce core sections that exhibit deep sediment mixing, such as the case for some cores examined in both 2017, and 2009.

Lateral transport by deposition/erosion/re-deposition needs to be better emphasized in this and the ‘Alternatives Evaluation Report’. This is a more accepted and convincing explanation for apparent physical mixing of surface sediments; mixing extent with depth was deemed to be shallow by the previous and the present studies. It is nearly impossible to vertically mix consolidated sediments to depths deeper than about 5-10 cm by purely physical mixing, e.g., by currents. In addition, the existence of a fluid mud layer, or “mobile pool of contaminated sediment” has been emphasized by a number of investigators (e.g., Geyer and Ralston, 2018).

Response: Not revised. Given the data constraining the Yeager report, it is impossible to differentiate between sediment that has been transported laterally and deposited (or eroded and re-deposited) from sediment that has been physically or biologically mixed vertically. So, “mixing” in the context of the Yeager report refers to all of these possibilities.

Figures 13 and 14 that have ‘sediment mixing’ effects as explanations of vertical profiles of grain size and porosity are completely backwards, if ‘mixing’ implies vertical mixing. For example, take “Figure 14: Comparison of sediment grain size distributions (sand : silt : clay) with depth for a core characterized as extensively mixed (left) vs. a core characterized as not extensively mixed (right). “Vertical mixing would tend to homogenize porosity and grain size distribution, while lateral transport of sediment from different locations would produce a more raggedy and layered profile of these tracers.

Response: Revised in part. As pointed about in the previous response, “mixing” in the Yeager report includes both vertical mixing, and “mixing” that is produced along with lateral transport and deposition/erosion/re-deposition. Dr. Santschi and I simply disagree on our interpretations of these data. In the simplest terms, sediment which has either been extensively mixed or not extensively mixed, do not exhibit only a single set of characteristics in terms of grain size distributions or porosity (or other physical variables – bulk

density, POC concentrations, etc.) to reflect that state. Other considerations, including the environment of deposition, the primary source(s) of sediment, seasonality, and any changes in these things (among other variables) can all influence the characteristics exhibited by the variables depicted in Figures 13 and 14. The interpretation given in the Yeager report is reasonable, and the report has been revised to include several additional references to the peer reviewed literature to substantiate that interpretation.

2. Assumptions for calculations of sedimentation rates. The main assumptions include 1) vertical mixing of sediments is negligible; 2) sedimentation rates are constant over the interval from surface to peak depth of pulse tracers ^{137}Cs or Hg, or steady-state tracer $^{210}\text{Pb}_{\text{xs}}$. These assumptions need to be stressed, and the extended mixed depths in the report are confusing the issue, as was said before, vertical mixing, even though not quantified in this report, must be very limited, and any homogenous sediment deposition could be also produced from lateral transport. The assumption of constancy of sedimentation could be viewed as obvious, as this is all that could be done with the data. However, when taken together, it cannot be stressed enough that sedimentation rates of $0.1\text{-}0.2\text{ cm y}^{-1}$ are likely upper limits, since in those cases the peak depths of ^{137}Cs and/or Hg would be around 5 to 10 cm. Given that vertical mixing of sediments extends over 1-3 (sometimes 5) cm, peaks would be smoothed out and displaced vertically and possibly, further distorted. Similarly, $^{210}\text{Pb}_{\text{xs}}$ profiles extending over the same depth intervals would be seriously affected by vertical mixing if those depth intervals would have been used to calculate sedimentation rates. This could also affect the calculation of contemporary Hg fluxes, as they would become upper limits as well, but not Hg inventories.

Response: Revised in part as suggested. Explicit statements of assumptions associated with models employed for each of the tracers utilized in the Yeager report have been added, as suggested. Additional revisions to stress the “upper limits” of sediment accumulation rates as “ $0.1\text{-}0.2\text{ cm y}^{-1}$ ” have not been added. Upon examination, there are several 2009 and 2017 core sections where evidence of mixing was limited, and yet peak activity concentrations of ^{137}Cs and concentrations of total Hg were found well below 10 cm depth, indicating clearly that sediment accumulation rates $> 0.2\text{ cm y}^{-1}$ are found here.

3. Non-zero intercepts in many correlations shown in figures need to be physically or sedimentologically meaningful. However, often correlations shown as least squares fits to a straight line with a non-zero intercept that do not make sense. In many cases, it would be more logical to force the correlation to go through the origin (without intercept). Examples are Figures 15, 16, 20, 22, 27, where one cannot imply that one of the geochronological parameters would have a non-zero sedimentation rate when the other parameter is zero. Or take Figure 20, where a non-zero Hg flux in 2017 at zero Hg flux in 2009 would be implied.

Response: Revised in part as suggested. Figure 15 is a bar chart with no correlations and remains unchanged. Figure 16 has been revised as suggested. In Figure 20, forcing the linear regression fit through zero results in an $R^2 < 0$, which simply indicates that a horizontal line through the data explains the data better than a linear regression model. As such, Figure 20 has been revised to remove the linear regression fit entirely. The four data panels in Figure 22 depict example total Hg concentrations over time at four stations, it makes no sense to force these regression fits through zero. The two data panels in Figure 27 depict total Hg fluxes and Hg recovery half times with distance to the main channel of the Orland River, it makes no sense to force these regression fits through zero.

4. A number of results should not only be displayed via figures, but also tabulated somewhere in the report. So, for example, for each core location, sedimentation rates (cm y^{-1}) and sediment accumulation

rates ($\text{g cm}^{-2} \text{y}^{-1}$) calculated via ^{137}Cs , Hg peak depths, or $^{210}\text{Pb}_{\text{xs}}$, but also contemporary Hg fluxes and Hg inventories should be summarized in a table. In addition, it would make it easier to follow if these rates, fluxes, and inventories would also be displayed in maps, as was done for locations and radionuclide (and other) profiles in Figures labeled “DRAFT Figure 2-1, 4-1 to 4-12; Sediment Coring Locations Thin Interval Core Sampling Report Penobscot River Phase III Engineering Study”.

Response: Revised in part as suggested. Table 2 already included sediment accumulation rates (cm y^{-1}) calculated via ^{137}Cs , Hg peak depths, and $^{210}\text{Pb}_{\text{xs}}$, and contemporary Hg fluxes. Sediment mass accumulation rates ($\text{g cm}^{-2} \text{y}^{-1}$) calculated via ^{137}Cs , Hg peak depths, and $^{210}\text{Pb}_{\text{xs}}$ have been added to Table 2, as suggested. Table 3 already included total Hg inventories. The suggestion regarding map revisions refers to the overall report, not the Yeager report specifically (which included no such maps). As such, this should be addressed as part of the revision of the overall report.

5. Appendix 1 of Yeager report lists an incorrect expression for water (fraction) content, f_w . Should be (sediment wet mass – dry mass)/wet mass, rather than (sediment wet mass/dry mass/wet mass).

Response: This was a typographical error, which has been revised as suggested. The actual calculations of F_w were carried out using the correct formula.

6. In tables, percent solids and percent solids residual are given, without any definition, and how that information was used in the report. The report only states that “Bulk density was performed at the Amec Foster Wheeler and University of Kentucky laboratories”. But, I could not find bulk density data anywhere in the report. Furthermore, ‘percent solids’ and ‘bulk density’ are not the same. Percent solids is commonly understood as weight percent in grams of dry sediments per grams of total (bulk) sediment, while bulk density is normally defined as grams of dry sediment per cm^3 of bulk sediment. 1 gram of bulk sediment is not equal to 1 cm^3 . I was wondering if there was any cross calibration between these two data sets. Furthermore, a definition of these terms, including porosity, and how they were calculated, should be given.

Response: Neither percent solids nor percent solids residuals were calculated or presented in the Yeager report. Bulk density data were calculated for the Yeager report as described in Appendix 1. These data, for every interval of every core processed at the University of Kentucky, were provided to the Wood Group in summary spreadsheets, as they requested (instead of in appendices included with the Yeager report). As such, all bulk density data should have been available upon request. To my knowledge, no effort was made to cross calibrate the percent solids and bulk density data sets. Appendix 1 of the Yeager report does define all relevant terms (i.e., those included in that report), including dry bulk density, fraction of water, fraction of organic matter, grain density, porosity, mass depth, and cumulative mass depth.

Thus, the appendices should better define and summarize the terms that are used in the report, e.g., how 1) sediment accumulation rate and sedimentation rate are defined and calculated; 2) contemporary Hg accumulation rate, and 3) Hg inventory are calculated.

Response: Not revised. All of the information requested here was already in the report. Specifically, 1) Sec. 3.4 defines sediment accumulation and mass accumulation rates, and how they were calculated; 2) Sec. 3.4 also defines how sediment accumulation and mass accumulation rates were determined using total Hg concentration profile data; and 3) Sec. 4.1 and Appendix 1 both define how total Hg inventories were calculated.

7. TOC and POC data tabulated in table 4-1 were determined by different methods. However, the data are not discussed in the report. Furthermore, I was wondering if there was any cross calibration of these two data sets.

Response: Not revised. The Yeager report considered only POC (not TOC). POC data were included in the summary spreadsheets accompanying the Yeager report, were considered when developing the Yeager report, but are not included in figures or data tables within the Yeager report itself. I am unaware of any cross calibration of the POC and TOC data sets.

8. Some titles to figures are not clear, e.g., Figure 24. Comment: Title ($\text{Hg } t_{1/2} - \text{At Hg}_{(\infty)} = 400 \text{ ng g}^{-1}$) is not clear, it would be better to write it out.

Response: Not revised. What is shown in this figure is written out clearly in the figure caption.

9. Relationship between ^{137}Cs and Hg derived sedimentation rates. It says in the Executive summary, page ES-iv, that “For these 21 cores from stations that were re-sampled in 2017, there was a strong statistical relationship between the ^{137}Cs -based sedimentation rate and the total mercury based sedimentation rate ($R^2 = 0.88$). Based on the robustness of this relationship, it was possible to estimate the sedimentation rate for 20 of the 34 cores analyzed for total mercury but not for radioisotopes.”

Response: No response required.

It is not clear, however, how the least squares relationship was used, if at all. For the Hg-derived sedimentation rate, the previously derived age (1967) of the Hg-peak depth by Santschi et al. (2017) and Yeager et al. (2018) was used. The age of the peak Hg discharge was derived from the geochronological reconstruction of the peak- ^{137}Cs in a core near the point source in the Penobscot River. Regardless, the Hg-derived sedimentation rates thus seem to be quite robust.

Response: Not revised. In the end, the least squares relationship was not figured into the estimates of sediment accumulation or mass accumulation derived using total Hg concentration profiles, as the correction that would have resulted would have been $< 10\%$ of the ^{137}Cs -derived rates.

10. Below, I review the document (WO4A-080 DRAFT_28Feb2018, including Appendix C, “Supplemental Spatial Analysis of Sedimentary Mercury (Hg) Distribution in the Lower Penobscot River Basin, ME – Informing System-Wide Remedial Design and Implementation”, by K.M. Yeager) and made some suggested improvements and pointed out some inconsistencies that need to be considered in any revision. In conclusion, once these inconsistencies are corrected, it appears to me that the differences in sedimentation rates, Hg inventories and fluxes between 2017 and 2009 data sets are likely even less pronounced than indicated in this report, indicating that for any remediation action, the whole 2017/2009 data set could be used as a guide.

Response: No response required.

Detailed Remarks:

1. Sediment inventories of total Hg

To verify the calculation of Hg inventories (calculated as $\Sigma \text{mass depth} * [\text{Hg}] * \text{depth interval}$), one needs to have access to the mass depth information, and how that was calculated from percent solids (or residual), which is given in the report, but I could not find that information anywhere.

Response: Total Hg inventories were calculated exactly as described above, and this was explicitly defined in Sec. 4.1 of the Yeager report. This information has also been added to Appendix 1 in the revised Yeager report for completeness. The calculations used to determine sediment mass depths and cumulative mass depths were given in Appendix 1 of the Yeager report, as mass depth (g cm^{-2}) = $[(1 - \varphi) \times \rho_s \times \text{interval thickness (cm)}]$; and cumulative mass depth (g cm^{-2}) = sum of mass depths over depth. Neither percent solids nor residual percent solids were used to calculate these values. Finally, the resultant values for mass depth and cumulative mass depth for every interval of every core were provided to the Wood Group in summary spreadsheets, as they requested (instead of in appendices included with the Yeager report). As such, all mass depth and cumulative mass depth data should have been available upon request.

In Figure 11 (incl. Table 3 and 4-1) the comparison looks quite good, except for Core PBR-28, where the 2017 value is about 9 times higher than the 2009 value, but Hg is always below $1,000 \text{ ng g}^{-1}$, confined to the upper 15 cm. It is not clear why, as Hg(o) values are quite similar, while the Hg(max) value is at least twice as high in 2009. No ^{137}Cs derived sedimentation rate is given for 2017; however, the Hg peak depth is about 14 cm (Table 4-1) while that for 2009 was about 20 cm, yielding a sedimentation rate of $\sim 0.4 \text{ cm y}^{-1}$ in 2009. In 2017, % solids was about 50% (Table 3), while the porosity in 2009 ranged from 88 to 60%. The results of this core, located in an embayment of the Penobscot River, are not shown in the subsequent comparisons of contemporary Hg fluxes, and little details are available to verify the reason for such a high inventory, except that this core was deemed not suitable for geochronological “modeling”. However, if it is suitable for Hg inventory calculation and comparison, then it should also be described in some better way for other parameters. Otherwise, it does not make sense to plot it together with ‘better-understood’ cores. Quite possibly, there was a mistake in the inventory calculation, as shown below, and thus, this needs to be checked and re-evaluated.

Response: Upon review, the total Hg inventory calculation for PBR-28 (2017) was correct, however a transcription error resulted in the wrong value being used to generate Figure 11. This has been corrected in the revised Yeager report, and the two values for this station (2009 and 2017) are quite similar. This necessitated that the left-hand panel of Figure 12 also be replaced, and the revised version exhibits a significantly improved linear relationship.

If we approximate g cm^{-2} in sediments by $50 \text{ g} / (50/2.5 \text{ ml} + 50 \text{ ml}) * 1 \text{ cm} = 5/7 = 0.7 \text{ g dry sediment cm}^{-2}$ wet sediment in 2017. In 2009, we have only porosity values given, but we can convert both into g cm^{-2} and compare: $\text{g cm}^{-2} \approx [(1 - \phi) \times \rho_s \times \text{interval thickness (1 cm)}] \approx 0.12 * 2.5 \text{ g cm}^{-3} * 1 \text{ cm} = 0.3 \text{ g cm}^{-2}$ to $0.4 * 2.5 * 1 = 1 \text{ g cm}^{-2}$ for 2009 for each 1 cm slice. This comparison shows that mass depth in 2017 is at most a factor of 2 higher than in 2009, but sedimentation rates are higher in 2009 (0.37 cm y^{-1}) than in 2017 ($\approx 14 \text{ cm}/50 \text{ y} = 0.28 \text{ cm y}^{-1}$). Together, given that Hg values in 2017 were also lower, this 9 times higher Hg inventory in PBR-28 from 2017 does not make sense, and is most likely a mistake. I conclude therefore that the comparison of Hg inventories is even better than is reported in the Yeager report, and outliers are likely due to errors. However, this assessment needs to be checked with exact numbers.

Response: The steps outlined in the previous response fully resolve this issue, so no additional response is required.

Alternatively to the way the Yeager report compares these data sets, I was wondering if one could argue with averages ± 1 standard deviation for 2009 and 2017.

Response: This approach is not unreasonable, however given that actual measurements are available for cores collected at the same stations during the two periods, the approach adopted by the Yeager report is both more representative and robust.

2. Sediment accumulation rates

The terms ‘sedimentation rates (cm y^{-1})’ and ‘sediment accumulation rates ($\text{g cm}^{-2} \text{y}^{-1}$)’ are commonly used in the published STOTEN papers from work done in 2009, not the other way, as it was done in the report.

Response: Not revised. In the Yeager report, and the STOTEN papers produced using the 2009 data set, the terms ‘sediment accumulation’ or ‘linear sediment accumulation’ refer to rates in cm y^{-1} ; whereas the term ‘sediment mass accumulation’ refers to rates in $\text{g cm}^{-2} \text{y}^{-1}$. This seems clear as it stands.

Also, some of the figures are misplaced. For example, the Hg inventory figure (Fig. 12) is with the discussion of sedimentation rates, and the sedimentation rate figures (Fig. 15-18) are with the discussion of contemporary Hg fluxes.

Response: Revised as possible. Convention was utilized here, where figures were incorporated into the text as quickly as possible following where they were cited. Given the data-intensive nature of the Yeager report, having some figures “spill over” into subsequent sections was unavoidable. In the revised Yeager report, we have tried to minimize this as possible.

Comparison of sedimentation rates between 2017 and 2009 in replicate stations. The sedimentation rates were quite similar, with three exceptions, PBR-19, PBR-16, and MM-7/C3, where the 2017 sedimentation rates were lower.

Response: Presumably, this refers to Figure 18; no response required.

Take PBR 19 as an example: While the sedimentation rate (cm y^{-1}) was higher by about a factor of 2 in 2009, the dry bulk density in 2009 was lower, and the surficial Hg concentrations, Hg(o), was also lower at that time. Thus, while there is a difference in sedimentation rates, the difference in Hg fluxes will be less significant (see below).

Response: No response required.

Take MM-C3-A (2017): Both total Hg and ^{137}Cs profiles could be interpreted with a peak around 25 cm rather than 20 cm (see Fig. 4-3), resulting in an apparent sedimentation rate for both tracers of the order of 0.5 cm y^{-1} , close to that of $^{210}\text{Pb}_{\text{xs}}$, rather than the value in the report (0.3 cm y^{-1}). In 2009, the apparent sedimentation rate reported by Yeager et al., and Santschi et al. for MM7 was 0.7 cm y^{-1} . Thus, the difference might be less than indicated in the report.

Response: For core MM-C3-A (2017) the mid-interval depths for peak concentrations of ^{137}Cs (18.5 cm) and total Hg (16.5 cm) yield sediment accumulation rates of 0.34 cm y^{-1} and 0.33 cm y^{-1} , respectively (assuming that peak ^{137}Cs and total Hg correspond to the years 1963 and 1967, respectively).

While the difference in sedimentation rates and other parameters in these three cores could be due to local heterogeneities, it could also be due to some mistakes, and this needs to be checked. As an alternative to the way the Yeager report compares these data sets, I was wondering if one could argue with averages ± 1 standard deviation for 2009 and 2017 for the different sites.

Response: The determination of sediment accumulation for all three cores noted above have been checked, and match the values reported originally in the Yeager report. We attribute the differences in rates between 2009 and 2017 at these locations to local heterogeneities, as Dr. Santschi mentions. The averages ± 1 standard deviation approach is not unreasonable, however given that actual measurements are available for cores collected at the same stations during the two periods, the approach adopted by the Yeager report is both more representative and robust.

3. Contemporary total Hg fluxes

The report defines contemporary total Hg fluxes as “Estimates of contemporary total Hg fluxes ($\text{ng cm}^{-2} \text{y}^{-1}$) to sediments are presented using the mean concentrations of total Hg (ng g^{-1}) in the upper 3 cm of sediment cores multiplied by mass accumulation rates (MAR) ($\text{g cm}^{-2} \text{y}^{-1}$) determined either by ^{137}Cs (geochronology cores) or total Hg peak depth.”

Response: This is correct, no response required.

Contemporary Total Hg Fluxes, as compared in Figure 20. First: It needs to be justified in the text (e.g., in the methods or results section), why these values were calculated in that way, i.e., taking appropriate values from 0-3 cm layers and not 0-1 cm depth. The sediment accumulation rate in $\text{g cm}^{-2} \text{y}^{-1}$ weighs denser sections in the sediment more heavily, and the 3 cm depth interval can be equivalent of six or more years of Hg accumulation. Thus, given the eight years since the last sediment sampling, when Hg fluxes are compared between 2017 and 2009, there is an additional error in the way it was calculated.

Response: Revised as suggested (see Results section). The mean total Hg concentration over the upper 0-3 cm interval was utilized in the determination of contemporary Hg fluxes because that was the approximate thickness of the active mixed layer as resolved from the 2009 data set (see PRMS, 2013; Yeager et al., 2018b).

In Figure 20, total Hg fluxes compare quite well between 2009 and 2017. However, there is one outlier, i.e., the PBR-19 value in the correlation of Hg fluxes in 2009 and 2017 values. This outlier requires further scrutiny.

Response: No response required.

When one recalculates values for 2017 using only a 1 cm depth interval, the comparison of results between the two sampling times ends up much closer than what is presented in the report, but with different values for both 2017 and 2009. This discrepancy should be mentioned and considered in the evaluation, and further scrutiny of the comparison of Hg fluxes should be carried out.

Response: The use of mean total Hg concentrations over the 0-3 cm interval is sound, and based on active mixed layer depth data presented in the original PRMS study (PRMS, 2013), which has been subsequently published in the peer-reviewed literature (Yeager et al., 2018a,b).

These inconsistencies in contemporary Hg fluxes at PBR-19 (values taken here from 0-1 cm depth) with those listed in Fig. 20 (listed as about 200 in 2017, and about $900 \text{ ng cm}^{-2} \text{y}^{-1}$ in 2009) are detailed below. Both are different from what I calculate below:

69% solids for 2017 = $(69 / (69/2.4)+31) = 1.18 \text{ g cm}^{-3}$ dry density.

2017: $0.5 \text{ cm y}^{-1} * 1.18 \text{ g cm}^{-3} * 1,164 \text{ ng g}^{-1} = 685 \text{ ng cm}^{-2} \text{y}^{-1}$

2009: $1.05 \text{ cm y}^{-1} * 0.84 \text{ g cm}^{-3} * 643 \text{ ng g}^{-1} = 567 \text{ ng cm}^{-2} \text{y}^{-1}$

These values seem to be pretty close to each other, but entirely different from what is listed in the report. After making these corrections, the contemporary Hg fluxes in 2009 and 2017 will be much more similar, whereby the differences are probably not significant considering local heterogeneity in these sediments.

Response: There are no “inconsistencies” as it stands. Upon review of the data from this station in 2009 and 2017, the mean total Hg concentrations over the 0-3 cm interval in each year were $1,066 \text{ ng g}^{-1}$, and $1,174 \text{ ng g}^{-1}$, respectively, which are quite similar. The main difference is found in the sediment accumulation rate, which was $0.88 \text{ g cm}^{-2} \text{y}^{-1}$ in 2009, and $0.22 \text{ g cm}^{-2} \text{y}^{-1}$ in 2017, which results in a much higher calculated total Hg flux in 2009 as compared to 2017.

PBR-18B, where surface Hg concentration values are, however, pretty close to each other and close to those listed in the report:

$$2009: 0.76 \text{ g cm}^{-3} * 0.4 \text{ cm y}^{-1} * 969 \text{ ng g}^{-1} = 295 \text{ ng cm}^{-2} \text{ y}^{-1}$$

$$2017: 32\% \text{ solids} = 32 / ((32/2.5) + 68) = 0.4 \text{ g cm}^{-3}$$

$$0.4 \text{ g cm}^{-3} * 854 \text{ ng g}^{-1} * 0.6 \text{ cm y}^{-1} = 203 \text{ ng cm}^{-2} \text{ y}^{-1}$$

These values agree pretty well with values shown in Figure 20, which are 320 ng cm⁻² y⁻¹ for 2009, and 200 ng cm⁻² y⁻¹ for 2017.

Response: No response required.

These two examples above show that contemporary Hg fluxes from 2017 and 2009 are much more similar, and thus, it is likely that the differences between 2017 and 2009 is less significant. These tentative calculations also show that those contemporary fluxes need to be further scrutinized with exact values. Alternatively, to the way the Yeager report compares these data sets, I was wondering if one could argue with averages ± 1 standard deviation for 2009 and 2017.

Response: It is not clear if the overall data set (2009 vs. 2017) would “agree” more or less if contemporary total Hg fluxes were calculated using Hg concentrations over a 0-1 cm or 0-3 cm interval. All of the flux calculations have been reviewed, and were correct. The averages ± 1 standard deviation approach is not unreasonable, however given that actual measurements are available for cores collected at the same stations during the two periods, the approach adopted by the Yeager report is both more representative and robust.

Any difference in fluxes or rates between 2009 and 2017 could also be related to the different flow regimes of the Penobscot River in summer (e.g., August) of 2017 (average of $\sim 7,500 \text{ ft}^3 \text{ sec}^{-1}$) vs. 2009 (average of $\sim 20,000 \text{ ft}^3 \text{ sec}^{-1}$), which could have resulted in different % solids contents. Values are taken from USGS website (https://nwis.waterdata.usgs.gov/nwis/uv?cb_00020=on&cb_00021=on&cb_00060=on&cb_00065=on&format=gif_default&site_no=01034500&period=&begin_date).

Response: This is possible, but is beyond the scope of the Yeager report.

4. Total Hg apparent recovery half times

Taking 21 years as recovery interval should be justified, as Santschi et al. (2017) decided to use 21 years as recovery interval because it is half of the inferred 42 (2009–1967) years since peak discharge of Hg recorded in sediments. Since sampling was conducted in 2017, 8 years later, one could also have decided to use an interval of 25 years as half of 50 years. While this would not make a lot of difference, it might shorten the estimated recovery half times a bit due to the fact that the exponential curve fit would generally begin at higher concentrations that would be more heavily weighted in the least squares curve fit.

Response: The only justification is that this is what the Wood Group project personnel requested, and this request was made based on the time scale (21 years) being consistent with what had been done previously (PRMS, 2013; Santschi et al., 2017). As Dr. Santschi points out, increasing the recovery interval from 21 to 25 years would have made very little difference in the results.

While half times for Hg recovery in PBR-19 are close to those determined in 2009, this is not the case for PBR-18, where the half recovery time is quite a bit higher, especially if 400 ng g⁻¹ Hg is assumed as the asymptotic value. Thus, these values need also be checked.

Response: The recovery time calculations for core PBR-18 have been reviewed, and are correct as given.

Figures 23, 24: Why is PBR-18 so different in recovery half-time? This station is near the Hg point source. The Hg fluxes at this station have actually decreased since 2009, but the recovery half time has greatly increased. The Hg surface concentration of a little over 900 ng g⁻¹ are now closer to the average of about 700 ng g⁻¹. I suspect that here, given the ‘raggedy’ profile in the upper 20 cm, the result might greatly depend on how a 21 (or 25) year Hg record is interpreted. The authors might want to comment on this. Alternatively, to the way the Yeager report compares these data sets, I was wondering if one could argue with averages ± 1 standard deviation for 2009 and 2017.

Response: The recovery half-time at PBR-18 is considerably longer in 2017 than in 2009, and this is a function of the very low slope value (0.004) of the best fit line to the total Hg concentration data over the relevant time period (21 years before present). In this core, the upper ~25 cm of the total Hg concentration profile is apparently homogenized, meaning that total Hg concentrations decrease very little over this depth interval, which corresponds in time to the relevant time period. The slope of the best fit line is utilized in the calculations of recovery half-times (regardless of what the asymptotic end point is set at), and as such, the half-time in this case is large. The averages ± 1 standard deviation approach is not unreasonable, however given that actual measurements are available for cores collected at the same stations during the two periods, the approach adopted by the Yeager report is both more representative and robust.

Figure 30. Title: Hg*t_{1/2} (y) is not clear. How about ‘t_{1/2} (y) of Hg’?

Response: Not revised. Between the labels on the figure panels and the information provided in the figure caption, it is clear to the reader what is being depicted.

5. Core transects in the Orland River and Mendall Marsh

Figure 28 is mislabeled. Figure caption says Mendall Marsh sediments, but label on horizontal axis in figure says ‘Distance from Orland River’. Also, to make it consistent, Figure 27 about the same thing in Orland River sediments should be shown in a consistent way, i.e., distance on the horizontal axis, not the vertical axis.

Response: The caption of Figure 28 has been revised as suggested. The plots in both Figures 26 and 27 have been revised as suggested, so that all of these figures are now consistent.

Also, it would be easier to follow if the discussion about Hg concentrations, inventories and fluxes in the Mendall Marsh transects would relate to the maps (Figs. 2-4 of summary report), as was attempted for locations and radionuclide (and other) profiles in Figures labeled “DRAFT Figure 2-1, 4-1 to 4-12; Sediment Coring Locations Thin Interval Core Sampling Report Penobscot River Phase III Engineering Study.”

Response: This suggestion refers to the overall report, not the Yeager report specifically (which included no such maps). As such, this should be addressed as part of the revision of the overall report.

Another comment about Figure 28. Orland River data indicate that the further away from the confluence with the Penobscot River, the slower the recovery, the lower the sedimentation rate, the lower the Hg flux and inventory. This is very convincing evidence that the source of this high Hg inventory and concentration is the Penobscot River. I fully agree with that conclusion. At that spot, there is also the flocculation and Hg scavenging zone based on other evidence (around 5-10 ‰ salinity), around where lots of Hg-laden suspended colloids and particles flocculate out, resulting in high Hg concentrations in these sediments (see Geyer and Ralston, 2018).

Response: No response required.

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